



**Determination of Chlorate by Flow
Injection Analysis Via Merging
zone Technique**

"Study and Application"

By

Rana Saheb Khalaf

A Thesis

Submitted to the Council of College of Science

University of Babylon

**In Partial Fulfillment of the Requirements for the Degree of
Master of Science in Chemistry**

September ٢٠٠٦

Sha'aban ١٤٢٧



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Supervisor

**Prof. Dr. Issam Mohammad
Ali Shakir Al-Hashimi**

**Prof. Dr. Dakhil Nasir Taha
Al-Zuragani**

September ٢٠٠٦

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تقدير الكلورات بتقنية الحقن الجرياني باستخدام المناطق المتداخلة دراسة وتطبيق

من قبل

رنا صاحب خلف

رسالة مقدمة إلى

مجلس كلية العلوم-جامعة بابل
وهي جزء من متطلبات نيل درجة الماجستير علوم
في علوم الكيمياء

شعبان ١٤٢٧

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بإشراف

الاستاذ الدكتور

داخل ناصر طه الزركاني

الاستاذ الدكتور

عصام محمد علي شاكر الهاشمي

شعبان ١٤٢٧

ايلول ٢٠٠٦

الإهداء

يا من ينخفض لهما الجناح وتطمئن النفوس برهما عند الغد والروح

شكراً أصلي لبارئ السمات

متوسلاً لحفظكما ذخراً وبركات

إليكما والدي ووالدي

أهدي جدي وأخلاصي والوفاء

الى . . . من جفف الدموع من عيني غامساً في نفسي الطموح

سانداً إياي بالفعل والكلمة نروحي العزيز

الى من هم سندي في شدتي وأنسي في وحدتي أخوتي وأخواني الى من اغرقوني بفضلهم

والد ووالدة نروحي وعائلتهما

الى النهر الذي يفيض بالعطاء الى من علمني سبل المعرفة والارتقاء

الى الشمعة التي تضيء من أجلكم العلم والعلماء الى أساتذتي الافاضل

أ. د. عصام محمد علي شاكر الهاشمي

أ. د. داخل ناصر طه الزهركاني

أهدي ثمرة هذا الجهد

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Praise be to Allah the Almighty for all that has been achieved.

Pray and Peace be upon the Prophet Muhammed, and his family and followers.

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Finally , I heartily thank my lovely husband and all those who help me in love way or another for their continuous encouragement, support and care.

Dedication

To those who are humbly served

And souls feel safe all the time by their respect

I pray to thank Allah

Beseeking him to keep you a treasure and blessings for you both my father and mother

I dedicate my effort Sincere and gratitude

To whom who dried tears from my eye

Existing ambitions in my soul

Assisting me actively and theoretically my dear husband

To those who are my support in my difficulty

And my partner with loneliness

My brothers and sisters

To the river which is full of gift

To whom who thought me the way of knowledge and superiority

To the candle which lights for the sake of science and scientists

To my dear teachers Assist Prof. Dr. Esam Mohammad Ali Shakir Al-Hashimi

And Prof. Dr. Dakhil Nasir Taha Al-Zuragani

I present the fruit of this effort

Rana

بِسْمِ اللَّهِ الرَّحْمَنِ الرَّحِيمِ

﴿ويسألونك عن الروح قل الروح من أمر ربي

وما أوتيتم من العلم إلا قليلاً﴾

بِسْمِ اللَّهِ الرَّحْمَنِ الرَّحِيمِ

الاسراء (٨٥)

Examination Committee

We are the examining committee, certify that we have read this thesis and examined the student **Rana Saheb Khalaf** in this content, and that in our opinion it is adequate with "Excellent" standing as a thesis for the degree of Master in Analytical Chemistry.

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Summary

This work includes the design of a whole flow injection analysis unit. Two paths were used, first using conventional spectrophotometric unit with home made valve and flow cell; while second unit a whole complete mini microphotometer based on radiation source, a special flow cell of ٢ mm path length and a photo silicon detector. With whole complete amplification and zero set. The unit is (٣x٣x٥ cm) on size.

The variable of physical and chemical of this method is based on the reaction of chlorate ion with potassium Iodide, coupling reaction in the presence of acidic medium forming I₂. Soluble has a maximum absorption at λ_{\max} ٣٥٠ nm.

This reaction in the first unit includes mixed hydrochloric acid (٢.٥M), potassium Iodide (٠.٥M) and flow rate (١.٩٥ ml.min⁻¹), for international injection unit.

Linear calibration graph for detection and measuring point with percentage linearity was in the range of (٠.٠٠٨٢٥ to ٤١٧٥ $\mu\text{g.ml}^{-1}$), for a sample of (١٢٧ μl) volume. Detection limit of (٦.١٢x١٠^{-٥} $\mu\text{g.ml}^{-1}$) was achieved.

The relative standard deviation was ٠.٠٤١% at two minutes for three successive measurement of chlorate ion with its applied method.

This method was applied successful in aqueous solution, match and hypochlorite are performed.

Physical and chemical parameters for determination of chlorate ion in the second unit includes mixed sulphuric acid ($1.0M$), potassium Iodide ($0.12M$), with flow rate ($4ml.min^{-1}$) and sample volume ($60\mu l$) for four successive measurement. The linearity of calibration graph was (0 to $600\mu g.ml^{-1}$), with detection limit about ($1\mu g.ml^{-1}$) and the percentage of R.S.D = 0.91% .

This unit was used for determination of chlorate ion in, home made and liquid detergent.

الخلاصة

تضمنت الدراسة تصميم جهاز تحليل الحقن الجرياني والذي اشتمل جزئياً: حيث تناول الجزء الاول استخدام جهاز قياس الطيف مع صمام مصنع محلياً، وخلية مصنعة محلياً (اسم)، بينما الجزء الثاني تناول وصف اجزاء منظومة مصنعة حلياً متكونة من صمام مصنع دولياً وخلية مصنعة محلياً (2 ملم) ومضخم مصنع محلياً لتقدير ايون الكلورات. المتغيرات الفيزيائية والكيميائية لهذه الطريقة اعتمدت على تفاعل ايون الكلورات مع يوديد البوتاسيوم في الوسط الحامضي وتقدير اليود عند طول موجي ($350nm$). هذا التفاعل تم تطبيقه في الوحدة الاولى تضمن مزج (2.5 مولاري) تركيز حامض الهيدروكلوريك و (0.5 مولاري) تركيز يوديد البوتاسيوم، وسرعة جريان (1.95 مل.دقيقة $^{-1}$) لمنظومة الحقن مصممة دولياً.

حيث ان منحنيات المعايرة لمتابعة تغير الاستجابة مع التركيز من (0.00825 الى 4175 مايكروغرام.مل $^{-1}$) لأنموذج حقن بحجم (127 مايكرو لتر) والحصول على حد الكشف (6.12×10^{-6} مايكروغرام.مل $^{-1}$). الانحراف القياسي النسبي كان مساوياً الى (0.041%) عند زمن حقن 2 دقيقة لثلاث قياسات متتابعة لتقدير ايون الكلورات.

هذه الطريقة طبقت بنجاح لتقدير ايون الكلورات في المحاليل المائية، الشخاط وفي محلول القاصر.

المتغيرات الفيزيائية والكيميائية لتقدير ايون الكلورات في الوحدة الثانية شمل مزج (١.٥ مولاري) تركيز حامض الكبريتيك، (٠.١٢ مولاري) يوديد اتلبيوتاسيوم وسرعة الجريان (٤ مل.دقيقة^{-١}) لحجم نموذج محقن (٦٠ مايكرو لتر) لاربعة قياسات متتابعة خطية منحني المعايرة كانت من (٥-٦٠٠ مايكرو غرام.مل^{-١}) والحصول على حد الكشف (١ مايكرو غرام.مل^{-١})، والانحراف القياسي النسبي مساوي الى (٠.٠٩١%). هذه الوحدة استخدمت لتقدير ايون الكلورات في محلول القاصر المستورد والمحلي.

Certification

We certify that this thesis is (**Determination of Chlorate by Flow Injection Analysis Via Merging zone Technique "Study and Application"**) prepared under our supervision at the Department of Chemistry, College of Science, University of Babylon, as a partial requirement for the degree of Master of Science in Chemistry and this work never published anywhere.

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In the view of the available recommendation , I forward this thesis for debate by the Examining Committee.

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شكر وتقدير

الحمد لله الأول الذي لا أول لأوليته .. والآخر الذي لا آخر لآخرته وأحمدته حمداً دائماً ما دامت السماوات والأرض وبقي الليل والنهار. وألف الصلاة والسلام على سيد المرسلين محمد (ص) الأمين وعلى خير خلقه ونجبائه أجمعين أهل بيت النبوة ومهبط الوحي وأمناءه على وحيه وخلقهم أجمعين ... ومن تبعهم بإحسان ووالاهم إلى يوم الدين ... وبعد.

يسرني وأنا أضع اللمسات الأخيرة في إعداد هذه الرسالة أن أقف وقفة شكر وتقدير وامتنان إلى أستاذي الفاضلين الأستاذ الدكتور عصام محمد علي شاکر والأستاذ الدكتور داخل ناصر طه لما قدماه لي من جهد علمي رصين ومخلص وما أبداه من توجيهات سديدة من أجل إيصالني إلى هذا المستوى.. فلهما الشكر والتقدير فجزاهما الله خيراً وأدامهما ذخراً للعلم والإنسانية.

كما وأتقدم بالشكر والتقدير الى الدكتور نغم شاکر تركي العوادي/ كلية العلوم- جامعة بغداد لما قدمته لي من مساعدة في اكمال هذا البحث ولم تبخل بأي نصيحة فاسأل الله أن يمن عليها بالموفقية والنجاح في دفع عجلة العلم في بلدنا.

ويسرني أن اشكر من تحمل معي عناء الدراسة بصبره وعطائه (زوجي العزيز) وأخيراً اشكر كل من وقف معي وقفة صدق ووفاء ولم يبخل بنصيحة أو جهد .

والله ولي التوفيق

Tables of corrections

Page	line	Error	correction
Dedication		Assist Prof. Dr. Esam	Prof. Dr. Esam
Abstract		Secondly	Second
۳ Table (۱.۱)		Adourless	Colorless
۴		This study (uses)	It used to describe
۱۳		FIA	SIA
۱۵		Reaoent ۱, Reaoent ۲	Reagent ۱, Reagent ۲
۲۰		The second carrier can also pass through a reaction coil for furthur dispersion or the first injection for injection in the second carrier.	The carrier can also pass through a reaction coil for further dispersion or dilution for removal a silce of peack from the first injection for injection in the second carrier
۲۰		۱ nal	۱ ml
۲۷ table ۲.۱		۸.۲۱۵	۸.۲۵۹, ۲.۴۷۷
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۲۸		volumetric flask	volumetric flask as in table (۲-۲), (۲-۳)
۳۰ ۲.۲ apparatus	۸	Home made	Germany
۳۰ ۲.۲ apparatus	۹	Germany	Home made
۳۰ ۲.۲ apparatus	۱۰	Amplifier [sketch diagram in figure (۳-۱۴)]	Amplifier
۴۰	۴	Value	Valve
۴۳	۳	Potentio metric	Potentiometric
۵۰	۷, ۸	L۲, L۱	L۱, L۲
۵۵	۲	L۱	L۲
۵۶	۱	Table (۴-۴):The effect of reagent volume [KI] on the reaction ($\text{ClO}_2^- - \text{I}^- - \text{H}_2\text{O}^+$) used in determination of	Table (۴-۴):The effect of reagent volume KI on the reaction ($\text{ClO}_2^- - \text{I}^- - \text{H}_2\text{O}^+$) used in determination of

		chlorate ion.	chlorate ion.
٥٧	١١	Table (٤-٥): The effect of sample volume [KClO _٣] in determination of chlorate ion.	Table (٤-٥): The effect of sample volume KClO _٣ in determination of chlorate ion.
٦٣ Fig. (٤-١٠)		٦٣٧	٦٢٦.٦٦
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٧٠ Table ٤-١١	Column ٤ line ٦	٢١٤.٦±٥.٧٣٦	٢١٣.٤±٥.٧٣٦
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٧٢ table ٤-١٢	Column ١١	Y=L.O.P	Y=L.O.D
٧٣	٣	٠.٠٥	٠.٥
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٧٦	٧	L١ , L٢	L٢ , L١
٧٦	٩ , ١٠	L٢ , L١	L١ , L٢
٧٨ table (٤-١٦)	Column ٥	%R	%RSD
٧٩ table (٤-١٧)	Column ٥	%R	%RSD
٩٢	١	Sample section volume (ml)	Sample section volume (μl)
١٠٦	٣	toward low	toward low

		concentration by amount ٦٠ ng for ٦٠ μl.	concentration by amount ٦٠ ng for ٦٠ μl.
١٢٦	١٠	$\text{ClO}^- - \text{I} - \text{H}^+ \text{O}^+$	$\text{ClO}^- - \text{I} - \text{H}^+ \text{O}^+$
١٢٦	١١	Khalat	Khalaf

Conclusions

and

Recommendations

Conclusions

١. FIA can be used to determine the trace concentrations of chlorate ion.
٢. The first design unit which consists of conventional spectrophotometric and homemade valve and flow cell can be used for determination of chlorate ion.
٣. The second design unit which consists of conventional valve and home made spectrophotometric and flow cell can also be used for the determination chlorate ion.
٤. The second design unit was more sensitive than the first one.
٥. Sequential injection analysis is used in the first design unit with good results.

Recommendations & further work:

١. Both design units can be used for determination of H_2O^+ and iodide.
٢. The introduction of the five three-ways valve and three three-ways expand the scope of new approaches for various determinations.
٣. Sequential injection analysis can be used to determine other ions instead of chlorate ion such as NO_3^- , Fe^{+2} , SO_4^{2-} ,

Conclusions

٦. FIA is used to determine the trace concentrations of ions.
٧. Using home made unit contains international valve and cell is home made (٢ mm).
٨. Comparison between international and home made unit.
٩. Sequential injection analysis is the best method in determination of chlorate ion.
١٠. The home detergent gives better results than imported one.

Recommendations:

٤. The home made unit is better than international unit to determination of low concentration ions.
٥. Using sequential injection analysis to determine another ions instead of chlorate ion.

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Chapter One

Introduction

CHAPTER ONE

1. Introduction

This chapter consists of two parts:

Part ((A)): This part deals with the distribution configuration, occurrence, properties, uses, generation, reactions and available methods for determination of chlorate ion.

Part ((B)) deals with the background of flow injection analysis.

Part ((A))

\ A- \ : Chlorate-General Introduction

The distribution configuration for chlorate ion is shown in figure (\ . \).⁽¹⁾

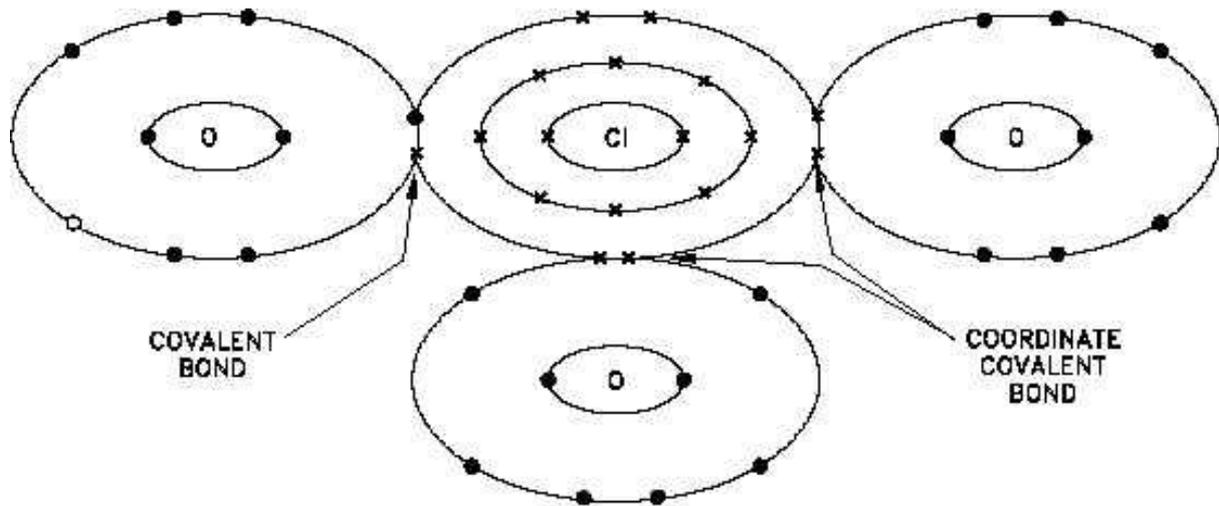


Figure (1.1) Configuration of chlorate ion.

The chlorates have been used historically as a herbicides to kill all terrestrial plants⁽⁷⁾, they also have a damaging effect when discharged to the recipient⁽⁷⁾ and the chlorates are oxidizing agents and all of their compounds are water soluble⁽⁸⁾.

1A-2: Occurrence

The fate of chlorates and their toxicity is linked closely to nitrate levels in the water⁽⁹⁾ and the critical nitrate levels appear to range from 0 $\mu\text{g.L}^{-1}$

where chlorate transport is rapid, to $10 \mu\text{g.L}^{-1}$, which almost completely inhibits nitrate transport^(7,8).

Recent monitoring data indicate that typical surface water concentrations of chlorates are about 0.04 mg.L^{-1} and about 0.02 mg.L^{-1} for the Rhine and IJssel rivers in the Netherlands^(8,9,10).

1A-3: Properties

Chlorates are a colorless, cubic or trigonal crystals or a white powder. The crystals are also reported to be pale-yellow or white which may be attributed to an impurities⁽¹¹⁾. Table (1.1) shows the properties of chlorate compound.

Table (1.1) Properties of chlorate compound⁽¹²⁻¹⁵⁾.

Colour	Boiling point b.p. °C	Melting point M.P. °C	Molecular weight M.wt g/mol	Density g/ml
a colorless	122 °C	248 °C	106.44 g/mol	2.49 g/ml

Chlorate is highly soluble in water; it is not toxic to bacterial suspension at a concentrations below 100 mg.L^{-1} ⁽¹⁶⁾ and the chlorate anion is unstable in water and decomposes to form oxy chloride ion and oxygen⁽¹⁷⁾.

1 A-4: Uses

Chlorate is used extensively for a variety of purposes; it used as a herbicide or defoliant, released when chlorine dioxide (ClO_2) is used as a bleaching agent in paper and pulp industry^(19, 20). Also it is used as the terminal electron acceptor^(19, 20).

It used in the manufacture of matches, explosive, dyeing, printing of fabrics, tanning and finishing of leather^(21, 22, 23).

1 A-5: Formation of chlorate

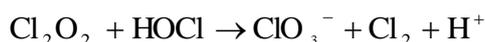
Chlorine dioxide oxidizes the organic material forming chlorite, which can then be oxidized to chlorate by ozone⁽²⁴⁾ or by hypochlorite⁽²⁵⁾. When the combination of chlorine dioxide and these disinfectant were used, chlorate is formed as a by product of chlorine dioxide generation⁽²⁶⁾. It can be present in a commercial hypochlorite solutions^(27, 28), ozonation of water with a chlorine residual⁽²⁹⁾, and chlorine dioxide residual⁽³⁰⁾, also results in the formation of chlorate.

It can be formed by decomposes of sodium hypochlorite by effect of temperature⁽³¹⁾.



And when excess of chlorine is present, the intermediate will form chlorate according to reactions below⁽³²⁻³⁵⁾.





chlorate ion can also be formed by reaction between chlorine dioxide and chlorine; therefore, that reaction may account for a fraction of the ClO_3^- in ClO_3^- treated samples⁽³⁷⁻³⁸⁾.

Table 1.2: Reactions of chlorate ion at different chemical media^(39, 40, 41). This reactions can be indicated table (1.2).

Table (1.2) Reactions of chlorate ion.

Reaction media or reagent used	Main reaction equation	Reaction product	Remarks
1. H_2SO_4 (concentrated)	$\text{KClO}_3 + \text{H}_2\text{SO}_4 \rightarrow \text{ClO}_2 + \text{HClO}_3 + \text{KHSO}_4 + \text{H}^+$	Greenish-yellow gas	Evolved gas form orange-yellow solution with H_2SO_4
2. HCl (concentrated)	$\text{KClO}_3 + \text{HCl} \rightarrow \text{Cl}_2 + \text{H}_2\text{O} + \text{KCl}$		Give a yellow colour due to the liberated Cl_2 gas acid
3. NaNO_2 (solution)	$\text{KClO}_3 + \text{NaNO}_2 \rightarrow \text{KCl} + \text{NaNO}_3$	Chlorate reduction to chloride	
4. AgNO_3 mixture $\text{HNO}_3 + \text{NaNO}_2$ (solution)	$\text{KClO}_3 + \text{AgNO}_3 + \text{HNO}_3 + \text{NaNO}_2 \rightarrow \text{AgCl} \downarrow + \text{KNO}_3 + \text{HNO}_3 + \text{NaNO}_3 + \text{O}_2$	White precipitate of silver chloride	Reduction of chlorate to chloride
5. Potassium Iodide (solution)	$\text{ClO}_3^- + \text{I}^- + \text{H}^+ \rightarrow \text{Cl}^- + \text{I}_2 + \text{H}_2\text{O}$	Pale yellow colour	Iodine liberation
6. Ferrous sulphate (solution)	$\text{KClO}_3 + \text{FeSO}_4 + \text{H}_2\text{SO}_4 \rightarrow \text{KCl} + \text{Fe}_2(\text{SO}_4)_3 + \text{H}_2\text{O}$	Formation of chloride	Reduction of chlorate to chloride
7. Indigo test	$\text{KClO}_3 + \text{H}_2\text{SO}_4 \rightarrow \text{Cl}_2$ or HClO_3	A pale-blue colour is form	The chlorate is reduced by the sulphuric acid to chlorine or to hydrochloride and the later bleaches the indigo
8. Aniline sulphate test		A deep-blue colour	
9. Manganous-sulphate-phosphoric acid test	$\text{Mn}^{2+} + \text{PO}_4^{3-} + \text{H}^+ + \text{ClO}_3^- \rightarrow \text{Cl}^- + \text{H}_2\text{O} + [\text{Mn}(\text{PO}_3)_2]^{2-}$	Violet-colour	To form mangani-phosphate ion and reduction of chlorate to chloride

1. Action of heat (1, 2, 3, 4)	$2\text{KClO}_3 \rightarrow 2\text{KCl} + 3\text{O}_2$ $2\text{KClO}_3 \rightarrow \text{KClO}_4 + \text{KCl} + \text{O}_2$	White product	Form chloride and oxygen Form perchlorate
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1A-4: Determination of chlorates

Different classical methods were used for the determination of chlorate ion. Table (1.3) tabulates some of the available methods.

Table (1.3) Determination of chlorate ion.

Base of the method	Main reaction scheme	Determination of product	References No.
1. Volumetric method	$\text{ClO}_2^- + \text{I}^- + \text{H}^+ \rightarrow \text{Cl}^- + \text{I}_2 + \text{H}_2\text{O}$	- Determination of released iodine by titration with standard sodium thiosulphate solution	40
	$\text{ClO}_2^- + \text{Fe}^{2+} + \text{H}^+ \rightarrow \text{Cl}^- + \text{Fe}^{3+} + \text{H}_2\text{O}$	-The excess (Fe^{2+}) ion is determined by titration with standard dichromate solution	46
2. Gravimetric method	$\text{ClO}_2^- + \text{Fe}^{2+} + \text{AgNO}_3 + \text{H}^+ \rightarrow \text{AgCl} + \text{OH}^- + \text{Fe}(\text{NO}_3)_2$	- By precipitation as silver chloride (AgCl).	47
3. Ion chromatography with post column reaction	$\text{I}^- + \text{ClO}_2^- + \text{H}^+ \rightarrow \text{I}_2 + \text{Cl}^- + \text{H}_2\text{O}$ $\text{I}_2 + \text{I}^- \rightarrow \text{I}_3^-$	-Chlorate is analyzed by ion chromatography followed by an osmate catalyzed post column reaction of chlorate with iodide.	48
4. Biological reduction method	$3\text{ClO}_2^- + \text{H}_2 \rightarrow 3\text{H}_2\text{O} + \text{Cl}_2 + \text{O}_2$	-Determination of high conc. Of chlorate ion in waste water by using micro. Organisms chlorate as an electron acceptor and hydrogen gas as a reducing agent.	49
5. Flow injection analysis		-Determination of chlorate by iodometry method in FIA	50, 51

Part ((B))

1 B-1: Flow Injection Analysis

FIA (Flow Injection Analysis) is a widely used technique for the determination tracing elements and the designation of FIA was proposed in 1970 by Ruzicka and Hansen^(22,23,24), and defined it "information gathering from a concentration gradient formed from an injected, well defined zone of a fluid, dispersed into a continuous unsegmented stream of a carrier⁽²⁵⁾".

The simplest flow analyzer consists of a pump, which is used to propel the carrier stream through a narrow tube, an injection valve, a micro reactor in which the sample, zone disperses and reacts with the components of the carrier stream, forming species that are sensed by a flow through a detector. The obtained signal is recorded on any read out system^(26, 27). Basic flow injection system is shown in figure (1.2).

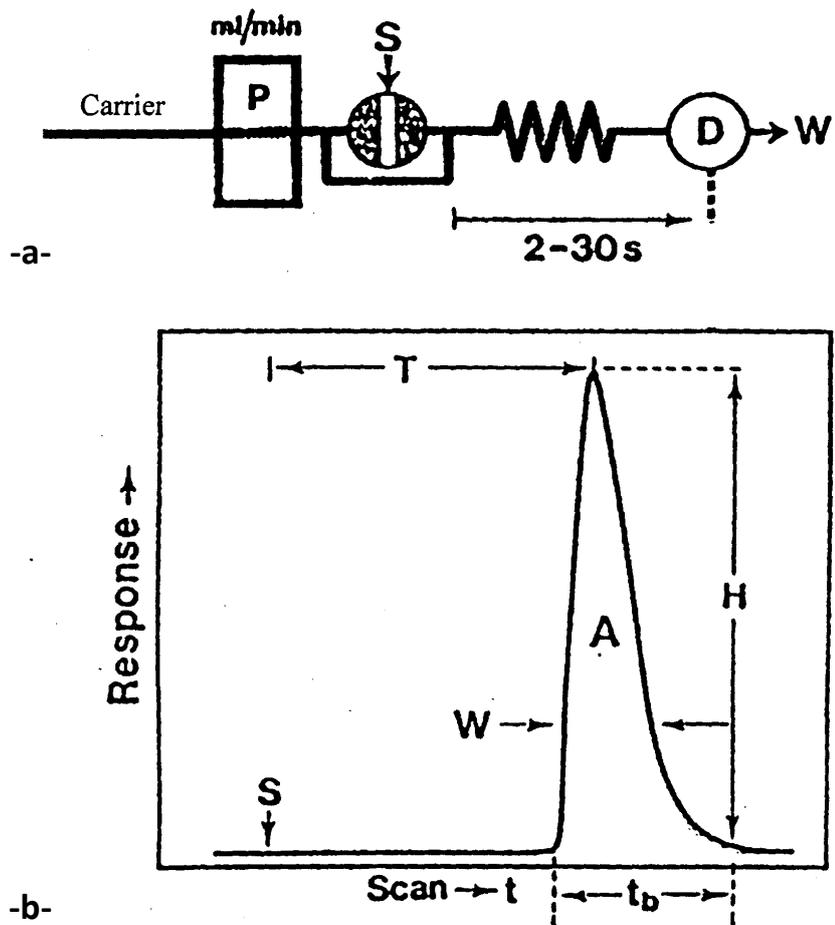


Figure (1-2): A schematic diagram of the basic flow injection system

a: The simplest single flow injection analysis manifold utilizing a carrier stream of reagent.

b- The analog output has the form of a peak

Figure (١.٣) shows the main stages that could be used in flow injection analysis^(٥٨, ٥٩).

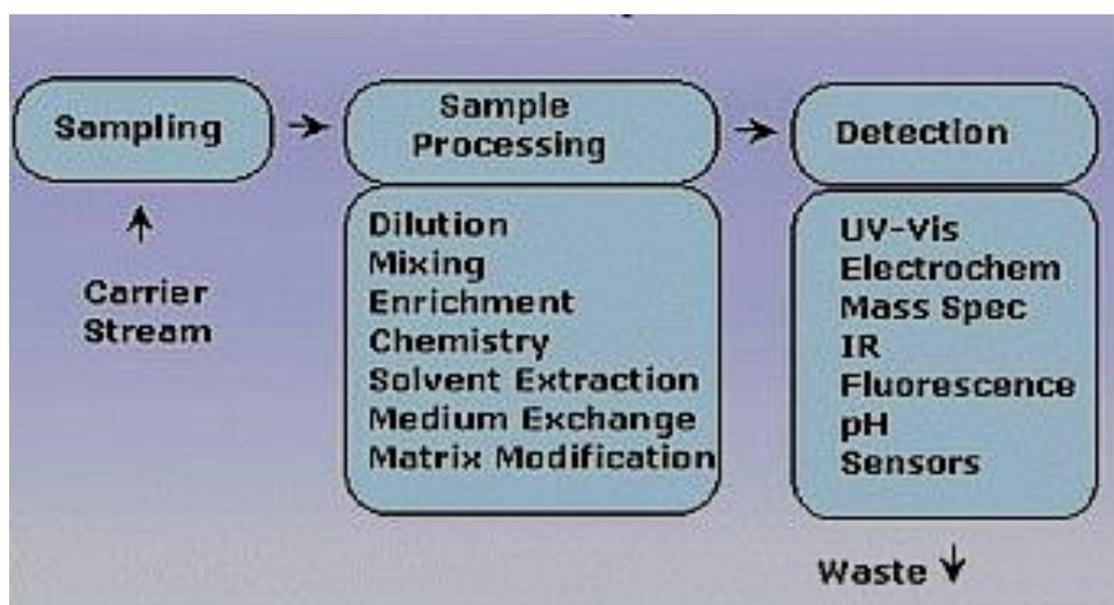


Figure (١-٣): Main steps in flow injection analysis

There are two types of continuous-flow methods, segmented and unsegmented.

The segmented flow method commercialized by Technicon in the "Auto analyzer" system, which corresponds to the classical version, was first

described by Skegg's in 1957⁽¹⁾, the samples were propelled sequentially and air bubbles separate (segment) the flow⁽¹⁾. A wash cycle between samples was also included. The air bubbles were usually removed before they reach the detector cell⁽¹⁾, as in figure (1.4).

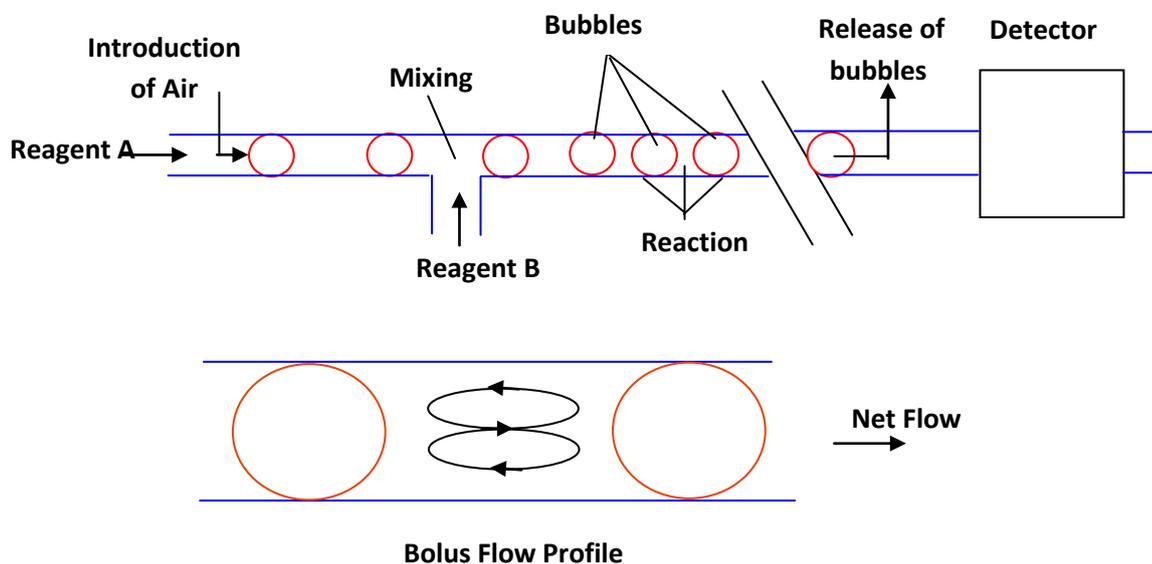


Figure (1-4): Air-segmented continuous flow analysis

While unsegmented-flow methods, described for the first time in 1974, are narrow and referred to as flow injection analysis methods and differ from segmented flow method.

The flow is not segmented by air bubbles, the sample is injected instead of propelled and neither physical (flow homogenization) nor chemical equilibrium has been attained by the time and the signal is recorded^(13, 14, 15). Figure (1.5) shows the laminar flow for unsegmented flow analysis.

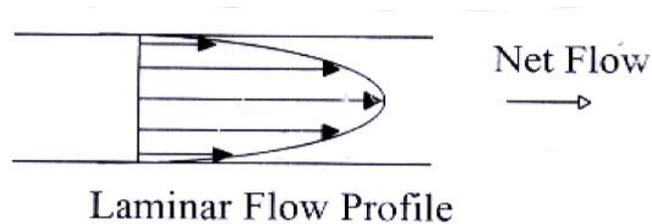


Figure (1.5): Laminar flow profile for unsegmented flow analysis

1B-2: Comparison between two chief continuous analyses segmented (sequential) (SFA) and un-segmented (FIA):

Figure (1.6) can be used to describe the basic components and principles of (FIA).

It's a simple and versatile analytical technology for automating wet chemical analysis, based on the physical and chemical manipulation of a dispersed sample zone formed from the injection of the sample a flowing carrier stream detection down stream^(16, 17).

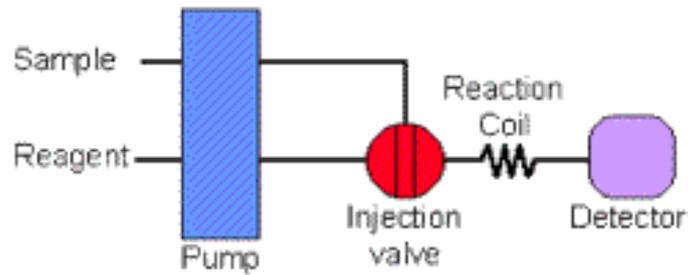


Figure (1-6): Simple flow injection analysis (un-segmented).

Sequential Injection Analysis (Segmented) is a new generation of FIA; this approach is to automate the sample manipulation which arose from a need to simplify manifolds^(18, 19). Figure (1.7) shows the main explanatory idea of the technique.

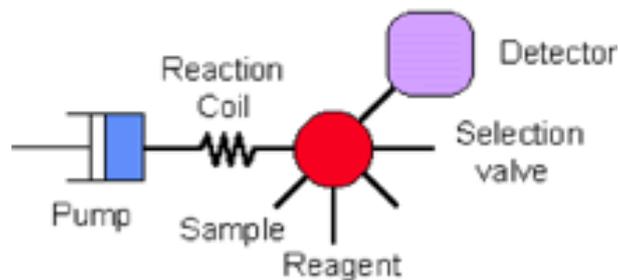


Figure (1-7): Simple Sequential Injection Analysis.

It should be stressed that (FIA) offers higher sample through put, uses smaller amounts of reagent, provides a layer number analytical data and opens new possibilities.

A detailed summary is presented in table (1.8).

Table (1.8) Comparison between (SFA) and (FIA).

Parameter	SFA	FIA	Ref.
Sample introduction	Aspiration	Injection	٧٠
Sample volume	٠.٢-٢.٠ ml	١٠-١٠٠ ml	٧١
Response time	٢.٠-٣٠٠ min.	٣-٦٠ sec.	٧٢
Bore tubing	٢.٠ mm	٠.٥-٠.٧ mm	٧٣
Detection	At equilibrium (homogeneity)	With controlled (dispersion)	٧٤
Sample throughput	≤ 8 sampler/hr	≤ 300 sampler/hr	٧٥
Precision	١-٢%	١-٢ %	٧٦
Reagent consumption	High	Low	٧٧
Wash-out cycle	Essential	Not required	٧٨
Continuous kinetic analysis	Not feasible	Stopped flow	٧٩
Titrations	Not possible	Possible	٨٠
Data produced	Peak height	Peak height Peak area-peak with peak to peak distance.	٨٠

The comparison between (FIA) and (SIA) can be noticed in the dispersion of the sample zone that is attained in both. It is worth noting that at the moment of injection in an (FIA) experiment, an un dispersed plug of sample is introduced into the carrier stream, while in (SIA) already during aspiration of the sample into the holding coil dispersion begins to take place and the flow

reversal that happens when the sample is sent off, plays a dramatic role in mixing the sample with the carrier^(1,12).

1 B-3: Development stages for FIA and Injection zone

1 B-3-1: Flow Injection Analysis (FIA)

The first generation of FIA techniques is also probably the most widely utilized⁽¹³⁾. In its simplest form, the sample zone is injected into a flowing carrier stream of reagent. As the injected zone moves down stream, the sample solution disperses into the reagent, causing the product to be formed. The modern flow injection analysis system usually consists of a high quality multichannel peristaltic pump, an injection valve, a coiled reactor, a detector such as a photometric cell and an auto sampler, additional components may include a flow through heater to increase the speed of chemical reactions, columns for sample reduction, de-bubblers and filters for particulate removal⁽¹⁴⁾.

Figure (1.8) Shows this generation and the emerging zone for it is shown in figure (1.9).

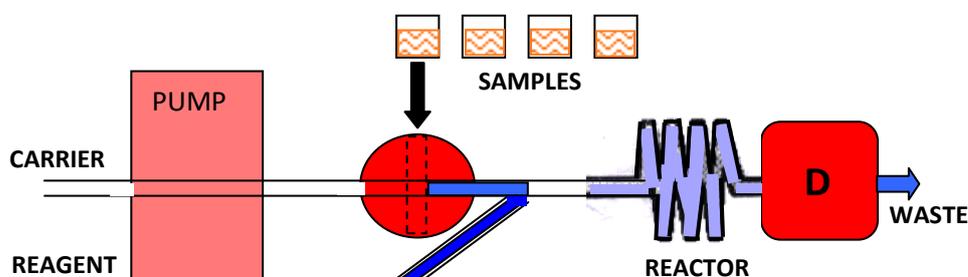


Figure (1-8): Flow Injection Analysis system.

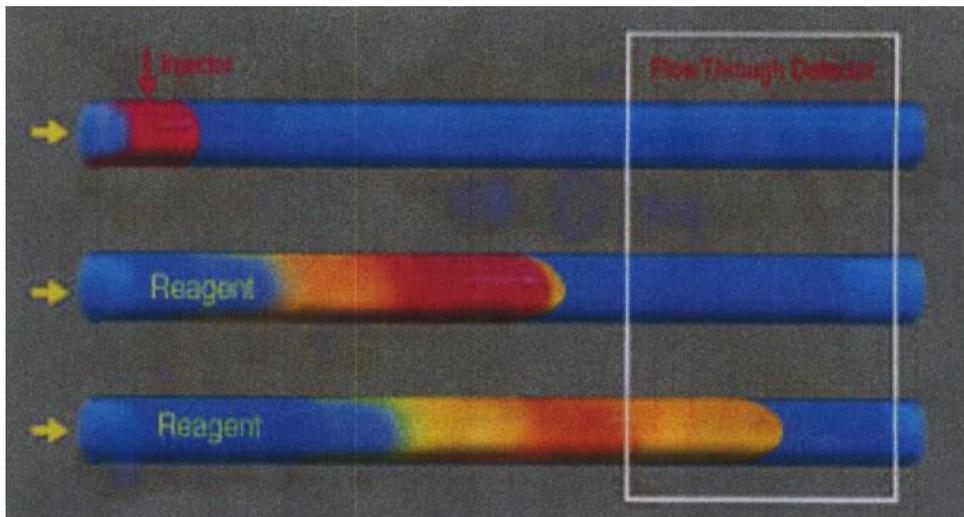


Figure (1-9): Emerging zone in flow injection analysis.

1B-3-2: Sequential Injection Analysis (SIA)

SIA is the second generation approach to flow injection analysis compatible assays. It usually consists of a single-channel high precision, bidirectional pump, a holding coil, a multiposition valve represented in (#1, #2, #3) and a flow through detector⁽¹⁰⁾.

This generation is indicated in figure (1-10).

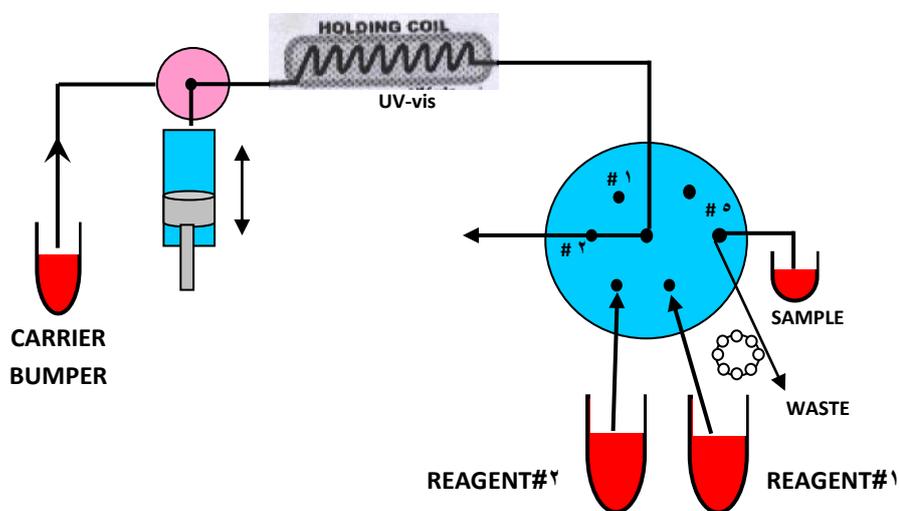


Figure (1-10): Sequential Injection Analysis system.

The system is initially filled with a carrier stream into which zone of sample and a zone of reagents (S), as in figure (1.11-A) , are sequentially aspirated into a holding coil, forming a linear stack, these zones become overlapped due to the parabolic profile induced by differences between flow velocities of adjacent stream lines such as in figure (1.11-B,C).

Flow reversals and flow acceleration further promote mixing. The multiposition valve is then switched to the detector position and the flow direction is reversed, propelling the sample/reagent zones through the flow cell which is indicated in figure (1.11)-D, E).

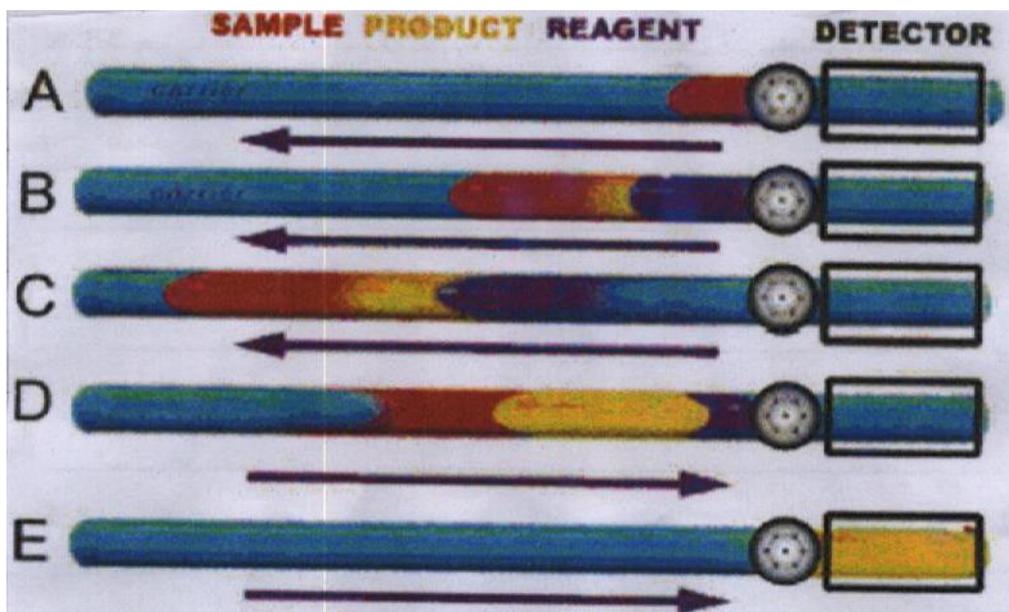


Figure (1-11): Sequential Injection Programmed.

1 B-3-3: Bead Injection Analysis (BIA)

BIA is the third generation and it is based on monitoring of (UV-Vis-IR) spectra of micro beads as they selectively capture a biomolecule of choice⁽¹⁴⁾.

To perform this assays, beads with a suitable interactant immobilized on their surface are trapped within a micro flow cell, where a solution containing bio molecule of choice is passed over bead surfaces by a precisely controlled flow, where reaction proceeds on surface of bead giving rise to reactant product^(14,15). Figure (1.12) shows third generation of bead injection analysis.

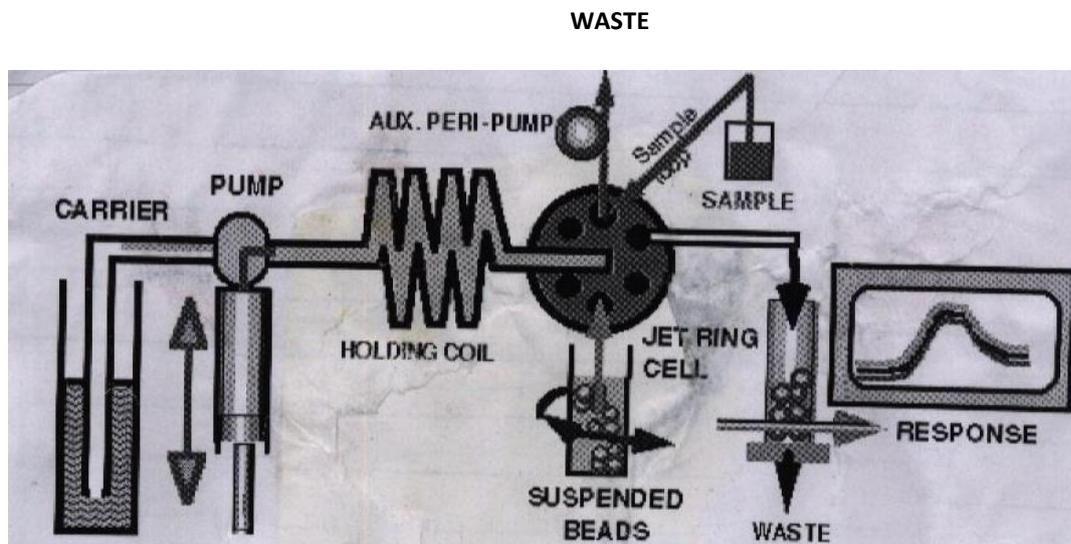


Figure (١-١٢):Bead injection analysis.

١B-٣-٤: Laboratory- On a valve

It is the fourth generation and it has been designed to miniaturized flow injection, sequential injection and bead injection, all with in a single monolithic mezzo fabricated component^(٩٠).

The precisely fabricated instrument integrates a flow through injection port, working channels and flow through cell in a strategically designed structure, that allows sample dilution, reagent addition, mixing, incubation and reaction rate measurements to be carried out under computer control in the forward, reversed flow/stopped flow regime⁽⁹⁾, (92, 93).

Figure (1-13): Laboratory fourth generation.

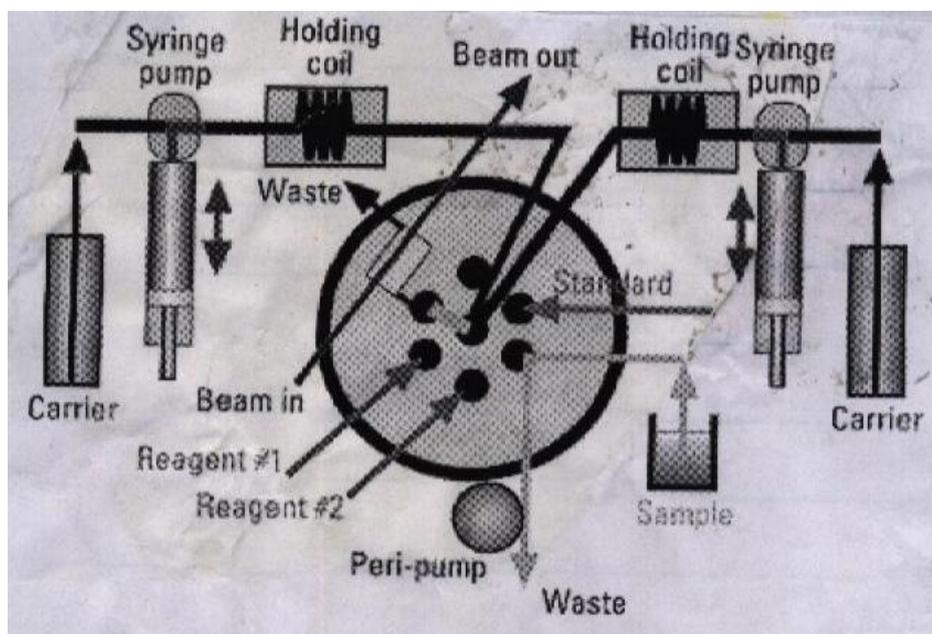


Figure (1-13): Laboratory-on a valve.

The sampling zone in flow injection analysis is a relatively simple and powerful technique for dilution. It is similar to the (heart-cut) technique used in chromatography.

It requires two sample injection valves set up^(٩٤-٩٨), as depicted in to the following figure (١٠٤).

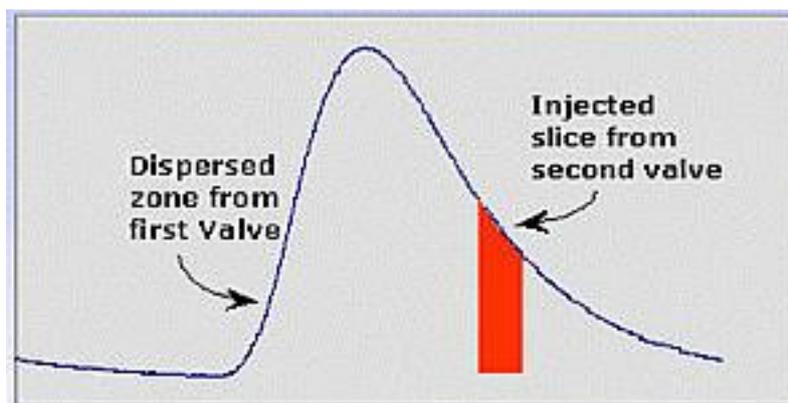
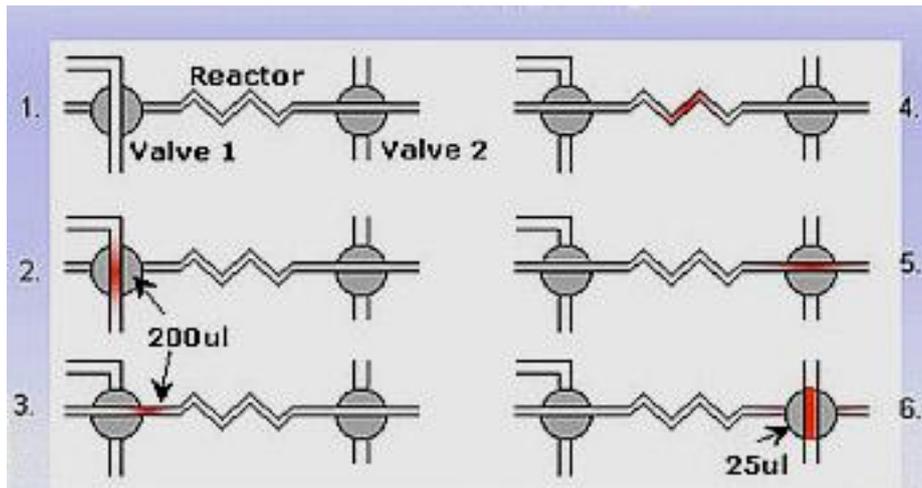


Figure (١٠٤): Zone sampling

In this first valve, a relatively large sample is injected, which then flows down dispersed by the reaction coil. As the dispersed sample zone fills the smaller sample loop of the second valve, a "a liquot" of the zone is injected into a second carrier stream⁽¹⁹⁾.

The second carrier can also pass through a reaction coil for further dispersion or the first injection for injection in the second carrier.

Dilutions by a factor of several hundred can be achieved. Precise timing of the two valves is important, requiring software or an electronic timer for optimum precision^(10, 11).

A gradient chamber is a simple device for dilution in FIA and SIA, as depicted in figure (1-10).

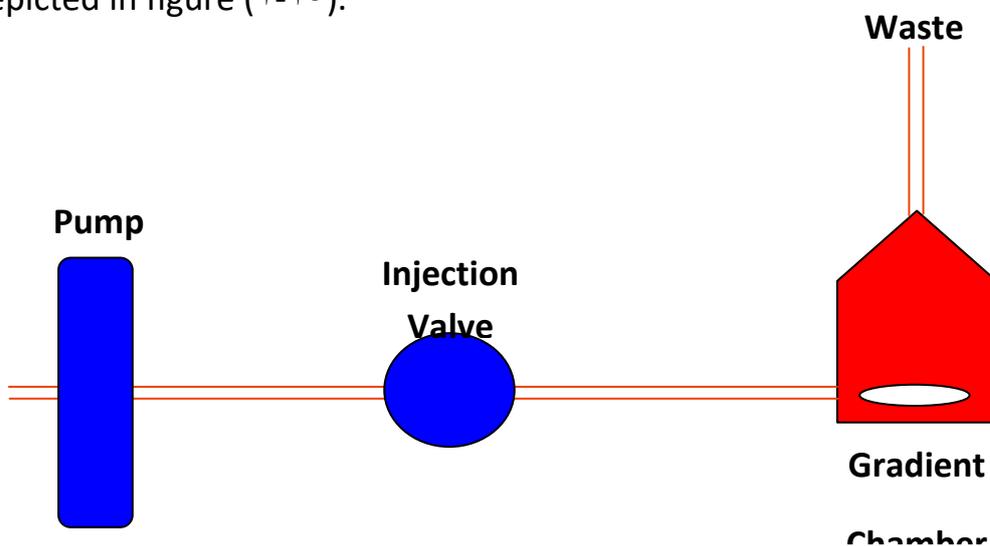


Figure (1-19): Gradient Chamber

The gradient chamber is small mixing vessel, generally with a stirring bar, an inlet and outlet for the carrier stream. The volume of the chamber is generally 1 ml or less. Sample is injected into the carrier and undergoes a large dispersion as it mixes with the much greater volume of the gradient chamber.

Dilutions by a factor of several hundred can be achieved with good precision^(1.1).

1B-4: Dispersion in flow injection analysis

The term dispersion coefficient (D) is defined as " the ratio of the concentration of the constituent of interest in a fluid element of the injected zone before and after dispersion^(1.1)". Expression of it is by equation (1.1):

$$D = C_0 / C \dots \dots \dots (1.1)$$

Where (C₀) is the original concentration of the constituent in the solution before dispersion, and (C) is the concentration of that fluid element of the dispersed fluid zone from which analytical read out is extracted. When the fluid element with the highest concentration is used for reading out, equation (1.1) is expressed as:

$$D = C_0 / C_{\max} \dots \dots \dots (1.2)$$

Where (C_{\max}) is the concentration of the constituent at peak maximum^(1.14).

There are two processes that contribute to dispersion:

First: pressure-driven (Laminar) flow in an open tube causes a parabolic flow profile, where solvent near the walls is stationary and solvent in the center moves with twice the average velocity.

The longer a solute passes through a tube, the more spread out it becomes. In the absence of diffusion, sample would be found along the entire length of the tube.

Second: The other source of dispersion is diffusion, which acts in two ways:

1. Diffusion along the length of the tube acts to dilute and spread the sample.
2. Diffusion in the radial direction acts to relax the parabolic profile.

The dispersion process typical of flow injection analysis system is shown in figure (1.16).

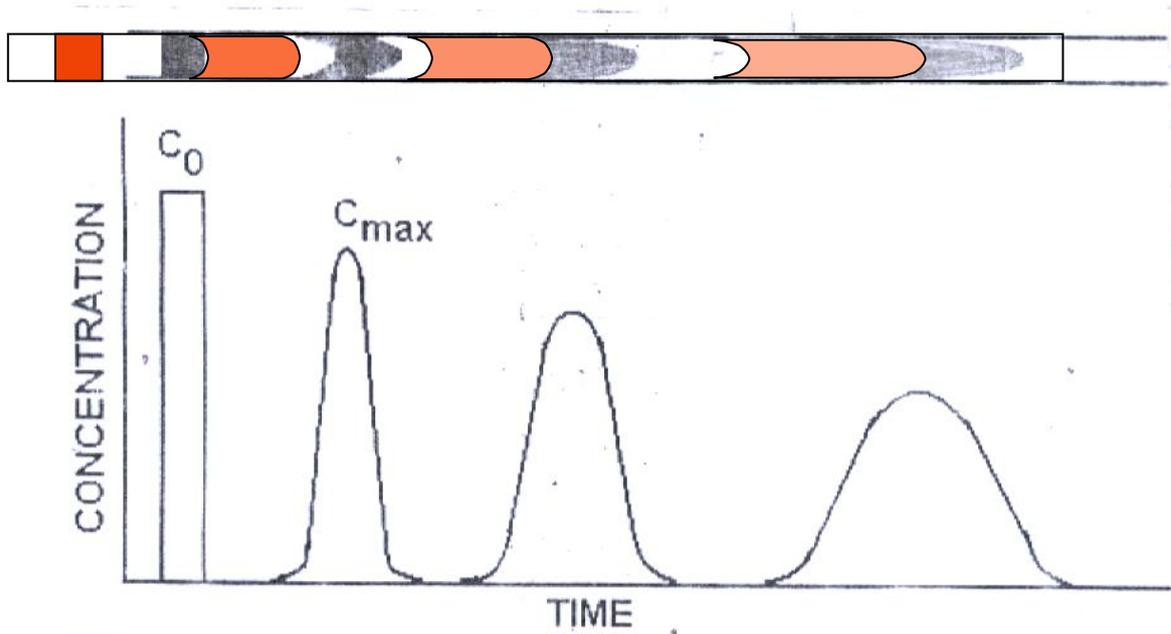


Figure (1-16): The typical dispersion process of (FIA) system

The sample is injected in a plug with concentration (C_0). The portion of the sample in the center of the tube moves down stream most quickly, while the sample at the tube wall is stationary⁽¹⁻⁹⁾.

Diffusion acts to relax the concentration profile in to a gaussian-shaped function.

The peak area is constant. Dispersion causes an increase in peak width and decrease in peak height.

There are three types of dispersion:

1. Limited dispersion

In one stream flow injection analysis, the sample is injected directly into the reagent stream and mixing occurs by dispersion as in the figure (1.18).

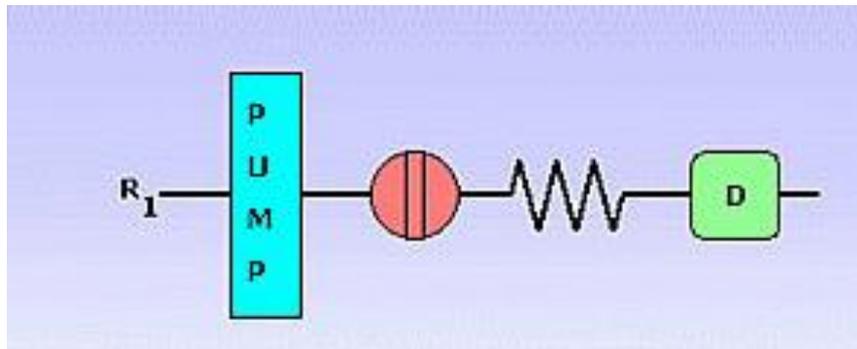


Figure (1-18): Single stream FIA

(R₁: Reagent 1, V: Valve, R.C.: Reaction Coil, D: Detector)

In two stream FIA, the sample is injected into buffer, while reagent is introduced in a separate stream; mixing is more efficient in this system (1.19), as in the figure (1.19).

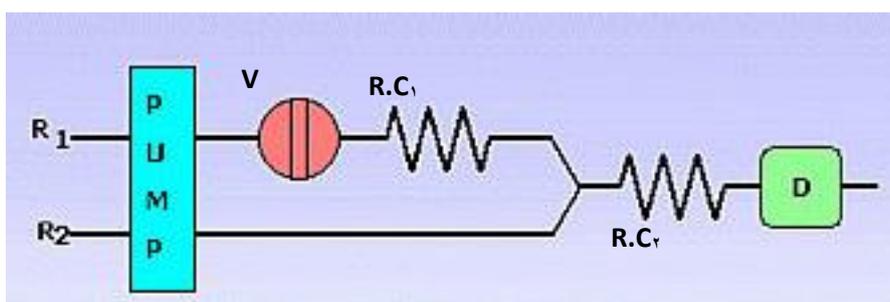


Figure (1-19): Two stream FIA

(R₁: Reagent 1, R₂: Reagent 2, V: Valve, R.C.: Reaction Coil,
D: Detector)

2. Large dispersion: ($D \gg 1$) FIA

Best for reactions needing time to equilibrate:

- Long reactors.
- Low-flow rates-(slow).
- Small sample volumes but high dispersion-(not used much)^(1.7).

1 B-9: Advantages of automation

1. Low cost and simple in instrumentation.^(1.8)
2. Low scheduled maintenance requirement.
3. Accurate and precise sample manipulation.^(1.9)
4. Quality control measures can be included to assure the integrity of the analytical results.
5. Applicable to a broad range of compounds by using a variety of reactions and simple photometric and electrochemical detectors^(1.10).
6. Constant flushing of the manifold lines minimizes the risk of fouling^(1.11).
7. A wide range of useful manifold components allows complex operations such as dilution, trace enrichment, gas permeation, dialysis and several others to be incorporated into the analyzer manifold^(1.12).

٢- Aim of research

This study aimed to:

١. Build up flow injection unit based on five-three ways valve which all together forms the home made injection valve. Also reaction cells were home made by using two loops.
٢. Design of flow injection unit based on cell and spectrophotometer.
٣. Style of flow injection unit depend on three-ways valve injection using one loop.
٤. Home made design of sequential injection unit depend on three-ways valve and cells using one loop.
٥. Determination of chlorate ion in an aqueous solutions, in safety matches and in hypochlorite solution locally manufactured (from Babylon company and Al-Fourat company) and an imported hypochlorite solution.

Chapter Two

Chemicals and Apparatus

CHAPTER TWO

2.1: Chemicals

All the chemicals used were analytical reagent grade and distilled water was used throughout the study.

2.1.1 Potassium Iodide

Potassium Iodide ($0.0M$) and ($0.10M$) were prepared by dissolving ($8.209g$, $2.477g$) in distilled water and completed to ($100ml$) in volumetric flask.

2.1.2 Potassium chlorate

Potassium chlorate ($0.00M$) and ($0.11M$) were prepared by dissolving ($0.30g$, $0.30g$) in distilled water and completed it to ($100ml$) in volumetric flask.

2.1.3 Hydrochloric acid

($0.0M$) was dilute ($100.2ml$) of (30%) HCl (sp.gr 1.18) with distilled water in a ($200ml$) volumetric flask.

2.1.3 Sulphuric acid

($0.0M$) was dilute ($20.04ml$) of (30%) H_2SO_4 (sp.gr 1.820) with distilled water in a ($200ml$) volumetric flask.

-Interfering ions solutions

All the solutions were prepared at the concentration of 100 ppm by dissolving an appropriate amount of each substance in distilled water and completed to 100 ml volumetric flask as in table (2-1), (2-2).

Table (2-1) Anion interfering solutions

Substances	Chemical formula	Interfering ion	Molecular weight	Weight (g)	Purity %	Company
Potassium permanganate	KMnO_4	MnO_4^-	158.03	0.132	99%	BDH
Potassium chromate	K_2CrO_4	CrO_4^{2-}	194.19	0.167	99.0%	BDH
Potassium sulphate	K_2SO_4	SO_4^{2-}	174.27	0.181	100%	Fluka
Potassium iodate	KIO_3	IO_3^-	214.00	0.122	99.0%	Riedal-DeHAEN
Potassium nitrate	KNO_3	NO_3^-	101.10	0.163	100%	Riedal-DeHAEN
Potassium chloride	KCl	Cl^-	74.59	0.209	99.0%	Riedal-DeHAEN
Potassium bromide	KBr	Br^-	110.40	0.148	99.0%	BAKER Analyzed

Table (۲-۲) Cation interfering solutions.

Substances	Chemical formula	Interfering ion	Molecular weight	Weight (g)	Purity %	Company
-Cadmium nitrate	$\text{Cd}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$	Cd^{+2}	۳۰۸.۴۷	۰.۰۲۷۴	۹۹٪	MERCK
-Copper nitrate	$\text{Cu}(\text{NO}_3)_2$	Cu^{+2}	۱۸۷.۰۰	۰.۰۲۹۰	۹۰٪	MERCK
-Cobalt nitrate	$\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$	Co^{+2}	۲۹۱.۰۴	۰.۰۴۹۳	۹۸٪	MERCK
-Ferric nitrate	$\text{Fe}(\text{NO}_3)_3$	Fe^{+3}	۲۴۰.۰۰	۰.۰۴۱۰	۹۸٪	MERCK
-Ammonium nitrate	NH_4NO_3	NH_4^+	۸۰.۰۰	۰.۰۴۴۴	۹۹٪	FLUKA
-Sodium nitrate	NaNO_3	Na^+	۸۰.۰۰	۰.۰۳۶۹	۹۹٪	RIEDAL-DEHAEN
-Lead nitrate	$\text{Pb}(\text{NO}_3)_2$	Pb^{+2}	۳۳۱.۰۰	۰.۰۱۰۹	۹۹٪	BDH
-Silver nitrate	AgNO_3	Ag^+	۱۶۹.۸۰	۰.۰۱۰۷	۹۹.۸٪	PANREAC
-Potassium nitrate	KNO_3	K^+	۱۰۱.۱۰	۰.۰۲۰۸	۱۰۰٪	RIEDAL-DEHAEN
-Tin chloride	SnCl_4	Sn^{+2}	۱۸۹.۶۹	۰.۰۱۰۹	۹۸٪	FLUKA
-Manganese chloride	MnCl_2	Mn^{+2}	۱۲۶.۰۰	۰.۰۲۲۹	۹۸٪	FLUKA
-Zinc sulphate	ZnSO_4	Zn^{+2}	۱۶۱.۳۰	۰.۰۲۴۷	۹۹.۰	MERCK

ॡ.ॡ: Apparatus

No.	Instrument or Equipment	Company
१.	Tubing pump model (Ismatic)	Germany
ॡ.	Spectronic ॡॡ (UV-Vis)	Milton Roy U.S.A
ॣ.	X-T Flat bed recorder No. (ॡ.ॣॡ Siemens)	Germany
।.	ॡ-ways injection valve (Merging zone version)	Home made
॥.	ॣ-ways injection valve (Merging zone version)	Home made
०.	Reaction coil made from glass, I.D=ॡ.ॡ mm, O.D=ॢ mm, Length= ॡ.ॡ cm	Home made
ॣ.	Flow injection cells: a- ॡ cm path length b-ॡ mm path length	Home made
०.	Balance, Sartorius, BL ॡॡ.ॡ	Germany
ॣ.	Tubes: A-sample loop made from teflon (ॡ mm I.D) :B: Glasses (ॣ mm I.D) :C- Nipples	Home made
ॡ.ॡ.	Amplifier	Home made

Chapter Three

Unit design

CHAPTER THREE

This chapter includes components of unit used in flow injection analysis and falls in two parts:

Part A:

It deals with the first unit which consists of pump, valves (home made), cell (1 cm) (home made), international spectronic, and recorder.

Part B:

It deals with the second unit which is composed of pump, international valve, cell (2 mm) (home made), spectronic (home made), recorder.

Part ((A))

ΨA- The components of the first unit:

This unit is composed of few channels peristaltic pump used to pump the carrier stream (acid solution) through the valve, variable flow rates can be obtained and this pump is shown in figure (Ψ. 1).

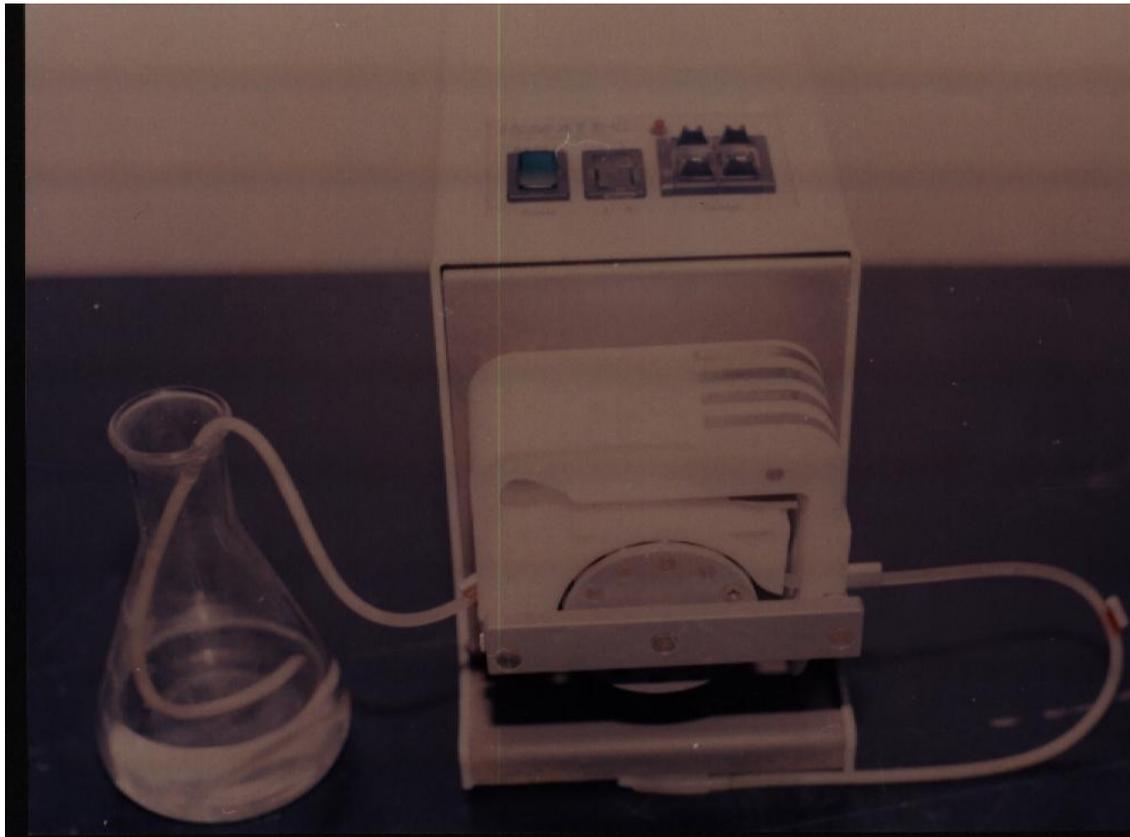
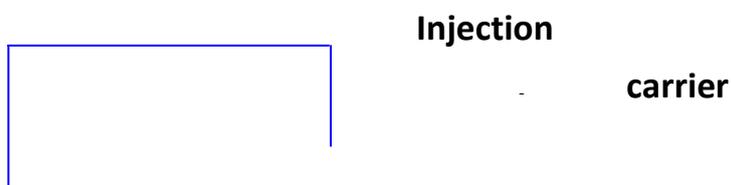


Figure (٣-١) Pump of flow injection analysis

The other part of this unit is five three- ways valve which is composed of five valve and two loops (L_1) and (L_2). (L_1) represents the interior loop that passes through it sample solution (Chlorate ion (ClO_3^-)) ($100 \mu\text{l}$) and (L_2) represents exterior loop that passes through it reagent solution (potassium iodide (KI)) ($31.5 \mu\text{l}$) and using valve (٢) to inject the sample (ClO_3^-) as in figure (٣-٢) and reagent show in figure (٣-٣) by valve (٣) and valve (٤) after moving it by angle (90°) to the left of the valve, valve (٥) is used to remove any quantity remained after filling (L_1) and (L_2).



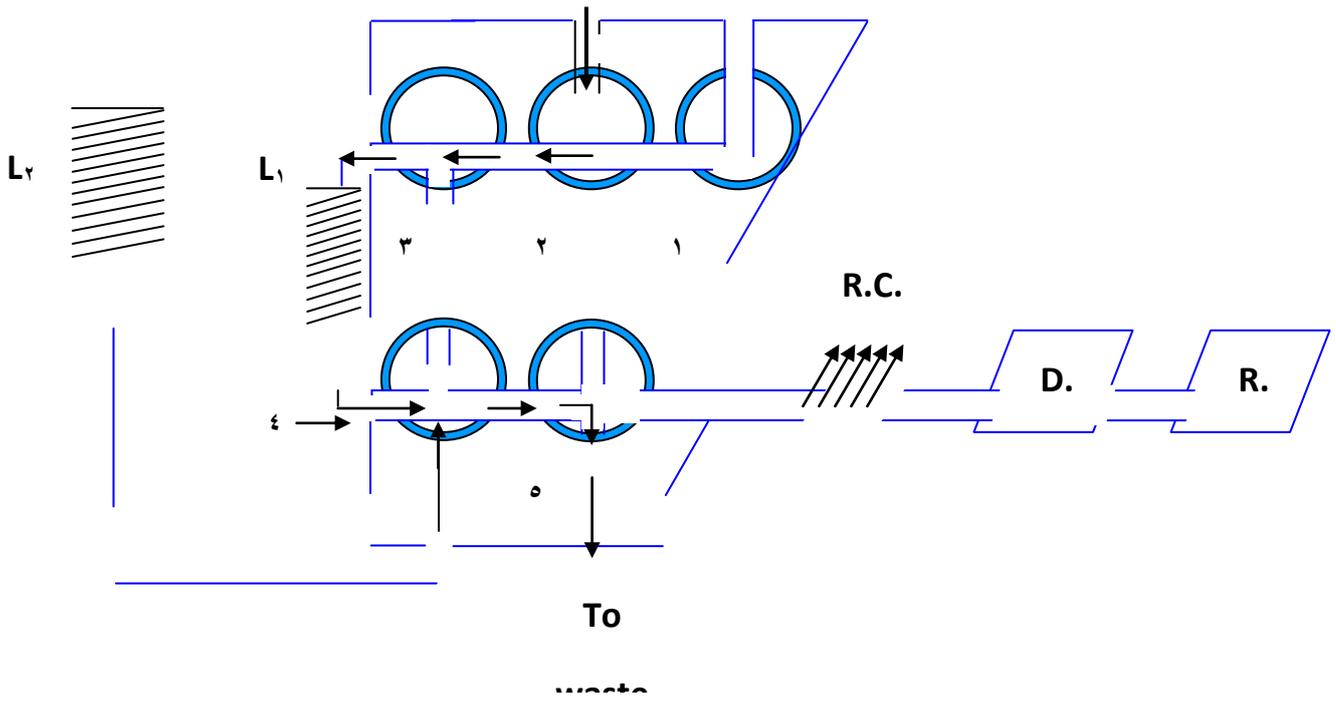


Figure (3-2): Injection the sample in loop (1)

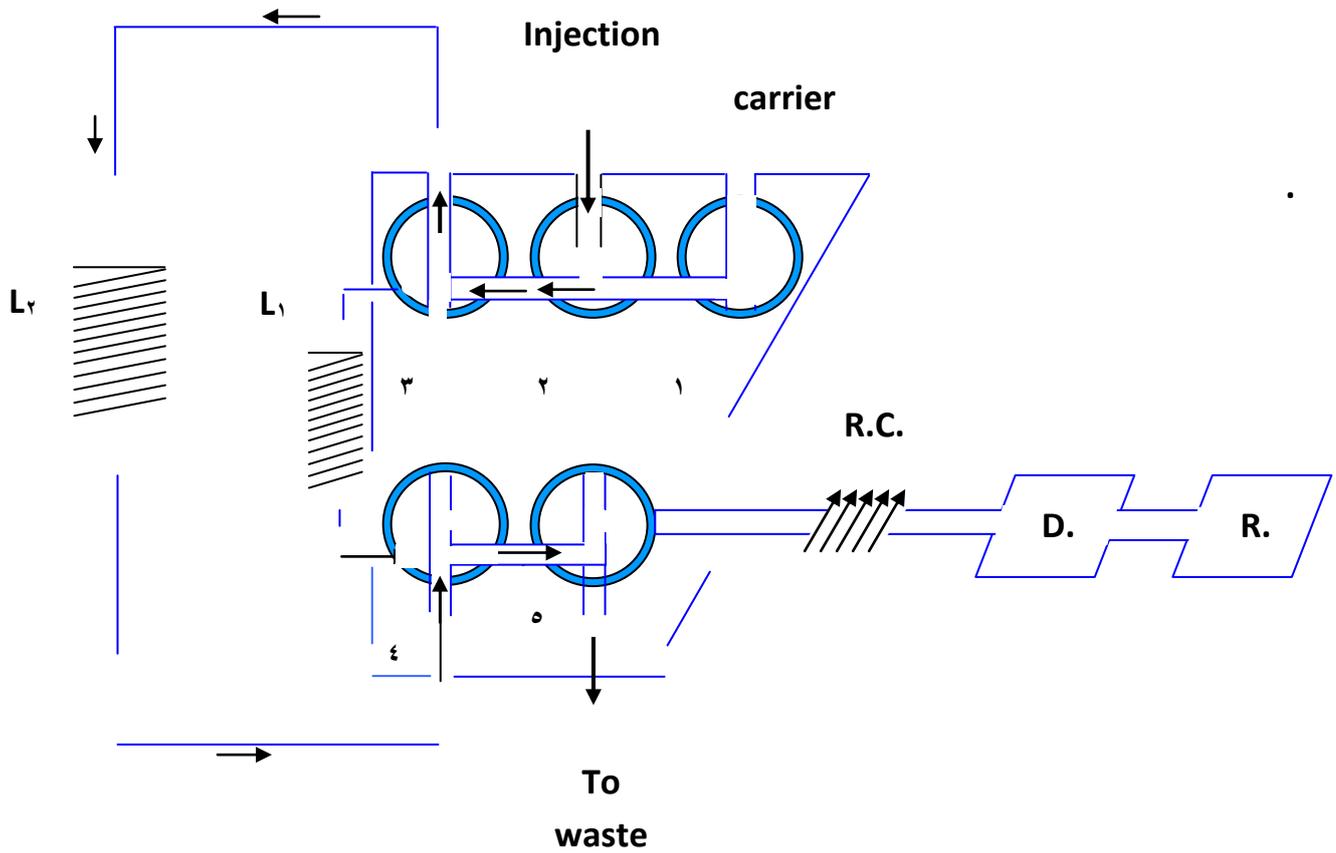


Figure (3-3): Injection the reagent in loop (2)

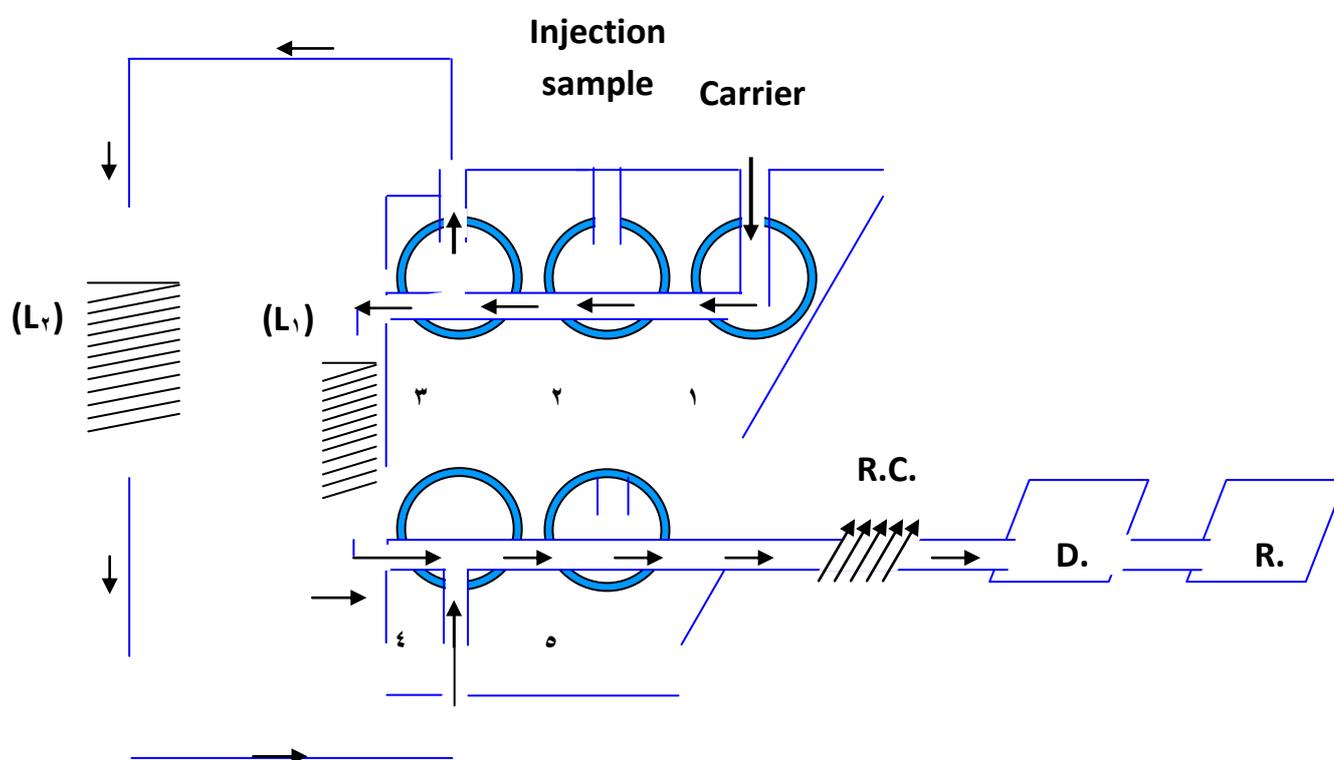


Figure (3-4): Shows the introduction of sample into the reaction manifold

Valve (1) is used to pass the carrier solution (Hydrochloric acid 2.0 M) through it to both loops and from it to manifold unit as shown in figure (3-4).

This valve which proves quite an alternative cheap, simple replaceable and easy to handle.

Three-Three ways valve has been used in this project; it is composed of one loop and three valves.

Valve (1) is used for injecting the sample volume and the carrier solution (composed of acid solution and the reagent), the sample volume ($125\mu\text{l}$) was injected in the loop and valve (3) is used to remove any volume of sample remains after injection the loop as shown in figure (3-5).

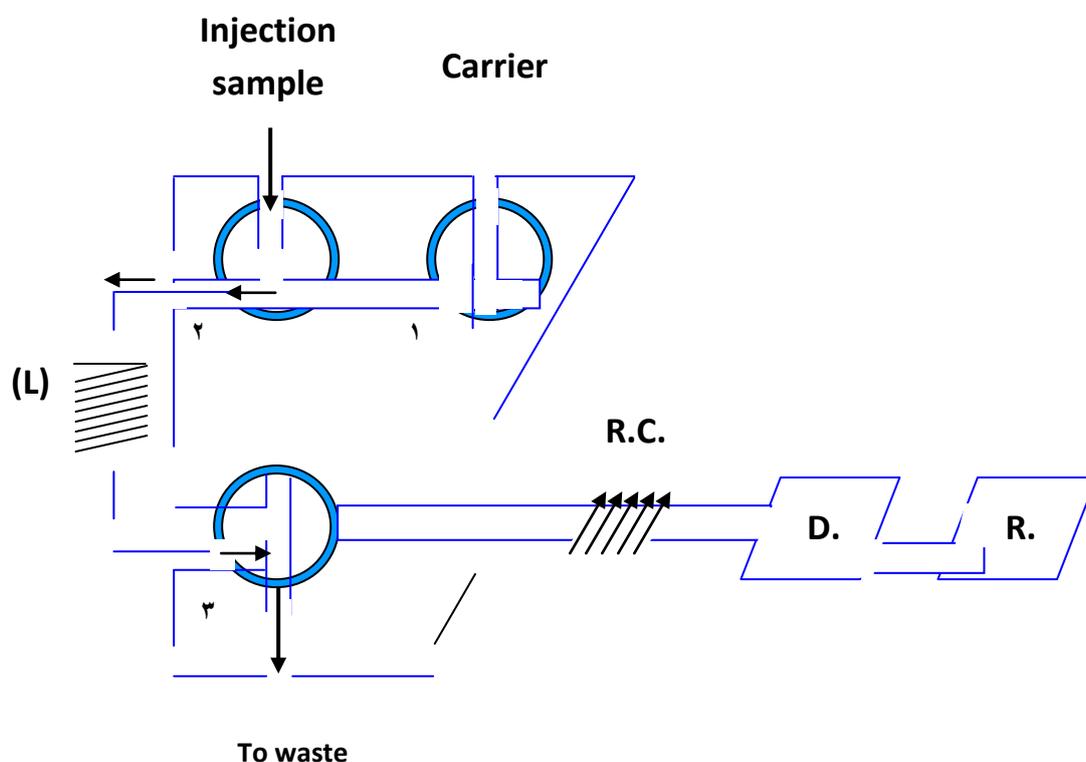


Figure (3-5): Injection of sample in the loop using three Three-ways valve.

Valve (1) passes the carrier solution from it to sample solution and through valve (3) then to the manifold unit and measures the absorbance at 300 nm as in figure (3-6).

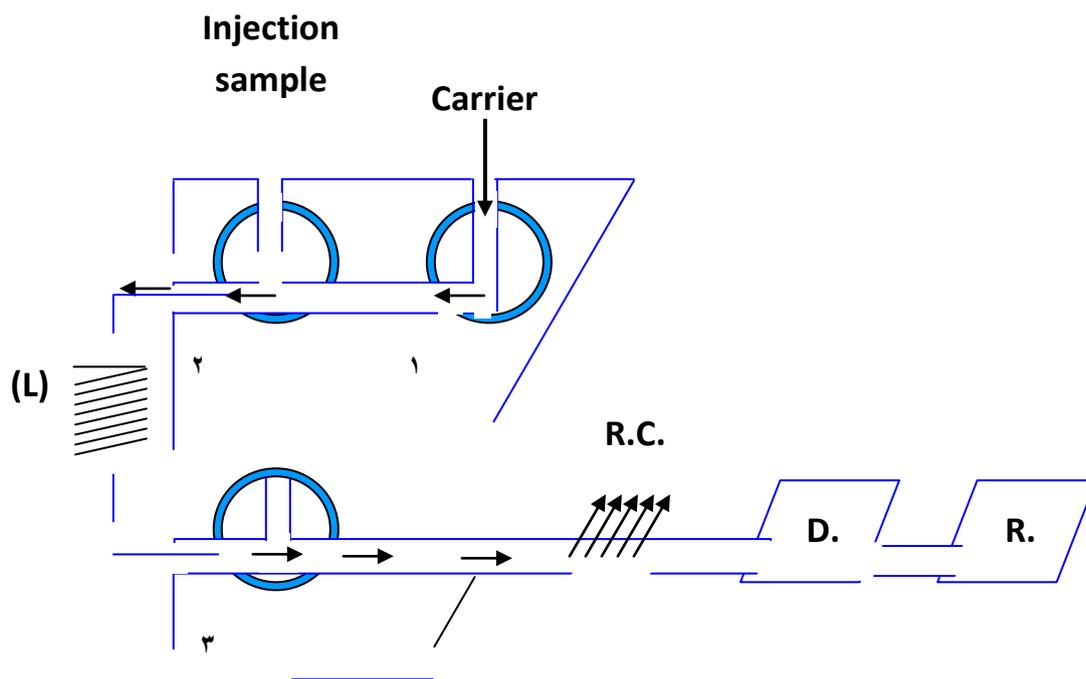


Figure (3-6): Introduction of sample in to reaction manifold

From five three- ways valve to reaction coil (RC: 100 cm in length with 2 mm I.D) where the main reaction is conducted as shown in figure (3-7).

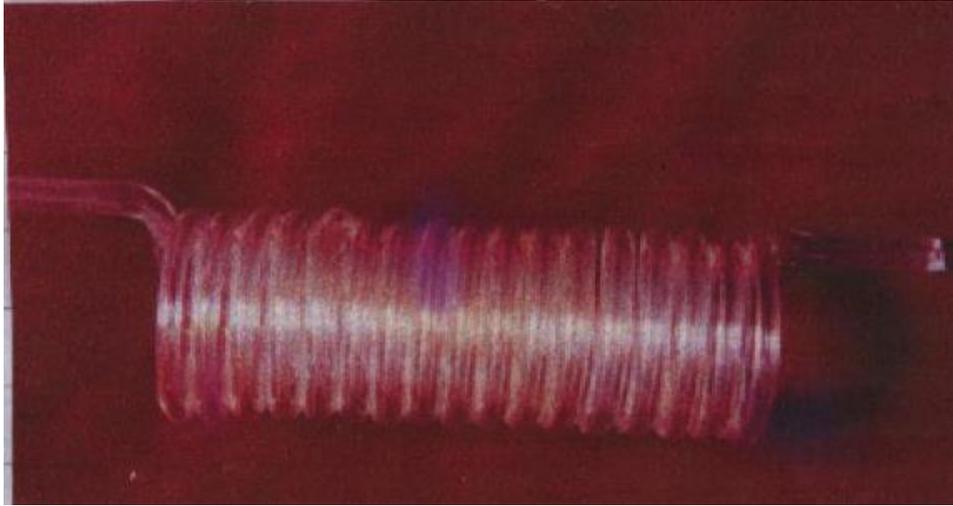


Figure (۳-۷): Reaction coil.

The next part flow-through cell that consists of two ends. The lower end represents the entry for the liquid and the upper end represents the going out of the liquid. The contact with the area of the passing light is made of quartz.

This cell gave acceptable repeatability through the work conducted in this project as shown in figure (۳-۸).

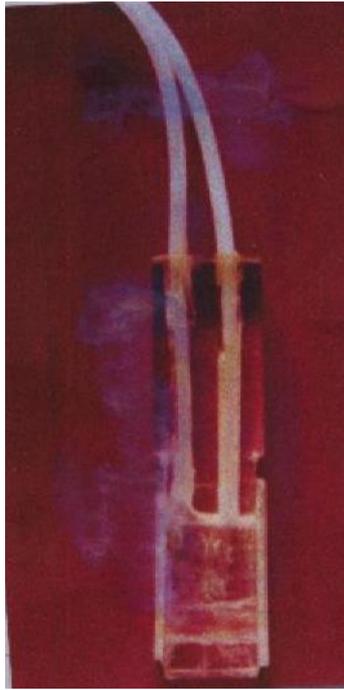


Figure (3-8): Absorption cell.

The absorbance that is obtained from spectrophotometer can be measured the signal by recorder. The whole components forming the unit are shown in the figure (3-9).

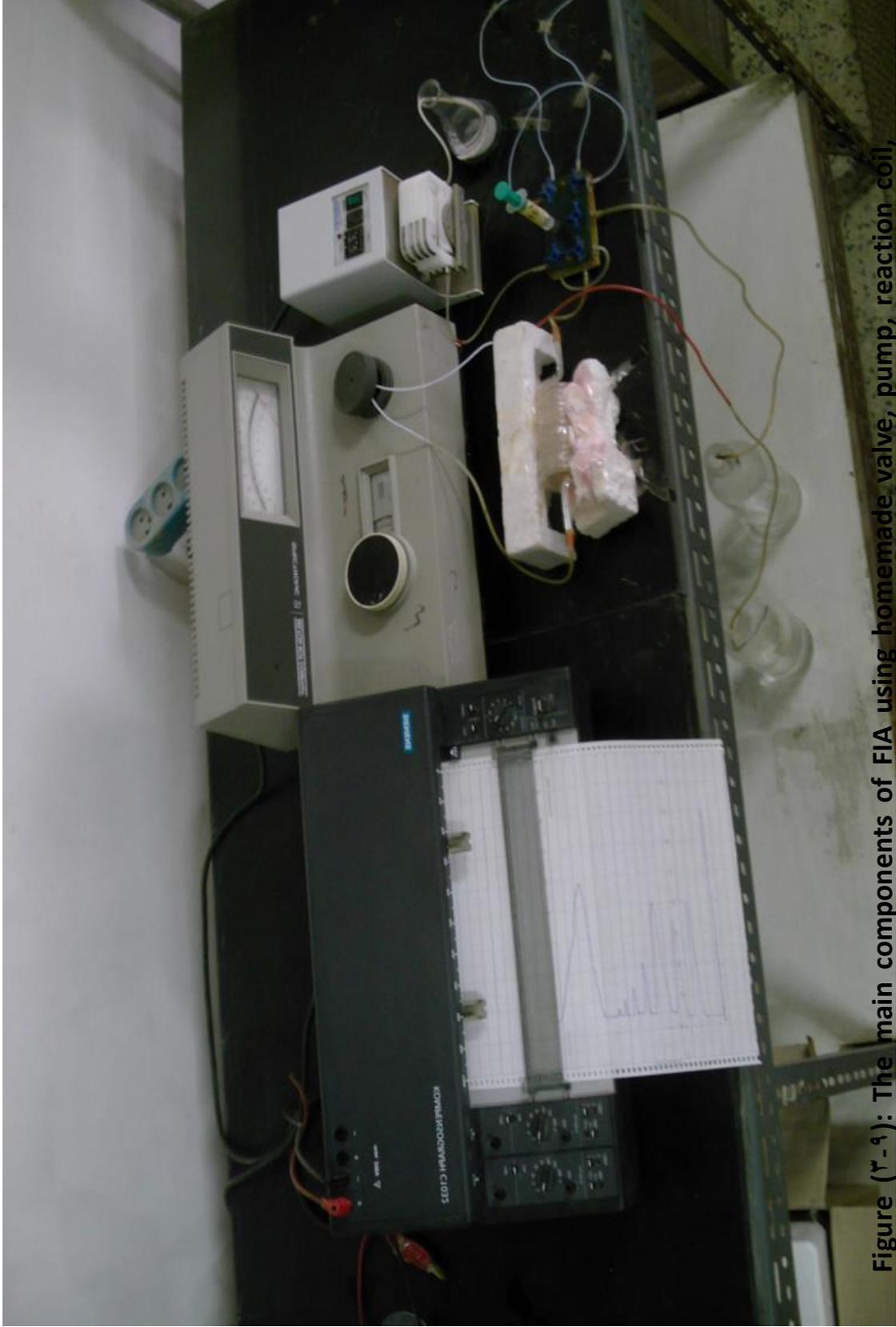


Figure (3-9): The main components of FIA using homemade valve, pump, reaction coil, homemade cell (1 cm), detector & recorder.

Eventually, the unit show in figure (3.9) was used to determine the chlorate ion and knowledge the degree of dispersion and detection limit of this method.

Fast and slow chart speed was used in order to notice any hidden shoulder in the profile (i.e pure release for one product or multi release or multi reaction product) as in figure (3-10).

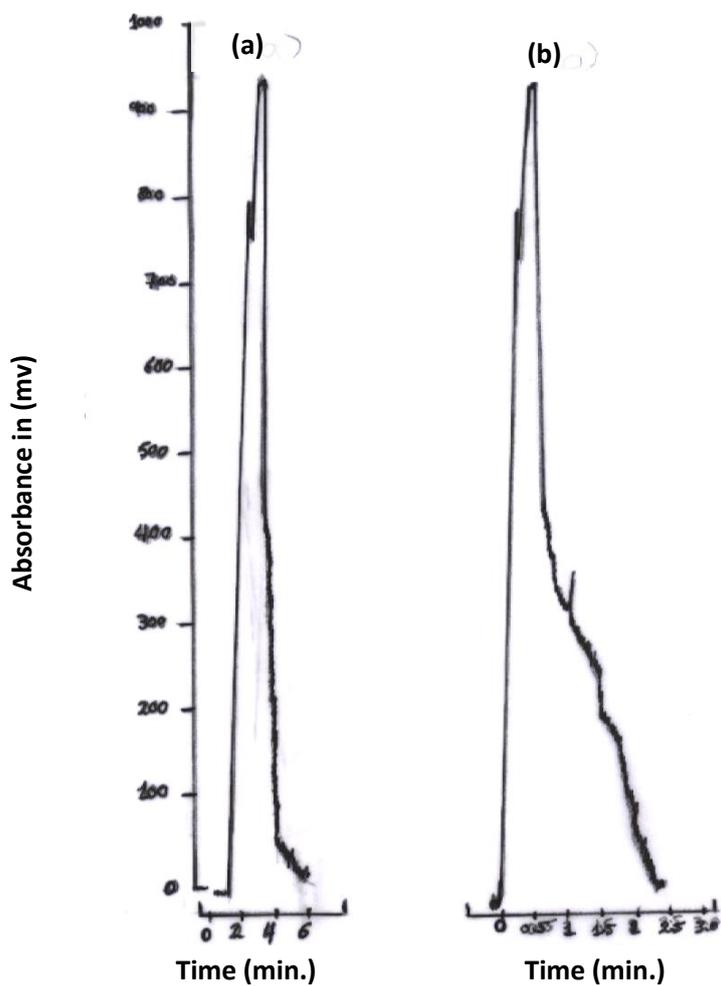


Figure (3-10): Absorbance time profile of the released I_2 using FIA

a: Fast chart speed (1 min.)

b- Slow chart speed (3 min.)

Part ((B))

3B - The components of the second unit:

This unit that is home made consists of three ways, the first way represents passing of sulphuric acid solution, while the second way passes reagent solution (potassium iodide) and the third way acts as transfer current for injected sample through an injection valve that has international design as shown in figure (3-11).

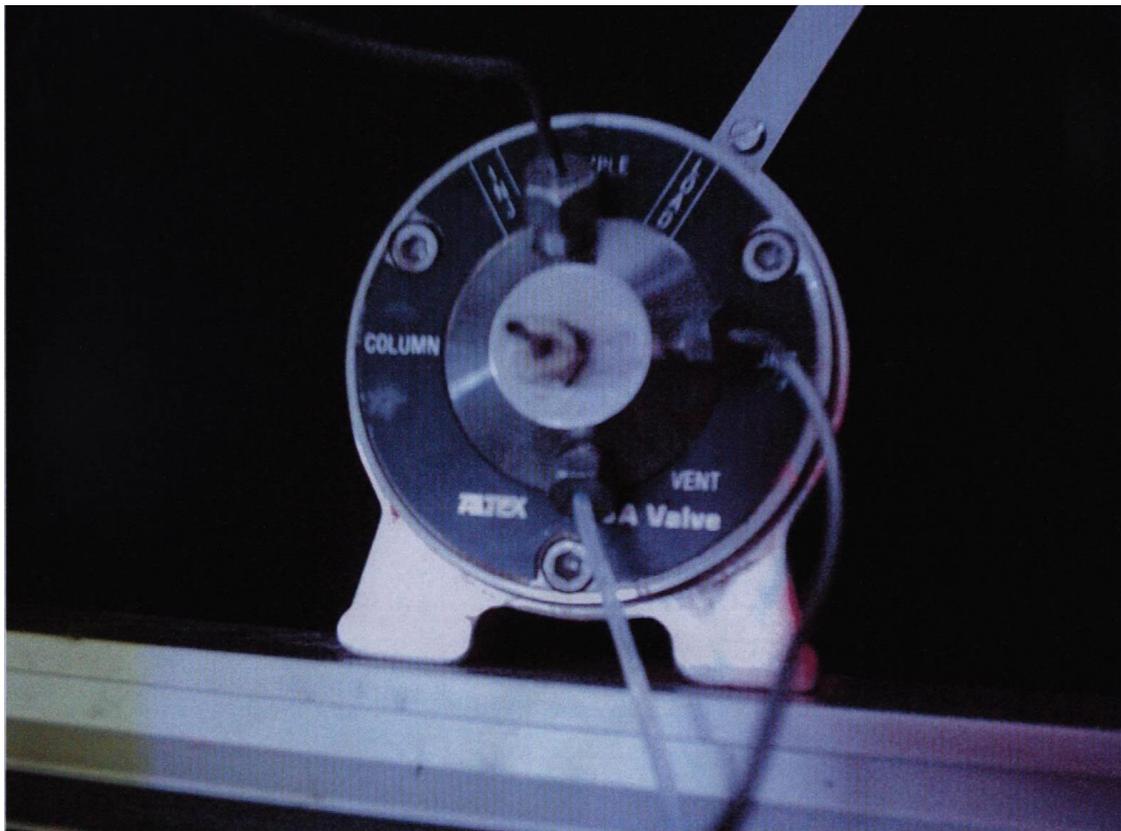


Figure (3-11): An injection valve

After passing acid and reagent solution through pump, figure (3-1), which is composed of many rates and from it we can choose the optimum rate for reaction ($\text{ClO}^- + \text{I}^- + \text{H}^+ \text{O}^+$).

Then acid and reagent solutions move toward primary mixing coil after merging out from primary mixing coil will meet transfer current of sample section that represents the third way of design unit. Now these components form the reaction and it mixes in secondary mixing coil and then to completion reaction coil that is made of Teflon whose length is (1.2 mm). Figure (3-12) indicates injection point.

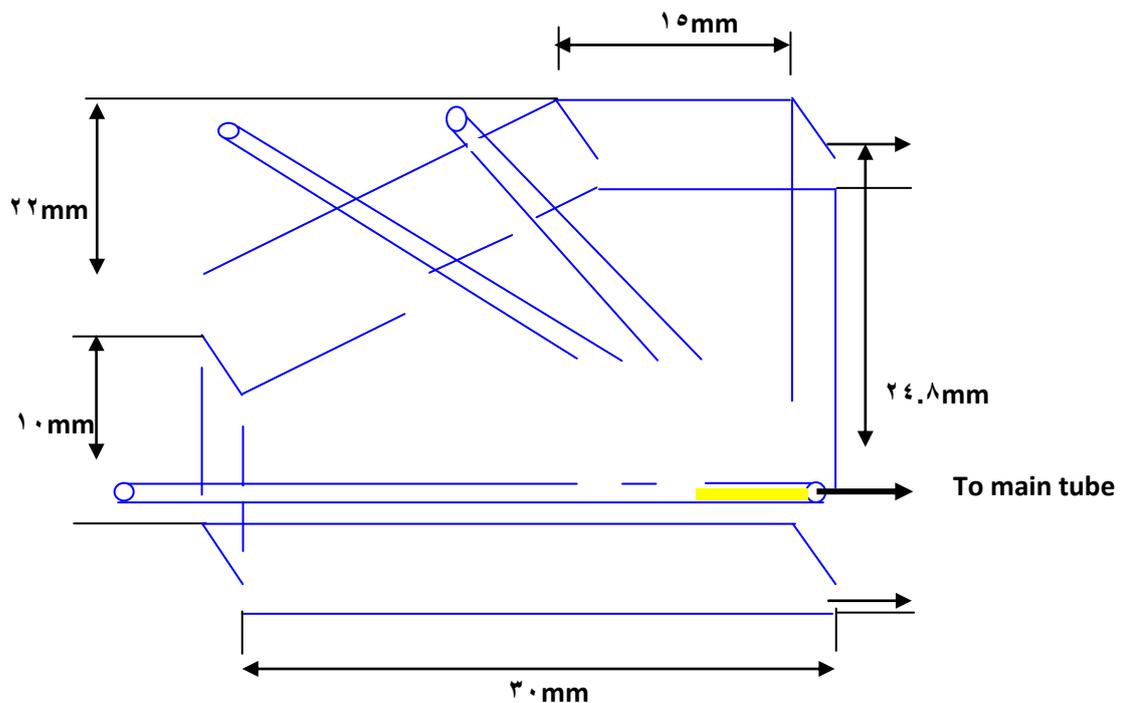
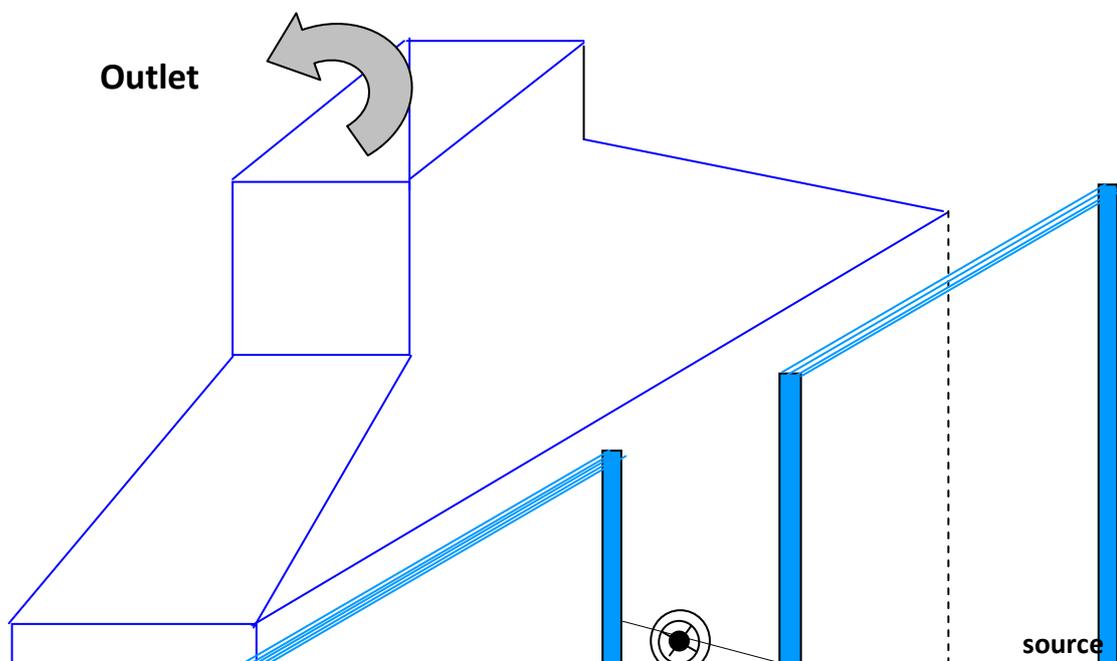


Figure (۳-۱۲): Schematic sketch indicating the dimension of the injection point

A homemade flow through cell made of quartz was used. Attached to one face a source (LED) blue, while the opposite side a photo silicone detector. Figure (۳-۱۳) shows a schematic represents this cell.



Sensitizer

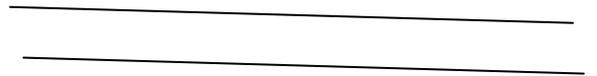


Figure (3-13): Reaction cell is larger than real cell by γ^2 time (path length γ mm)

The output signal from photo silicone detector (Psd) passes to an amplifier followed by a read out device in our case X-T-potentiometric recorder was used.

The following figures (3-14) and (3-15) show the schematic diagram and shape of style unit.

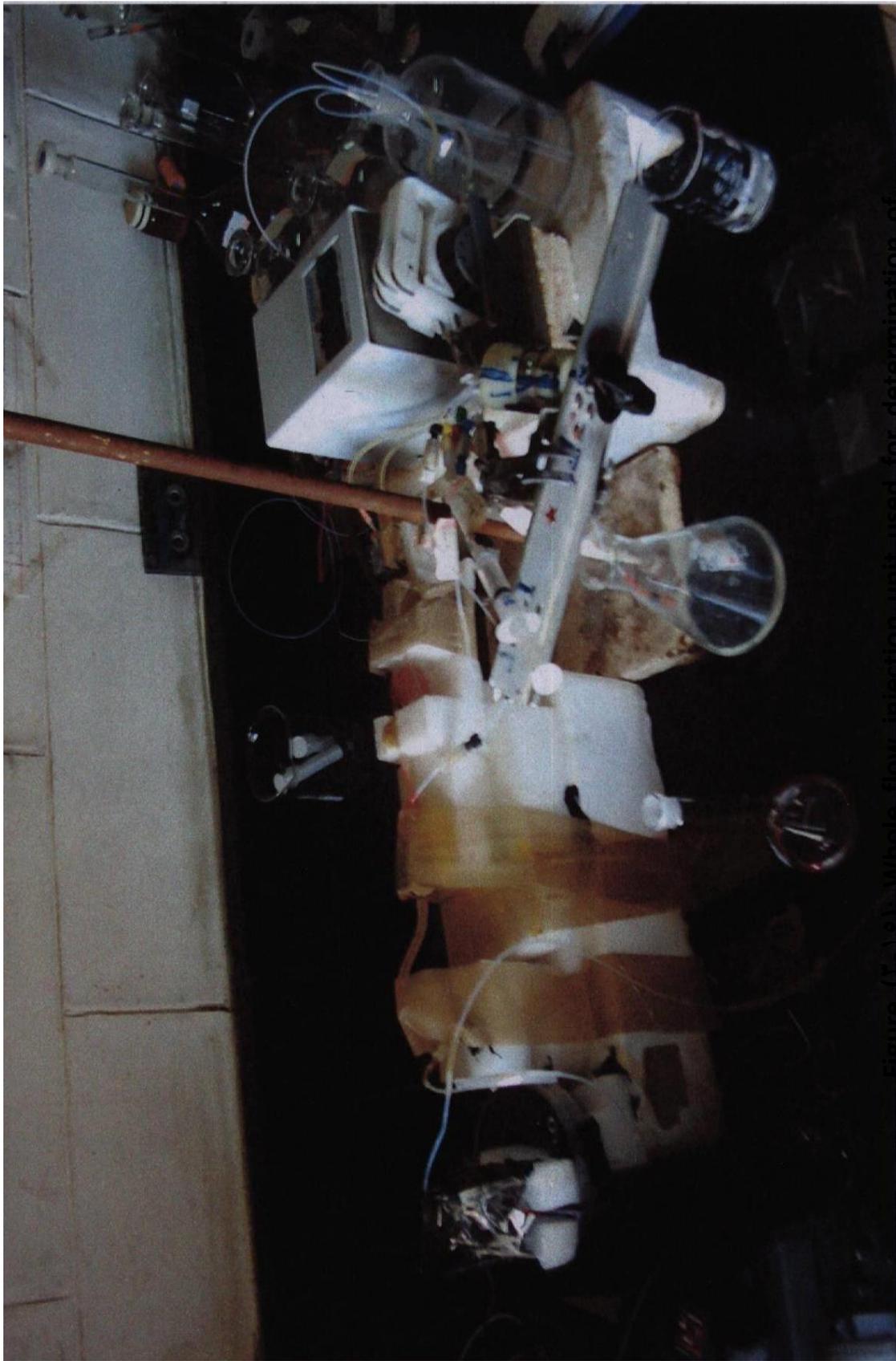


Figure (1.1.7): whole new injection unit used for determination of

chlorate ion.

Figure (3-14) shows a complete flow injection unit for the determination of released iodine for the chlorate ion determination. Electronic unit in determination, is also shown in figure (3-14).

Fast and slow chart speed was used in order to notice any hidden shoulder in the profile (i.e pure release for one product or multi release or multi reaction product as shown in figure (3-16)).

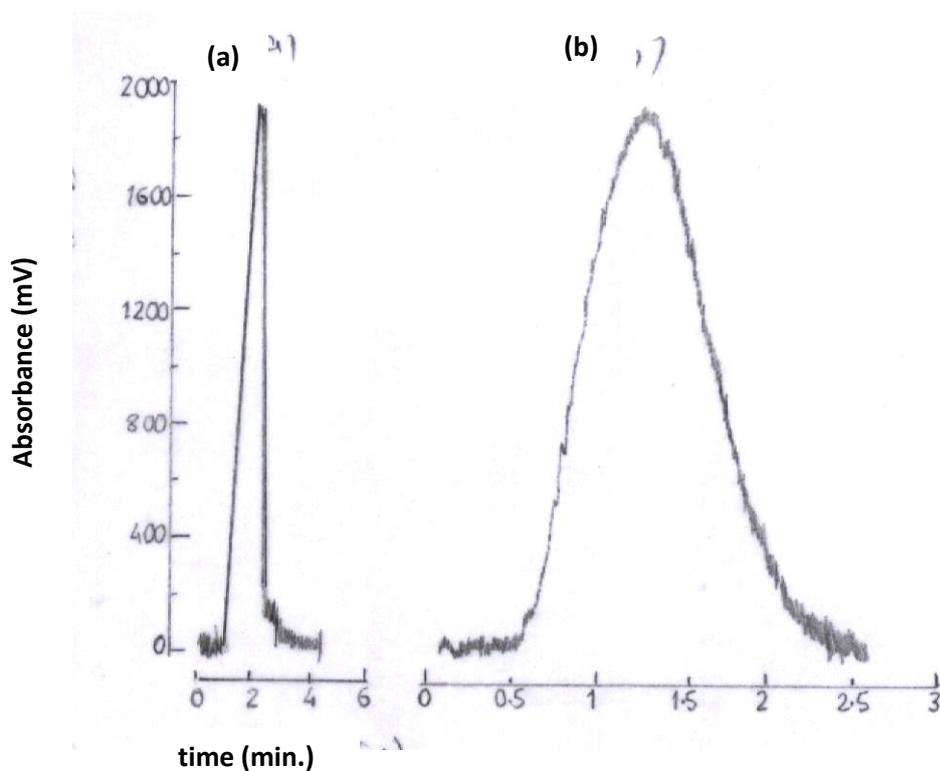


Figure (3-16) Absorbance time profile of signal obtained for the released iodine from chlorate determination.

a. Fast chart speed (4 min.)

b. Slow chart speed (2.0 min.)

Chapter Four

Results and Discussion

CHAPTER FOUR

This chapter is divided into two parts:

Part ((A)):

This part treats results, discussion and applications for unit used in part ((A)) of chapter three.

Part ((B)):

Part B deals with results, discussion and applications for the unit used in part ((B)) of chapter three.

Part ((A))

ξA-1: The study of the dispersion phenomenon in sample zone and comparison between FIA and SIA:

To measure the dispersion value in different sample zones of ($ξ1.0, ξ1.5, ξ1.7 μg.ml^{-1}$) chlorate ion, two experiments were carried out by using unit in figure (3-9).

In the first experiment after mixing of reactants ($ClO_3^- - I^- - H_2O^+$) and form iodine that passes through manifold unit giving continuous response of constant concentration for chlorate ion; this indicates non-existence of dispersion effect by convection or diffusion. This measurement represents (C_0). While the second experiment includes injecting different concentration of

($4170, 417.0, 41.70 \mu\text{g}\cdot\text{ml}^{-1}$) chlorate ion in the interior loop (L_1) and $31.4 \mu\text{l}$ of ($0.0 \text{ mol}\cdot\text{L}^{-1}$) potassium iodide (KI) in the exterior loop (L_2), by using of ($2.0 \text{ mol}\cdot\text{L}^{-1}$) hydrochloric acid (HCl) as a carrier stream. The obtained value from this experiment represents intensity response for sample injected (C_{max}) as shown in figure (4-1).

The equation used to calculate dispersion (D) is:

$$D = \frac{C_o}{C_{\text{max}}}$$

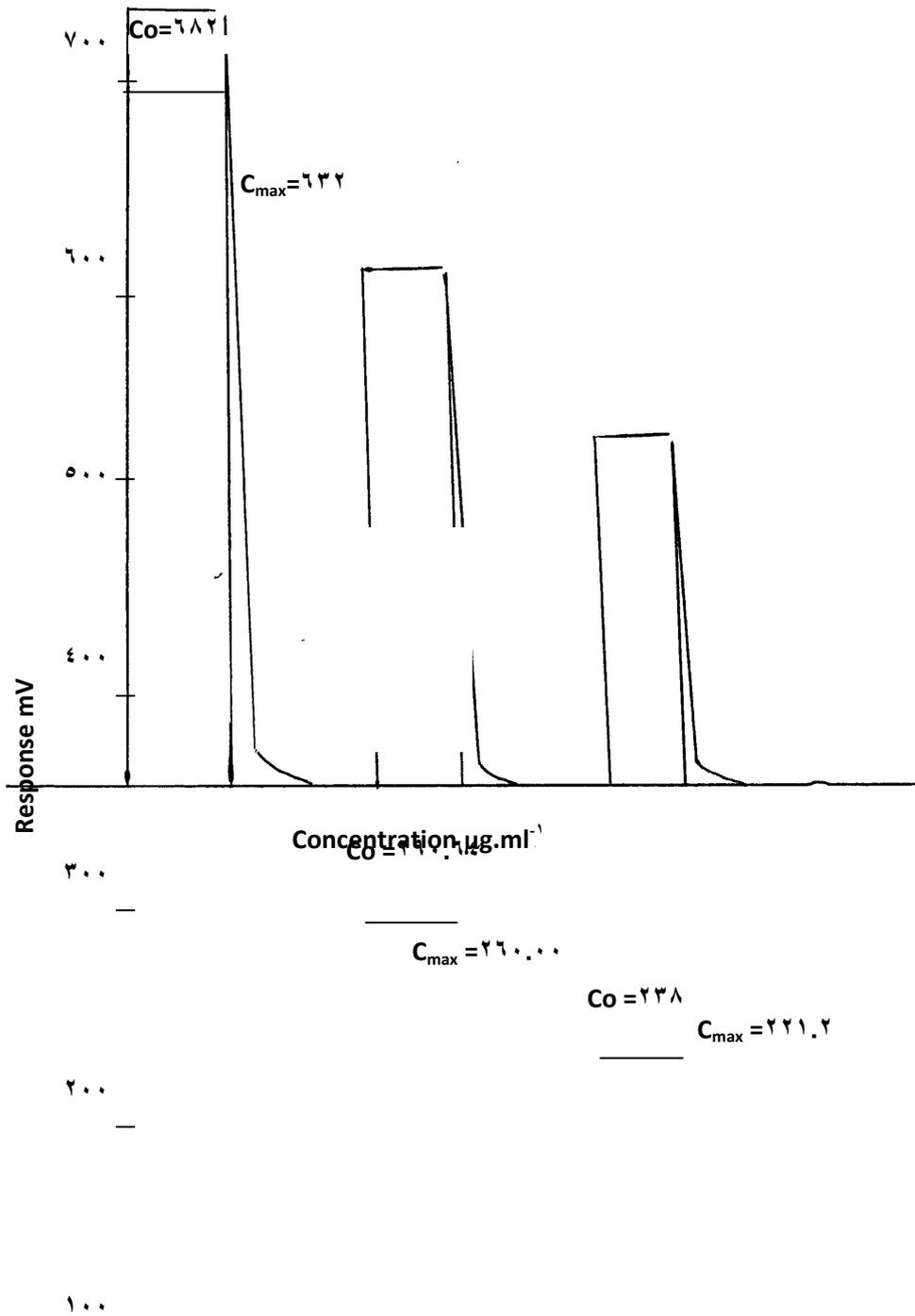
As in table (4-1), these values fall in limit state of dispersion.

Table (4-1): The dispersion of ($4170, 417.0, 41.70 \mu\text{g}\cdot\text{ml}^{-1}$) chlorate ion for system ($\text{ClO}_3^- - \text{I}^- - \text{H}^+ \text{O}^+$).

Chlorate ion concentration ($\mu\text{g}\cdot\text{ml}^{-1}$)	Response in (mV)		Dispersion (D) $D = \frac{C_o}{C_{\text{max}}}$
	C_o (mV)	C_{max} (mV)	
4170	682	632	1.0791

417.0	290.64	260	1.1178
41.70	238	221.2	1.0709

The optimum value obtained from dispersion of ($41.70 \mu\text{g.ml}^{-1}$) chlorate ion.



170

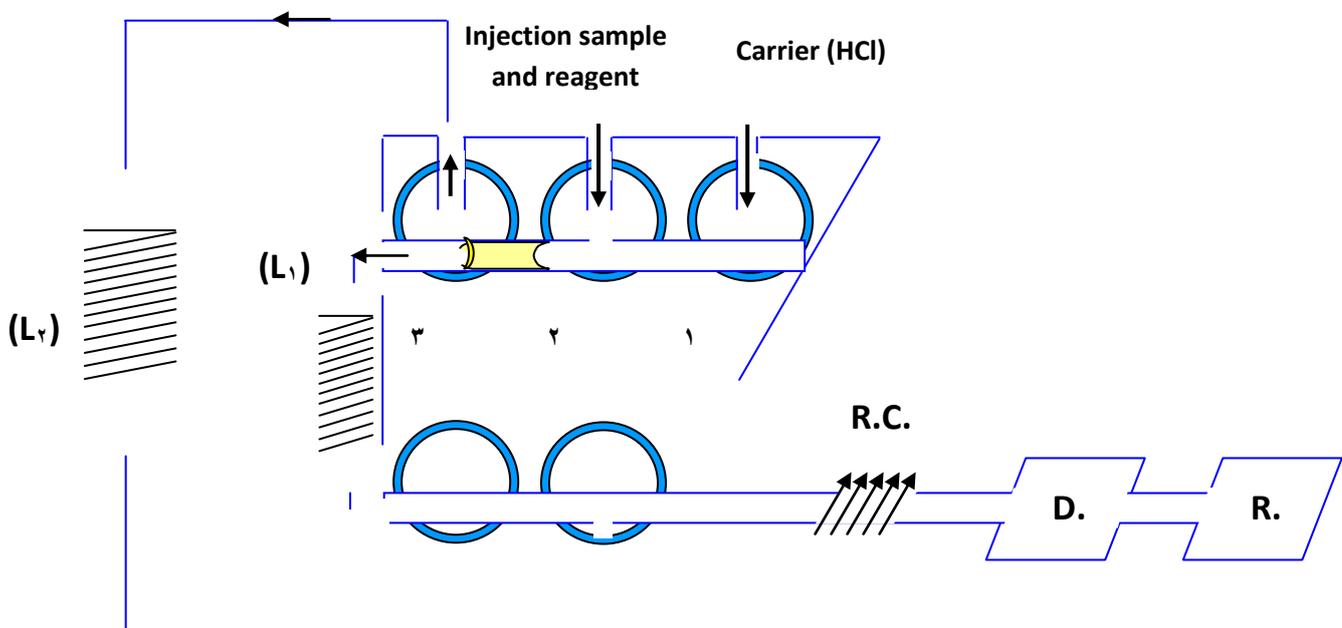
17.0

17.0

Figure (1) The dispersion of chlorate Ion using (170, 17.0, 17.0 $\mu\text{g}\cdot\text{ml}^{-1}$) in the system of $(\text{ClO}_3^- - \text{I}^- - \text{H}^+ \text{O}^+)$.

And the comparison between flow injection analysis and sequential injection analysis that can be noticed in the dispersion of the sample zone that is attained is shown in figures (2) and (3).

Figure (2 a, b, c) indicating new valve (Five three- ways valve) is homemade and injected (170, 17.0, 17.0 $\mu\text{g}\cdot\text{ml}^{-1}$) of chlorate ion and (0.0 M) of potassium iodide using (2.0 M) of hydrochloric acid as a carrier stream In figure (2 a,b) injected chlorate ion in (L1) and potassium iodide in (L2) and toward the arrow, while figure (2 c) shows pushing process the carrier (HCl) to sample and reagent and shape sample section.



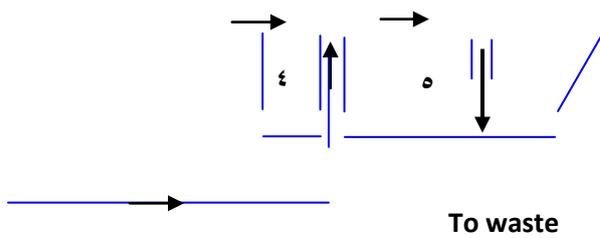
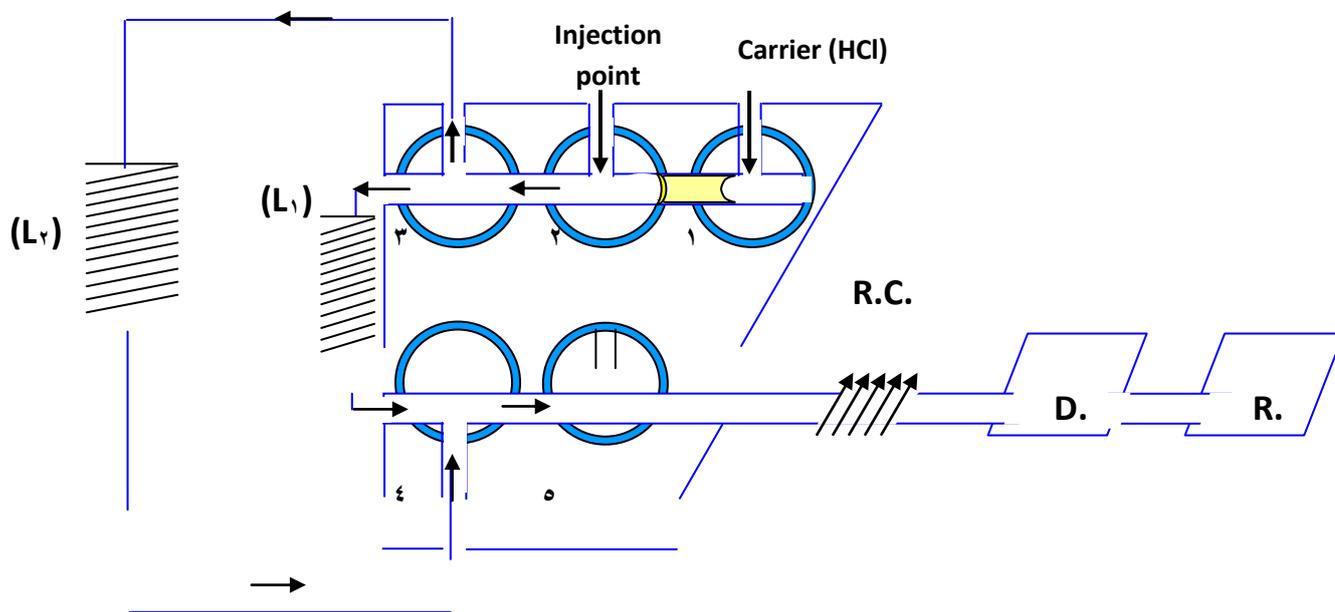


Figure (ξ - γ) (a): Injection samples and reagent



(ξ - γ) (b)

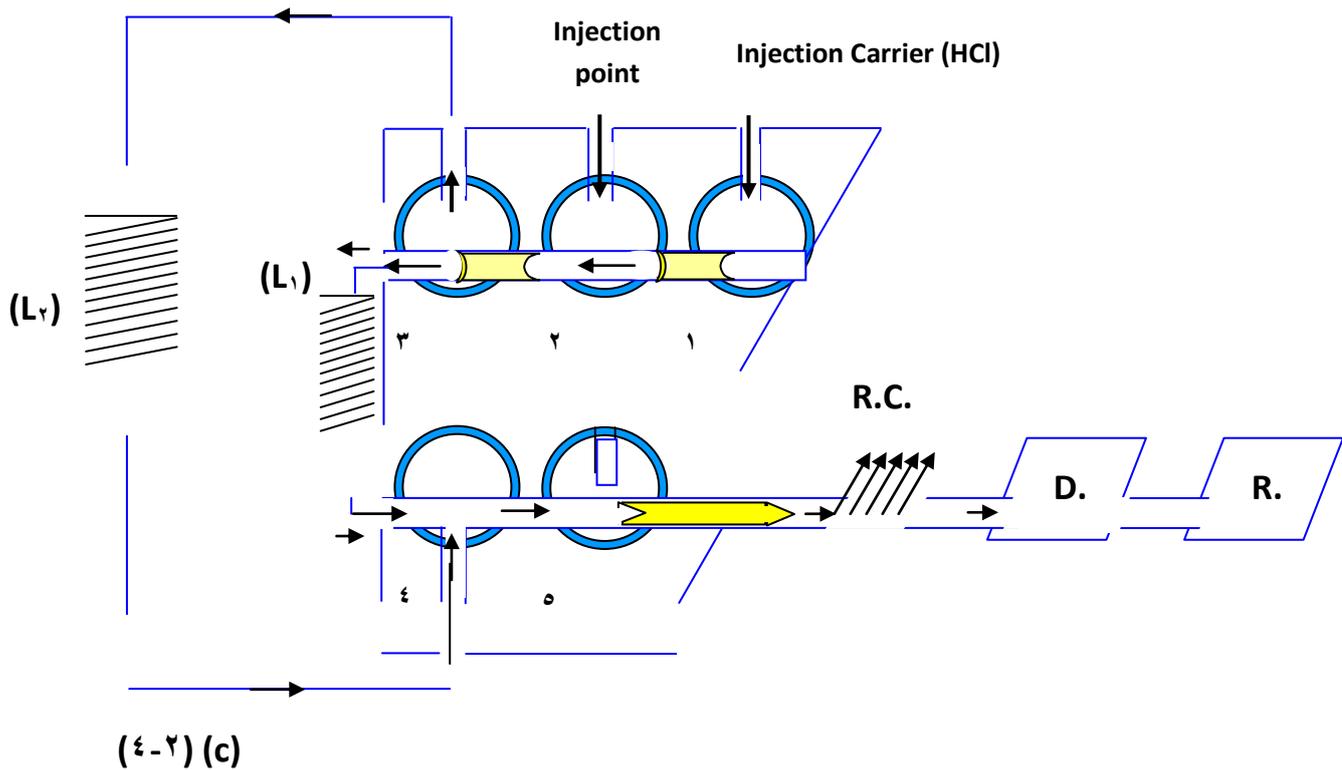


Figure (ξ-γ a,b,c): The dispersion of sample zone in FIA critically

where: a: Injection sample and reagent.

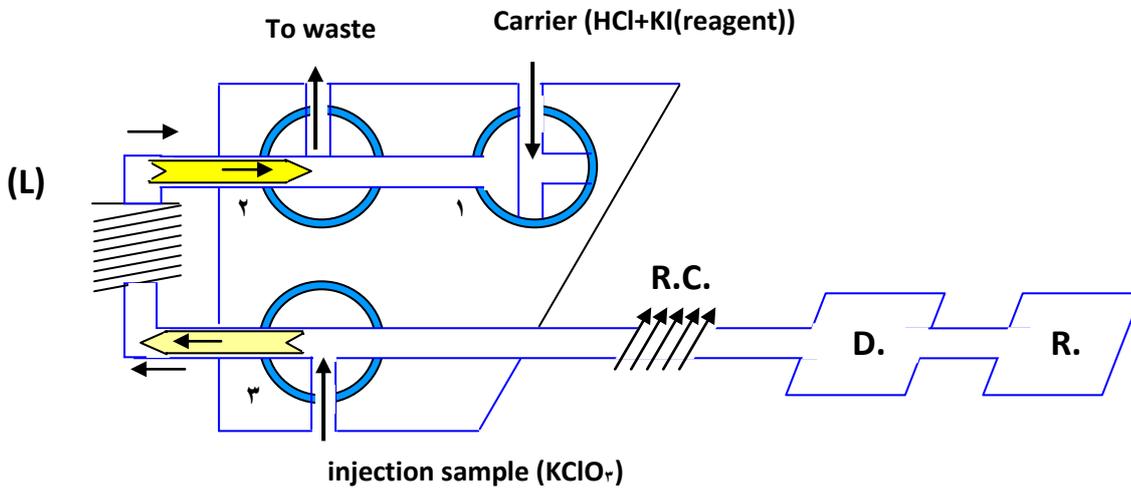
b- Injection carrier solution .

c- Dispersion of sample zone that attained in FIA.

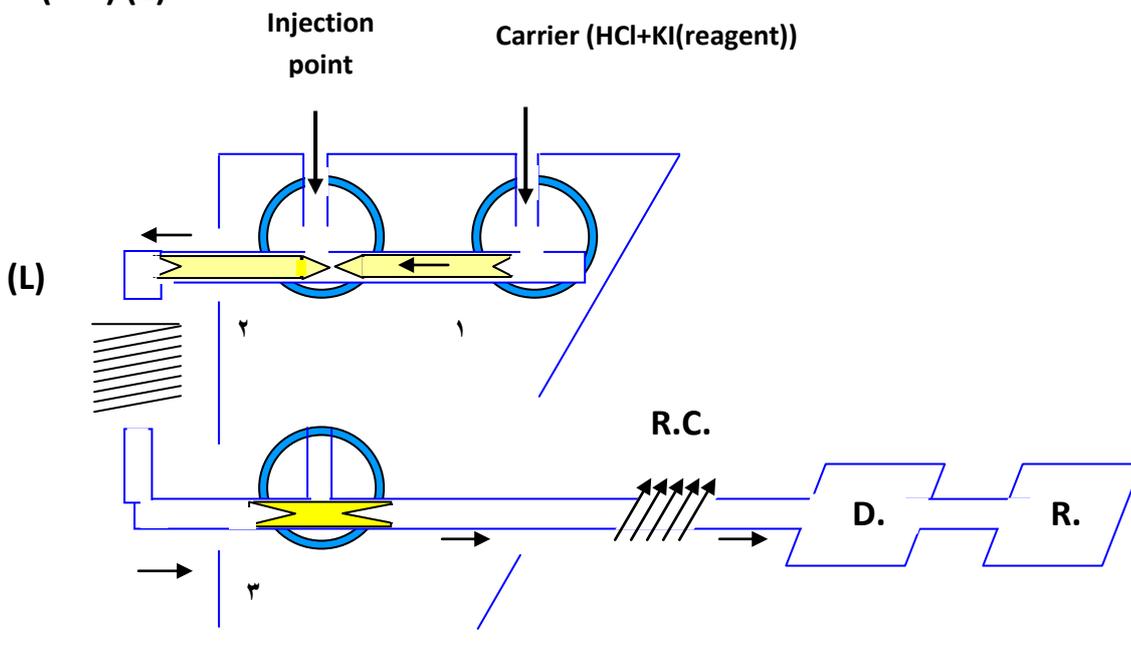
While figure (ξ-γ a, b) is three three-ways valve (homemade) injection (ξ1γ0, ξ1γ.0, ξ1.γ0 μg.ml⁻¹) of sample and (0.0 M) of potassium iodide (reagent) in opposite direction as in figure (ξ-γ a).

Whereas figure (ξ-γ b) indicates injection carrier to push the sample and reagent for other parts of unit and by this process noticed the shape of sample section that indicating the decreasing in dispersion.

Through these experiments in figures (ξ-ϒ a, b, c) and (ξ-ϓ a, b) we noticed the value of absorbance for released iodine to system ($\text{ClO}_2^- - \text{I}^- - \text{H}_2\text{O}^+$) at 350 nm, as in table (ξ-ϒ).



(ξ-ϓ) (a)



(ξ-ϓ) (b)

Figure (4-3 a,b): dispersion of sample zone in SIA practically

where: a: Injection sample.

b- Injection carrier solution in SIA

Figure (4-4), shows the comparison between FIA and SIA in dispersion of sample zone theoretically.

And table (4-1) shows the difference between FIA and SIA practically.

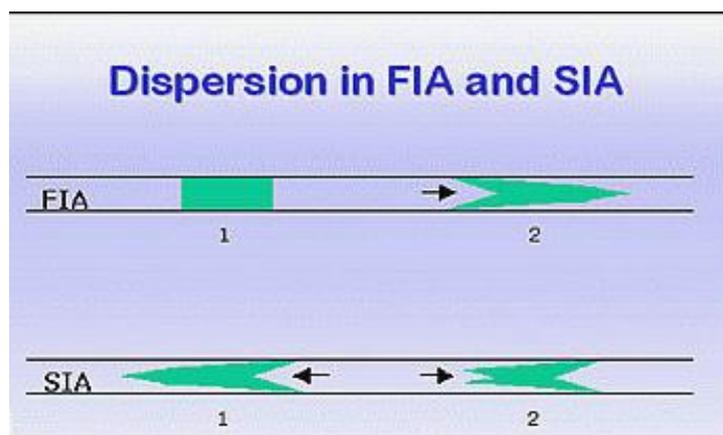


Figure (4-4): Comparison between FIA and SIA theoretically.

Table (4-2): The difference in absorbance of iodine between FIA and SIA practically using (0.01 M) of HCl and (0.01 M) of KI at 350 nm.

Conc. Of ClO_2^- $\mu\text{g}\cdot\text{ml}^{-1}$	Absorbance (FIA)	Absorbance (SIA)
--	------------------	------------------

	mV	mV
٤١٧.٥	٢٦٠, ٢٦٠, ٢٦٠	٧٠٠, ٧٠٠, ٧٠٠
٤١٧٥	٦٣٢, ٦٣٢, ٦٣٢	٨٨٠, ٨٨٠, ٨٨٠

٤A-٢: Physical parameters:

٤A-٢-١: Effect of flow-rate:

Flow-rate is studied by using different flow rates extends from (١.٣-٥.٥ ml.min⁻¹) using (١٢٧ μl) of (٠.٠٥ M) of chlorate ion and (٣١.٤ μl) of (٠.٥ M) of potassium iodide and (٢.٠ M) of hydrochloric acid.

Table (٤-٣) and figure (٤-٥) show that ١.٩٥ ml.min⁻¹ is the optimum flow-rate to obtain the best absorbance.

Table (٤-٣): Variation of absorbance of released iodine expressed as average peak height (mV) versus flow rate at constant concentration of potassium iodide (٠.٥ M), concentration of acid (٢.٠ M) and chlorate ion (٠.٠٥M).

Flow-rate ml.min ⁻¹	Absorbance (mV)			\bar{Y}	SD	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
١.٣٠	٥٢٤	٥٢٤	٥٢٤	٥٢٤	.	.	٥٢٤

1.90	068	068	068	068	.	.	068
2.00	008	008	008	008	.	.	008
3.00	448	448	448	448	.	.	448
3.30	424	424	424	424	.	.	424
3.90	360	360	360	360	.	.	360
4.60	304	304	304	304	.	.	304
0.00	288	288	288	288	.	.	288

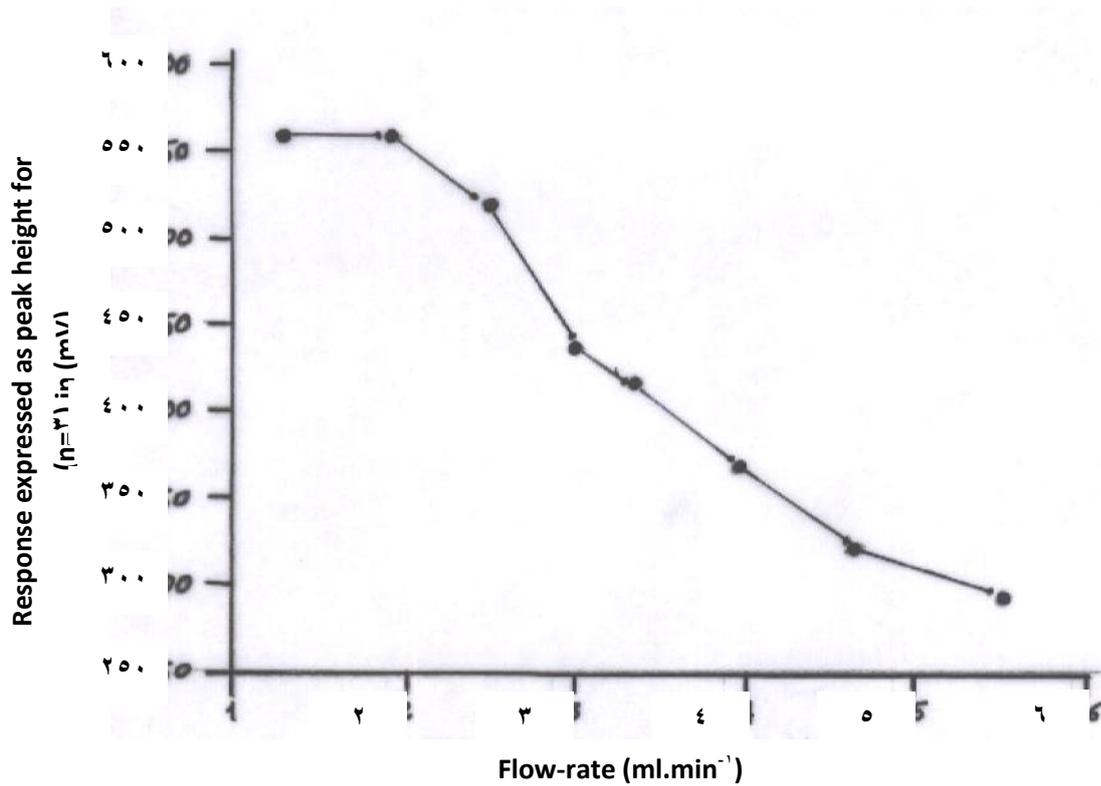


Figure (4-0): The effect of flow rate

ξ A-۲-۲: The effect of reagent volume (KI):

A set of injected volumes of potassium iodide ranging from (۱۰.۷۱-۰۰.۰۰ μl) by changing the length of iodide loop (L_1) were evaluated using (۱۲۷ μl) of (۰.۰۰ M) of chlorate ion, (۲.۰ M) of hydrochloric acid as a main carrier stream and flow-rate (۱.۹۰ ml.min⁻¹). Figure (ξ-۶) and table (ξ-ξ) show the variation of absorbance of released iodine expressed as peak height in (mV) (average of three measurements) versus the reagent volume. A reagent volume of (۳۱.۴ μl) is chosen as the optimum value.

Table (ξ-ξ):The effect of reagent volume KI on the reaction ($\text{ClO}_3^- + \text{I}^- + \text{H}^+ \rightarrow \text{O}^+$) used in determination of chlorate ion.

Volume of reagent (μl)	Absorbance (I_r) (mV)			\bar{Y}	SD	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
۱۰.۷۱	۶۱۸.۰	۶۱۸.۰	۶۱۸.۰	۶۱۸.۰	.	.	۶۱۸.۰
۲۳.۰۶	۶۱۶.۰	۶۱۴.۰	۶۰۰.۰	۶۱۰.۰	۸.۷۱۷	۱.۴۲۹	۶۱۰.۰ ± ۲۱.۶۰۶
۳۱.۴۰	۶۲۲.۴	۶۲۴.۰	۶۲۴.۰	۶۲۳.۴	۰.۹۲۳	۰.۱۴۸	۶۲۳.۴ ± ۲.۲۹۳
۳۹.۲۰	۰۴۲.۰	۰۴۰.۰	۰۴۰.۰	۰۴۰.۶	۱.۱۰۴	۰.۲۱۳	۰۴۰.۶ ± ۲.۸۶۷
۰۰.۰۰	۰۷۲.۰	۰۷۲.۰	۰۷۲.۸	۰۷۲.۲	۰.۴۶۱	۰.۰۸۰	۰۷۲.۲ ± ۱.۱۴۰

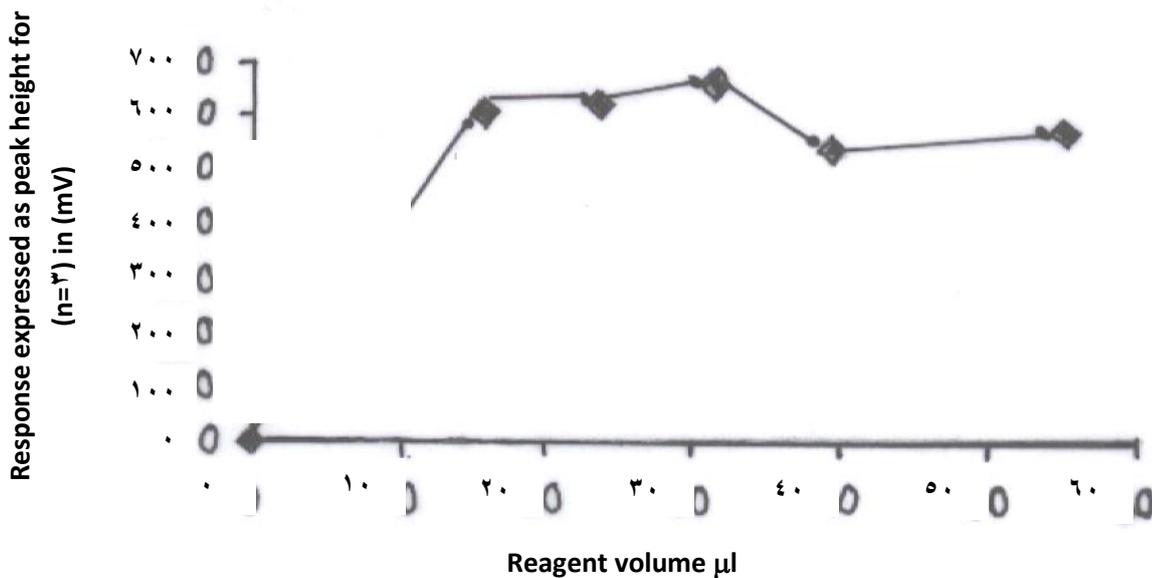


Figure (4-6): Effect of reagent volume (KI)

4A-2-3 Effect of sample volume:

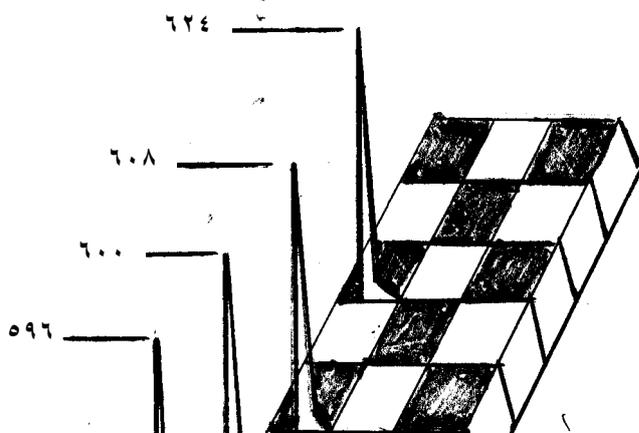
The effect of sample volume is examined in the range from (36.4-127.0 μl) by changing the lengths of sample loop (1) using (0.00M) of chlorate ion, (31.4 μl) of (0.0 M) of potassium iodide, (2.0 M) of hydrochloric acid as a carrier stream and flow-rate (1.90 ml.min⁻¹).

Table (4-5) and figure (4-7) show the variation of absorbance of released iodine expressed as peak height in (mV) (n=3) versus the sample volume.

(127 μ l) of chlorate ion is chosen as an optimum volume, while at increasing the volume larger than (127 μ l) will decrease in intensity of response.

Table (4-5): The effect of sample volume KClO₃ in determination of chlorate ion.

Volume of sample (μ l)	Absorbance (I _v) (mV)			\bar{Y}	SD	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
37.4	092	092	091.2	091.7	0.019	0.087	091.7 \pm 1.289
54.6	096	090.6	098	096.0	1.280	0.210	096.0 \pm 3.192
72.8	700	700	700	700.0	0.000	0.000	700
91.0	708	708	708	708.0	0.000	0.000	708
127.0	724	723.2	724	723.7	0.471	0.074	723.7 \pm 1.140



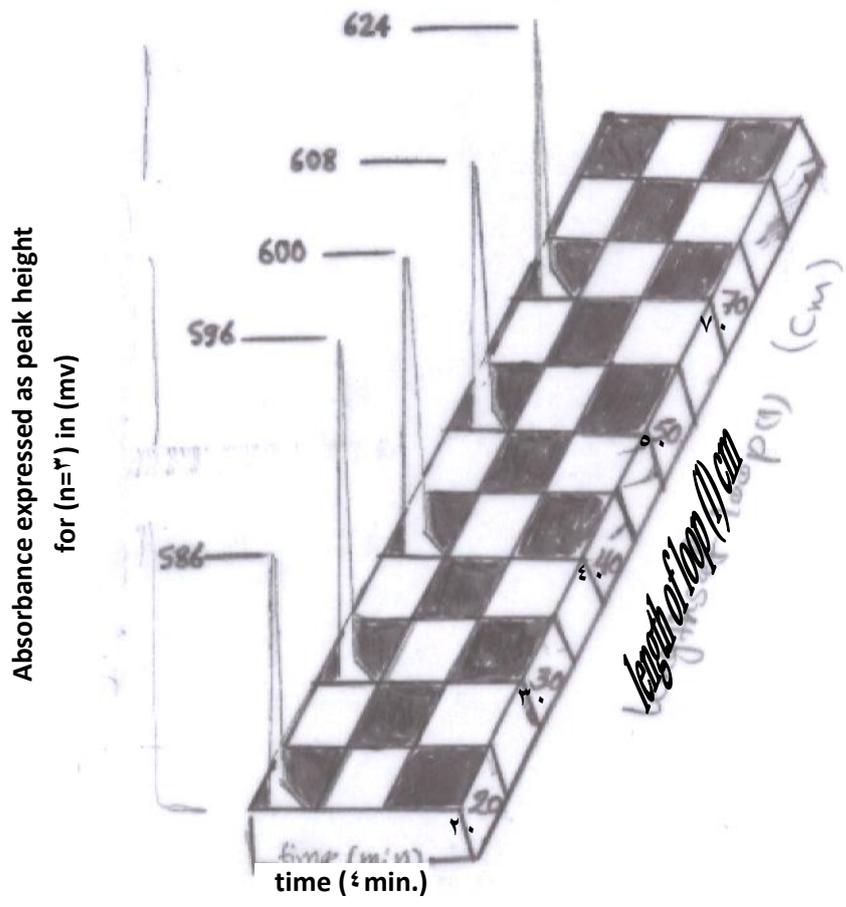


Figure (4-V): The effect of ClO_2^- volume concentration

ξ A-γ-ξ: Effect of interior loop shape:

Interior loop represents loop (1) for chlorate ion (ClO_3^-); in this experiment loop (1) is used as a helix shape and other time is linear shape, and shows the difference between the two peaks that were obtained in both cases.

Table (ξ-6) and figures (ξ-8) and (ξ-9) show the difference in the absorbance by using the different shape.

From this experiment, linear loop (1) is more important than helix loop (1), because the linear shape gives a nice narrow peak with higher response and without shoulder, figure (ξ-9) shows the shape of the loop.

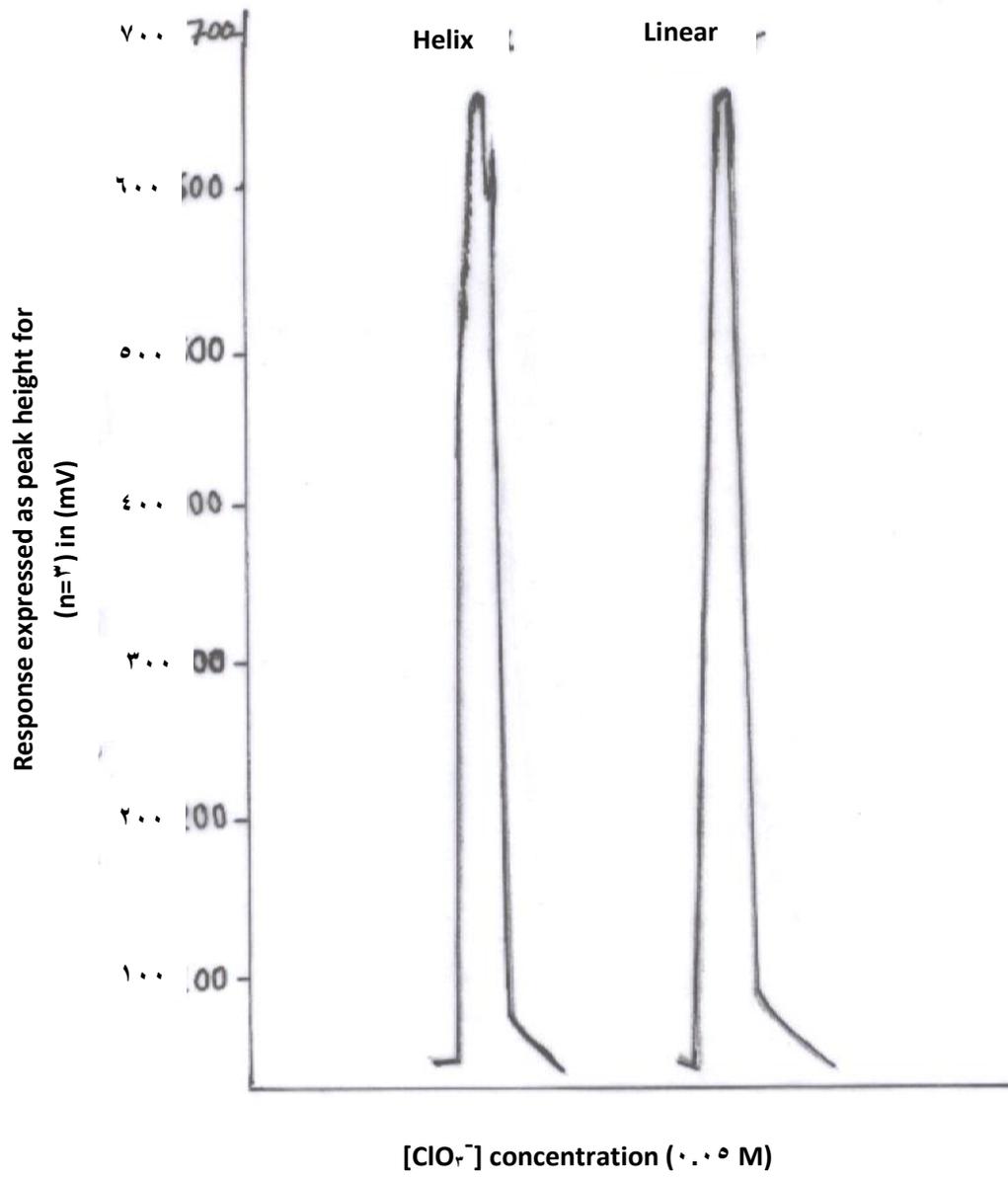


Figure (4-8): The difference in response between linear and helix loop(1)

Table (٤-٦): Variation of absorbance of released iodine at ($\lambda=350$ nm) expressed as average peak height (mV) versus the shape of loop (λ) at concentration of sample (1.1×10^{-3} M), carrier [HCl] (2×10^{-2} M) and reagent KI (1×10^{-2} M) and flow rate (1.9 ml.min^{-1}).

Shape of loop (λ)	Absorbance (I_r) in (mV)			\bar{Y}	SD	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
	٦٠٠	٦٠٨.٠	٦٠٦.٠				
Helix	٦٠٠	٦٠٨.٠	٦٠٦.٠	٦٠٤.٦	٤.١٦٣	٠.٦٨٨	٦٠٤.٦ \pm ١٠.٣٤٢
Linear	٦٢٠	٦١٩.٦	٦٢٠.٠	٦١٩.٨	٠.٢٣٠	٠.٠٣٧	٦١٩.٨ \pm ٠.٥٧١

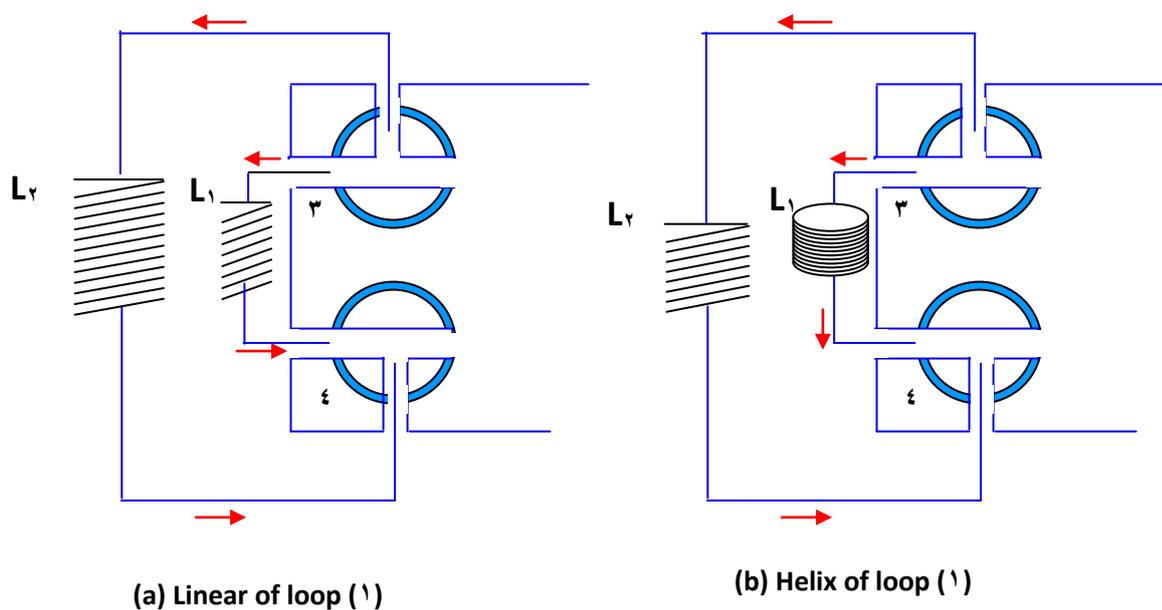


Figure (4-9): The difference in shape of loop (1)

a- Linear shape

b- Helix shape

4A-2-9: Effect of reaction coil length

By changing the reaction coil length from (0.200 cm), it has been shown that the sensitivity of the method for the determination chlorate ion increases with the increase of length of the reaction coil by using (0.001M) of chlorate ion, (0.01 M) of potassium iodide, (0.01 M) of hydrochloric acid and flow rate (1.00 ml.min⁻¹); this was due to the long residence time resulting from the increase in the reaction yield that was up to (1.00 cm), increase and base width of response will increase too due to the dispersion from the results.

Table (4-10) and figure (4-11) show the absorbance in (mV) versus reaction coil length (cm).

(1.00 cm) length is selected for reaction coil as an optimum length.

Table (4-10): The effect of reaction coil length on the released iodine in the determination of chlorate ion

Length of coil (cm)	Absorbance (I _r) (mV)	\bar{Y}	SD	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
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Figure (4-10): The effect of the reaction coil length

4A-2-6: Effect of temperature

The reaction of (0.001 M) potassium iodide and (0.001 M) of hydrochloric acid as a carrier stream with ($100 \mu\text{l}$) of (0.001 M) chlorate ion is done in different temperature by use optimum condition obtained previously former. It was

found that there was no effect of temperature between (20-50 °C) on the reaction, as shown in table (4-8).

Table (4-8): The effect of temperature on the absorbance of iodine released in the reaction system ($\text{ClO}_2^- - \text{I}^- - \text{H}^+ \text{O}^+$).

Temperature °C	Absorbance (I _v) (mV)			\bar{Y}	SD	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
20	328.0	328.0	327.6	327.86	0.23	0.07	327.86 ± 0.051
30	327.6	327.6	328.0	327.73	0.23	0.07	327.73 ± 0.051
40	328.4	328.0	328.0	328.13	0.23	0.07	328.13 ± 0.053
50	328.0	327.6	328.0	327.86	0.23	0.07	327.86 ± 0.053

ξ A-ϳ: Chemical parameters:

ξ A-ϳ-ϱ: Influence of acid concentration

Variable acid concentrations ($1.0-2.0$ M) are used in the reaction of (0.005 M) chlorate ion with (0.01 M) of potassium iodide and flow rate (1.00 ml.min⁻¹) to release the iodine which is measured at 350 nm.

The results showed that the concentration of iodine generated increase swiftly with acid concentration up to (2.0 M) and the absorbance will be constant when the concentration is larger than (2.0 M).

(2.0 M) of acid is selected for this study. Table (ξ-9) and figure (ξ-11) show the variation of absorbance of released iodine expressed as average peak height in (mV) versus the concentration of (HCl).

Table (٤-٩): The effect of hydrochloric acid concentration on the peak height in the reaction of (ClO_٢⁻-I⁻-H_٢O⁺).

Conc. of HCl (mol.L ⁻¹)	Absorbance I _٢ (mV)			\bar{Y}	SD	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
١.٠٠	٢٢٠	٢٢٨	٢٢٦	٢٢٤.٦٦	٤.١٦٣	١.٠٨٣	٢٢٤.٦٦ ± ١.٢٤٣
١.٥٠	٣١٢	٣١٠	٣١٤	٣١٢.٠٠	٢.٠٠٠	٠.٦٤١	٣١٢.٠٠ ± ٤.٩٦٨
٢.٠٠	٤٨٠	٤٨٦	٤٨٤	٤٨٣.٣٣	٣.٠٥٥	٠.٦٣٢	٤٨٣.٣٣ ± ٧.٥٨٩
٢.٢٥	٥٩٨	٥٩٨	٥٩٨	٥٩٨.٠٠	٠.٠٠٠	٠.٠٠٠	٥٩٨
٢.٥٠	٦٠٤	٦٠٦	٦٠٤	٦٠٤.٦٦	١.١٥٤	٠.١٩٠	٦٠٤.٦٦ ± ٢.٨٦٨

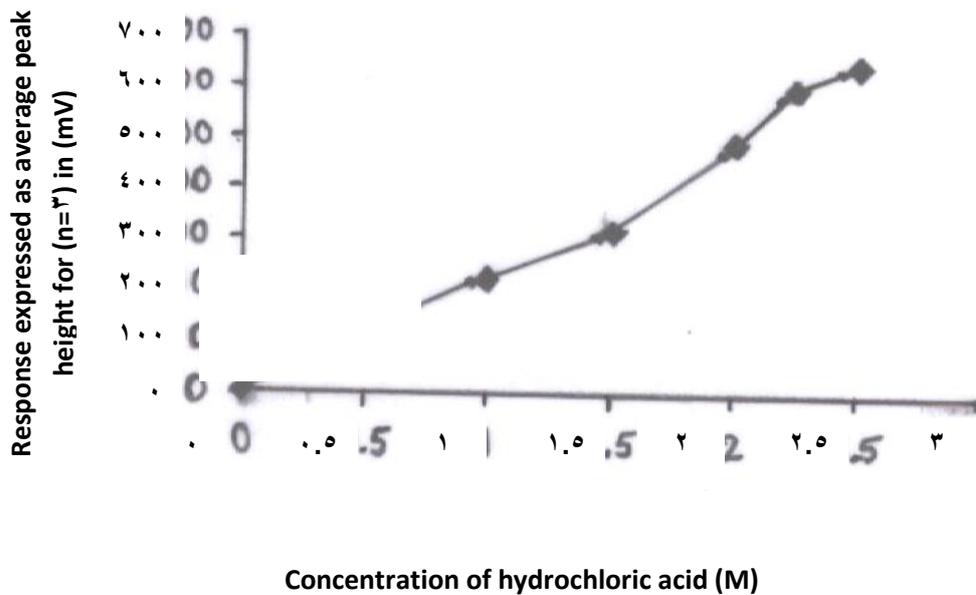


Figure (4-11) Effect of hydrochloric acid concentration

4A-3-2: The effect of potassium iodide concentration

The effect of potassium iodide concentration for absorption measurements is studied in the range of (0.020-0.620 M) that can be used in the second loop (31.4 μ l).

By using (127 μ l) of (0.00M) chlorate ion, (2.0 M) of hydrochloric acid is used as a carrier stream and flow-rate(1.90 ml.min⁻¹).

Figure (4-12) shows the variation of absorbance expressed as average peak height (n=3) in mV versus the molar concentration of potassium iodide solution.

The results showed that by increasing potassium iodide concentration up to (0.0 M) the absorbance of the released iodine increased, and at higher than the value is decreased.

(0.0 M) of potassium iodide concentration is selected for the further study and the results are shown in the table (4-10).

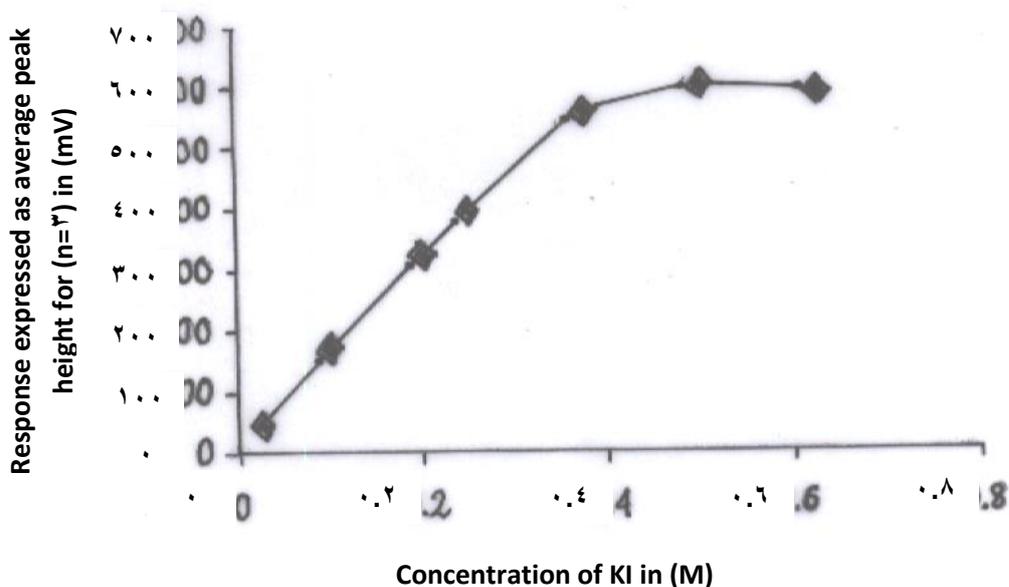


Figure (4-12) Effect of potassium iodide concentration

Table (4-10): The effect of potassium iodide concentration on the system (ClO₃⁻-I⁻-H₂O⁺) used in determination of chlorate ion.

Conc. of KI (mol.L ⁻¹)	Absorbance (mV)			\bar{Y}	SD	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
0.020	44.4	44.0	44.0	44.13	0.230	0.523	44.13 ± 0.071

٠.١٠٠	١٦٨.٠	١٦٨.٠	١٦٤.٠	١٦٦.٦٦	٠.٣٠٩	١.٣٨٥	١٦٦.٦٦ ± ٠.٧٦٧
٠.٢٠٠	٣٢٤.٠	٣٢٦.٠	٣٢٢.٠	٣٢٤.٠٠	٢.٠٠٠	٠.٦١٧	٣٢٤ ± ٤.٩٦٨
٠.٢٥٠	٣٩٢.٠	٤٠٠.٠	٣٩٤.٠	٣٩٥.٣٣	٤.١٦٣	١.٠٥٣	٣٩٥.٣٣ ± ١.٣٤٣
٠.٣٧٥	٥٥٦.٠	٥٥٨.٠	٥٥٦.٠	٥٥٦.٦٦	١.١٥٤	٠.٢٠٧	٥٥٦.٦٦ ± ٢.٨٦٨
٠.٥٠٠	٦٠٠.٠	٦٠٠.٠	٦٠٠.٠	٦٠٠.٠٠	٠.٠٠٠	٠.٠٠٠	٦٠٠
٠.٦٢٥	٥٨٥.٦	٥٨٥.٠	٥٨٥.٠	٥٨٥.٨٠	٠.٢٣٠	٠.٠٣٩	٥٨٥.٨ ± ٠.٥٧١

ξ A-ξ : Calibration graph:

A series of potassium chlorate solutions of the range ($0.00830-4170 \mu\text{g.ml}^{-1}$) were prepared from stock solutions under the optimum conditions of reagent and manifold variables, by repeating the measurement of each concentration three times as indicated in table (4-11).

The typical detector response for iodine is shown in figure (4-13). The treatment of the results in linear regression terms is shown in table (4-12).

Table (٤-١١): Results of Changing the response with concentration

[ClO ₂ ⁻] ppm	Response for n=٣ \bar{y} in (mV)	σ_{n-1} %RSD	$\bar{y} \pm t_{0.05} \frac{\sigma_{n-1}}{\sqrt{n}}$	\hat{y} predicted in (mV)
.	.	.	.	٥٥.٥٨
٠.٠٠٨٣٥	٢٠.٨	.	٢٠.٨	٢١٣.٨١
٠.٠٠٤	٢٠.٩.٣	٢.٣٠٩ ١.١٠٣	٢٠.٩.٣±٥.٧٣٦	٢١٣.٨٢
٠.٠٠٨	٢١٢	.	٢١٢	٢١٣.٨٣
٠.٠٤٢	٢١٣.٤	٢.٣٠٩ ١.٠٨٢	٢١٣.٤±٥.٧٣٦	٢١٣.٨٧
٠.٠٨٤	٢١٤.٦	٢.٣٠٩ ١.٠٧٥	٢١٤.٦±٥.٧٣٦	٢١٣.٩١
٤.١٨	٢١٥.٣	١.١٥٤ ٠.٥٣٦	٢١٥.٣±٢.٨٦٧	٢١٤.٢٤
٨.٣٥	٢١٦	.	٢١٦	٢١٤.٦٦
١٦.٧	٢١٧.٣	٢.٣٠٩ ١.٠٦٢	٢١٧.٣±٥.٧٣٦	٢١٥.٥
٤١.٧٥	٢٢٠	.	٢٢٠	٢١٨.٠١
٦٦.٨	٢٢١.٣	٢.٣٠٩ ١.٠٤٣	٢٢١.٣±٥.٧٣٦	٢٢٠.٥
٨٣.٥	٢٢٢.٦	٢.٣٠٩ ١.٠٣٧	٢٢٢.٦±٥.٧٣٦	٢٢٢.١٩
١٦٧	٢٣٢	.	٢٣٢	٢٣٠.٥
٤١٧.٥	٢٦٠	.	٢٦٠	٢٥٥.٦٥
٦٦٨	٢٨١.٣	٢.٣٠٩ ٠.٨٢٠	٢٨١.٣±٥.٧٣٦	٢٨٠.٧٥

830	297.3	2.309	0.776	297.3 ± 0.737	297.48
1670	380	.		380	381.13
ε170	632	.	632	632.09	

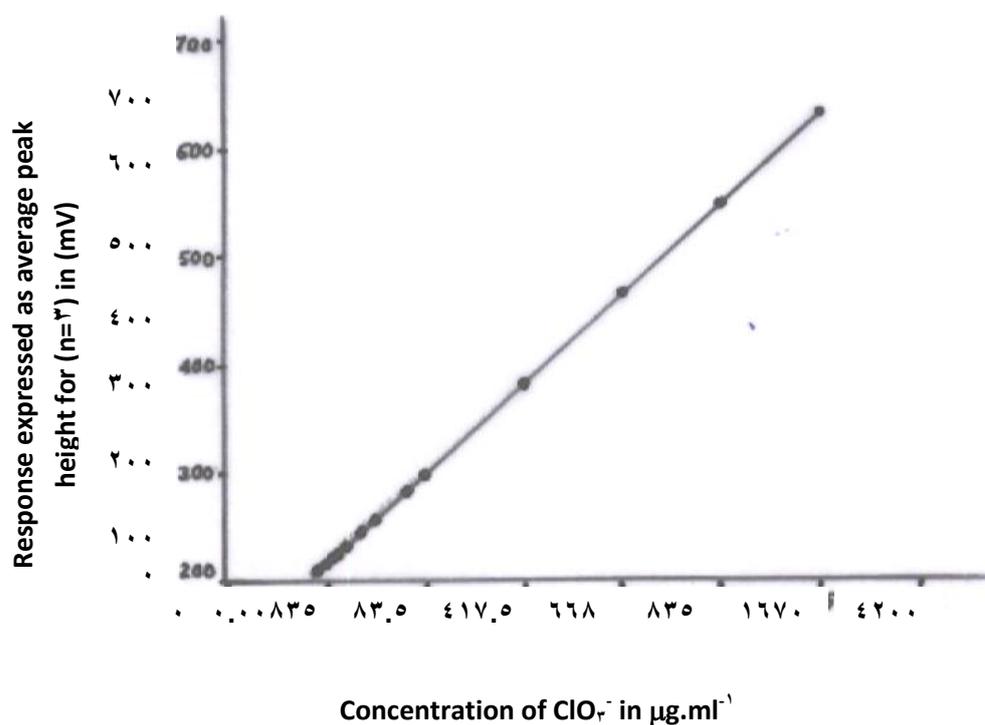


Figure (ε-13) Determination of chlorate ion by changing the response with concentration for system ($\text{ClO}_3^- - \text{I}^- - \text{H}_2\text{O}^+$)

Table (٤-١٢) Changing the response with concentration for obtaining on the calibration curve

Lowest value theoretically can begin it calibration curve $x = \text{DL } \mu\text{g.ml}^{-1}$		$20 * 10^{-3} \text{ mol.L}^{-1}$
Detection limit each $10 \mu\text{L}$	Theoretically from linear equation $y = \text{L.O.D.} = Y_B + r S_B$ at confidence limit ٩٥%	221.0 mol.L^{-1}
	Theoretically from equation $\text{D.L.} = \frac{3S_D}{\text{slope}}$	$1.07 * 10^{-3} \text{ mol.L}^{-1}$
	Theoretically from dilution to low conc. In calibration curve	$6.12 * 10^{-5} \mu\text{g.ml}^{-1}$
Conc. Allowed to reach it calibration curve ($1.0\%r \rightarrow r$)		$0.9997 \rightarrow 0.8997$ ٣
T calculate from $t = \frac{ t \sqrt{n-2}}{\sqrt{1-r^2}}$		٧.٥.٤
T from table at confidence limit ٩٥% for (n-٢)		٤.٣.٣
Correlation coefficient and percentage of linearity $\%r^2$		0.9997 $\%99.94$
No. of $[\text{ClO}_4^-]$ measured		٢٥
Linear equation at confidence limit ٩٥% Abs.I. $(\text{mV}) = (a \pm \text{Sat}) + (b \pm \text{Sbt}) [\text{ClO}_4^-] \mu\text{g.ml}^{-1}$		213.82889 ± 1.08 $2 * 4.3.3 + 8360.2$ $8 \pm 0.381 * 4.3.3$

Range of $[\text{ClO}_3^-]$ in $\mu\text{g}\cdot\text{ml}^{-1}$ in calibration curve (range)	$0.00835 \rightarrow 4170$
$[\text{ClO}_3^-]$ in $\mu\text{g}\cdot\text{ml}^{-1}$ measured	$4.10 \times 10^{-6} \rightarrow 4170$

ξ A-φ: Reproducibility

Reproducibility is studied in determination of chlorate ion via measurement of released iodine from system ($\text{ClO}_3^- - \text{I}^- - \text{H}_2\text{O}^+$) by using (0.00M) of chlorate ion, (0.0M) of potassium iodide, (2.0M) of hydrochloric acid with flow-rate of $1.90\text{ ml}\cdot\text{min}^{-1}$.

The relative standard deviation (R.S.D.) for replicate injections ($n=10$) is found to be 0.0432 as in table (ξ-13).

Table (ξ-13): The reproducibility for this method using in determination of chlorate ion by system ($\text{ClO}_3^- - \text{I}^- - \text{H}_2\text{O}^+$).

Conc. of ClO_3^- in ($\mu\text{g}\cdot\text{ml}^{-1}$)	Peak height (cm) for $n=10$	Peak height (mV) for $n=10$	\bar{Y} (mV)	σ_{n-1}	%RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
4170	10.6	624	624	0.2699	0.0432	624 ± 0.1929

The mean percentage recovery of chlorate ion concentration of 99.96% is obtained as shown in figure (ξ-14).

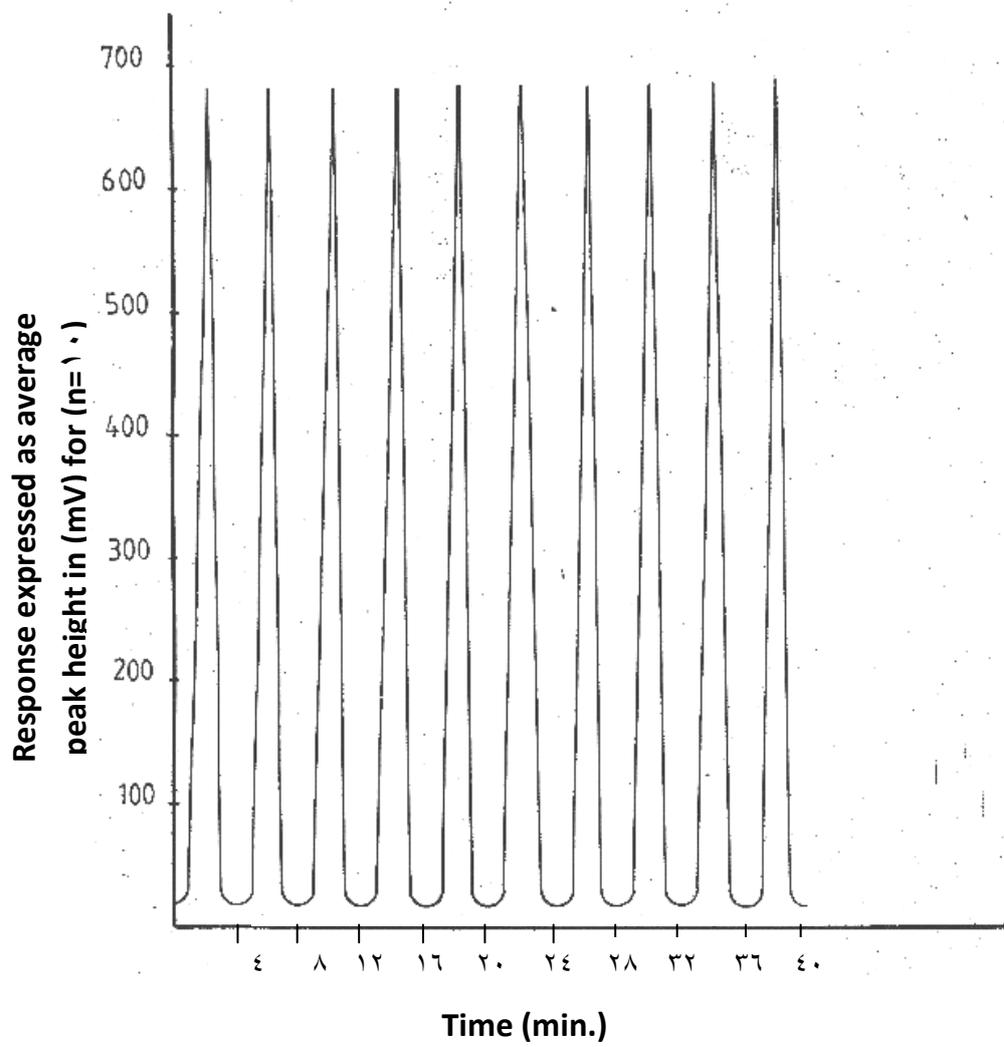


Figure (4-14): The reproducibility of ten measurements of released iodine for $(0.1 \times 10^{-3} \text{ M})$ chlorate ion

4-A-6: Detection limit⁽¹⁴⁾

detection limit (DL) is defined as the concentration corresponding to a signal three times the noise level of the background, in fact, it is the point at which we can make a decision on whether the element or the compound is present or not. Three times the detection limit is often called the limit of determination (LOD). In the determination of chlorate ion, the LOD found is $0.1 \times 10^{-3} \text{ mol.L}^{-1}$ and its mean is $(6.12 \times 10^{-5} \text{ ppm in } \mu\text{g.ml}^{-1})$.

4-A-7: Study of the interference

Many of foreign ions are studied in this method to ensure the validity of the proposed method for the determination of chlorate ion. The effect of various foreign ions on the determination of $(100 \mu\text{g.ml}^{-1})$ of chlorate ion is studied and table (4-14) shows the results of this study by using many cations and anions. It can be seen that there is no serious interference at the studied level.

Table (٤-١٤): Effect of interfering ions

Interference Effect %												Conc. of cation fold
CO ²⁺	Cd ²⁺	Cu ²⁺	Mn ²⁺	Sn ²⁺	Pb ²⁺	Zn ²⁺	Fe ²⁺	NH ₄ ⁺	K ⁺	Na ⁺	Ag ⁺	
•	•	-١.٣	-٠.٨	-١.٥	-١.٥	•	+٠.٧	+٠.٢	-٠.٤	+٣.٥	•	١
-٠.٤	+٠.٢	-١.٢	-١.٠	-٢.٥	-١.٠	•	+٠.٨	+٢.٤٢	-٠.٤	+١.٧٥	•	٢
+٠.٦	+٠.٣٥	-١.١٠	-١.٤	-٣.٠	-٠.٥	•	+٠.٨	+٢.٢	-٠.٥	+١.١٠	•	٣

Interference Effect %							Conc. of Anion fold
MnO ₄ ⁻	CrO ₄ ⁻	IO ₃ ⁻	NO ₃ ⁻	Br ⁻	Cl ⁻	SO ₄ ⁻	
•	+٠.٣	+٠.٥	•	-٠.٢	•	+٠.٥٠	١
+٠.١	-٠.٥	+٠.٧٥	•	-١.٢	+١.٠	+٠.٧٥	٢
+٠.١	-٠.٩٨	+٠.٨	-٠.٣	-١.٣	•	+٠.١٥	٣

٤A-٨: Study of the dead volume

To ensure accurate results obtained from this unit, we must be studied.

Wherever, the dead volume is small it means a best results.

Three experiments were done, in the first the iodine was formed from the system ($\text{ClO}_2^- - \text{I}^- - \text{H}_2\text{O}^+$), the carrier solution was H_2O^+ and injection I^- in (L_2). H_2O was injected instead of (ClO_2^-) in (L_1) and there was no response.

In the second experiment, (ClO_2^-) was injected in (L_1) and injection (H_2O) in (L_2) instead of (I^-) and the carrier solution was (H_2O^+), and there was no response obtained. From this experiment as well. In the third experiment, I^- was injected in loop (γ), and (ClO_2^-) was injected in loop (δ) and the carrier solution was (H_2O) and there was also no response.

This means that there was no dead volume and the unit was well designed.

ξ A-9: Applications:

ξ A-9-1: Determination of chlorate ion in aqueous solution:

Procedure:

The carrier of (2.0 M) hydrochloric acid is pumped at a flow-rate of (1.90 ml.min⁻¹). A (127 μl) aliquot of sample solution containing chlorate ion (0×10^{-6} , 0×10^{-5} , 0×10^{-4} , 0×10^{-3} M) are injected in the first loop and (31.2 μl) of potassium iodide concentration is injected in the second loop. Figure ($3-2$) shows that the carrier, sample and potassium iodide are mixed in the mixing coil at room temperature; the released iodine is measured spectrophotometrically at 350 nm.

The results obtained by the reaction system ($\text{ClO}_3^- - \text{I}^- - \text{H}^+ \text{O}^+$) using the homemade unit figure ($3-9$) of the standard samples are summarized in table ($2-10$) from which it can be seen that a good agreement is achieved between the standard value and the found value.

Table ($2-10$): Application in aqueous solutions.

Standard concentration of chlorate ion (M)	Found concentration of chlorate ion (M)
0×10^{-6}	2.990×10^{-6}
0×10^{-5}	0×10^{-5}
0×10^{-4}	0.3×10^{-4}
0×10^{-3}	2.99×10^{-3}

ξ A-9-2: Determination of chlorate ion in safety matches:

Due to the many uses and importance of matches in our life, which consists of material low kindling point, interesting phosphorus sesquisulfide (P_4S_3) with oxidant material such as potassium chlorate or barium chlorate that gives oxygen required to start the burning (Blaze) and mixing it with this materials soft glass powder with glue⁽¹¹⁰⁾, chlorate ion in match is determined by flow injection analysis technique figure (3-9), the response is found (7.96×10^{-5} M) which is (0.066 M) concentration of chlorate ion.

Procedure:

Taking five sticks, weighting them and dissolved in 20 ml of distilled water. The sample is injected in loop (1) replace potassium chlorate and injected (0.0 mol.L⁻¹) of potassium iodide in loop (2), (0.0 mol.L⁻¹) of hydrochloric acid used as a carrier stream at 1.90 ml.min⁻¹ of flow-rate. The results shown in table (ξ-16).

Table (ξ-16): The chlorate concentration in one stick of match.

Sample No.	Conc. of chlorate ion in (M)	\bar{Y}	σ_{n-1}	%R.S.D.	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
------------	------------------------------	-----------	----------------	---------	---

١	٨×١٠^{-٤}	٧.٩×١٠^{-٤}	٥.٧×١٠^{-٦}	٠.٧٢٤	$٧.٩ \times ١٠^{-٤} \pm ١.٤ \times ١٠^{-٥}$
٢	٨×١٠^{-٤}				
٣	٧.٩×١٠^{-٤}				

٤A-٩-٣: Determination of chlorate ion in hypochlorite solution:

The determination of chlorate in hypochlorite solution is done by using a sample of hypochlorate which is homemade by Babylon company for soap and detergent manufacturing limited-Baghdad, and taking a constant volume from it (١.٠ ml) and diluting it by distilled water (٥:١), then injecting in loop (١) figure (٣-٩) instead of potassium chlorate solution, and the results are shown in table (٤-١٧).

Table (٤-١٧): Determination of chlorate ion in hypochlorate solution.

Sample No.	Conc. of chlorate ion in (M)	\bar{Y}	σ_{n-1}	%R.S.D.	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
١	٩×١٠^{-٢}	٠.٠٨٩	٠.٠٠١٧	١.٩٤٦	٠.٠٨٩ ± ٠.٠٠٤٢
٢	٩×١٠^{-٢}				
٣	٨.٧×١٠^{-٢}				

4 B- Determination of chlorate ion by second unit:

4 B-1: Study the factors influencing on the absorbance in the determination of chlorate ion:

Study the influence of variables on absorbance of released iodine through the reaction of chlorate ion with potassium iodide in the presence of sulphuric acid for system $(\text{ClO}_3^- - \text{I}^- - \text{H}_2\text{O}^+)$, which includes physical and chemical parameters for the home made unit which consists of three ways. The first way for sulphuric acid solution passes while the second way passes potassium iodide solution and the third is to transfer stream of sample injected through an injection valve and completing this reaction after passing through primary mixing coil, secondary mixing coil, and completion reaction coil then to cell reaction and to amplifier that is home made and finally to recorder for recording the signal.

ξB-1-1: Physical parameters optimization

ξB-1-1-1: Injection time:

Using experimental concentrations of sulphuric acid (1.0 M) and potassium iodide (0.12 M) by injecting sample volume (10 μl) of chlorate ion and flow rate (5 ml.min⁻¹), then study if the injection time has an effect on the absorbance of released iodine from system (ClO₃⁻-I⁻-H₂O⁺).

The time of injection applied was (10, 20, 30, 40, 50, 60) count obtained from the results shown in table (ξ-18) and figure (ξ-19) explains the change in the intensity and shape of the response obtained when injection of chlorate ion at concentration (300 μg.ml⁻¹), the changes were increase with an increasing the time period which allows the valve in the injection place to ensure from exit of sample section totally from injection valve as a result obtained from the response has intensity represent concentration of chlorate ion reaching to (60 sec) (40 count).

Table (ξ-18): Effect of time of injection on the absorbance to system (ClO₃⁻-I⁻-H₂O⁺) 300 μg.ml⁻¹ of chlorate ion.

Time of injection (count)	Reaching time section of sample to cell (sec)	response \bar{Y} in (mV)	σ_{n-1} %RSD	$\bar{y} \pm t \frac{\sigma_{n-1}}{\sqrt{n}}$
10	48.0	1020	1.00 0.098	1020 ± 2.48
20	54.0	1460	0.90 0.070	1460 ± 2.36

۳.	۵۷.۶	۱۹۲.	۰.۲۳ ۰.۰۱۲	۱۹۲.±۰.۵۷
۴.	۶۰.	۲۰۷.	۰.۸۵ ۰.۰۴۱	۲۰۷.±۲.۱۱
۵.	۶۶.	۲۰۸.	۰.۵۵ ۰.۰۲۶	۲۰۸.±۱.۳۷
۶.	۷۲.	۲۰۹.	۰.۷۵ ۰.۰۳۴	۲۰۹.±۱.۸۶

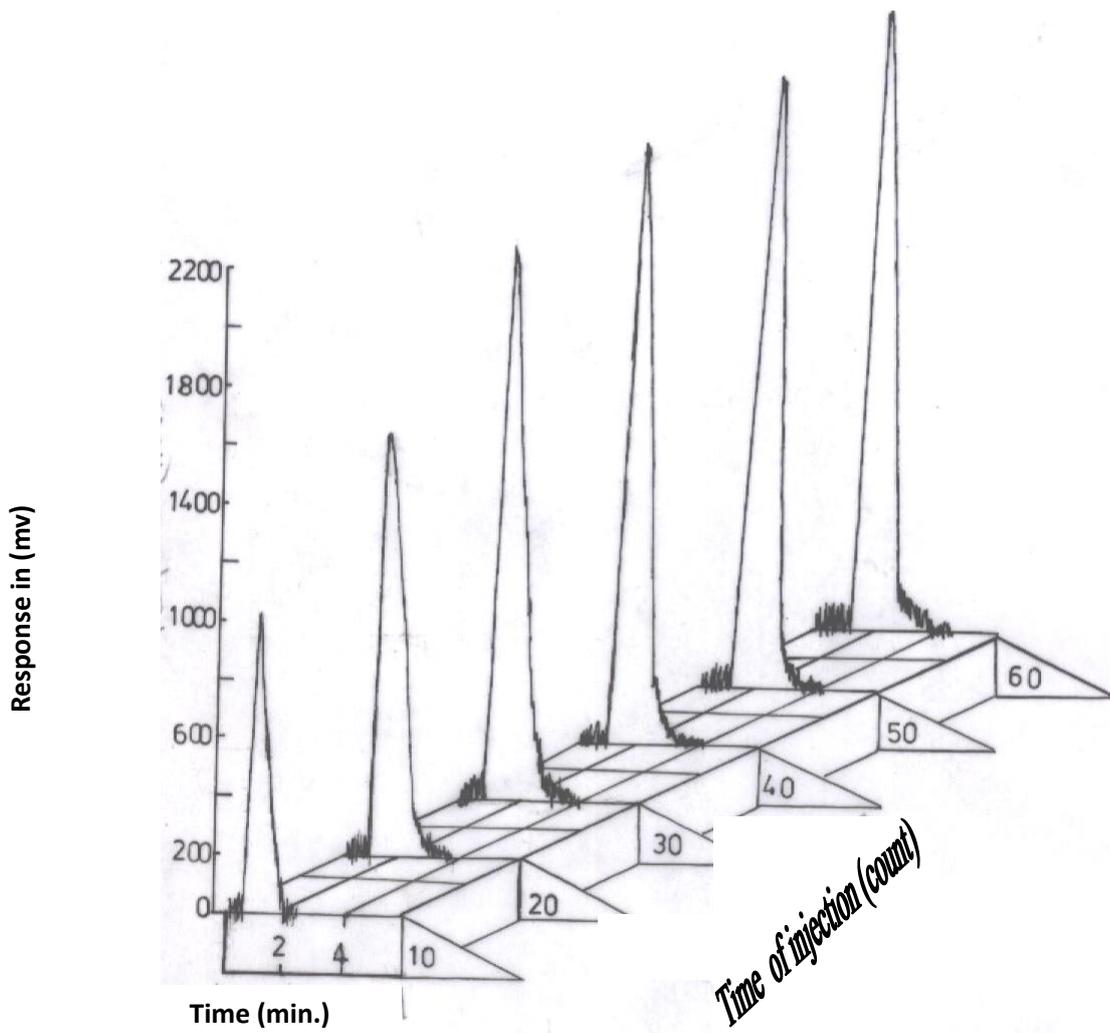


Figure (2-10): Effect of changing in time of injection on the height and shape of the response by using ($300 \mu\text{g.ml}^{-1}$) concentration of chlorate ion .

Although the increase of injection time caused a high intensity response, it causes an increase in width of the response peak by the effect of dispersion from diffusion, convection and process of dilution to coloured section. This increases of effect with increasing of path that passes for reaching to cell absorbance (at increasing time of injection), thus increasing the physical variables perhaps leads to low concentrations of chlorate ion (slump in detection limit).

The best time is (60 sec) to assure the exit of section from injection valve, as shown in figure (4-16) which shows minor differences of response intensity obtained from released iodine for system ($\text{ClO}_3^- - \text{I}^- - \text{H}_2\text{O}^+$) to reach injection time above (60 sec.).

To obtain accurate details of response, the recorder paper chart speed must be increased to ($3 \text{ cm} \cdot \text{min}^{-1}$) in comparison with speed of recorder paper ($0.5 \text{ cm} \cdot \text{min}^{-1}$), as shown in figure (4-16).

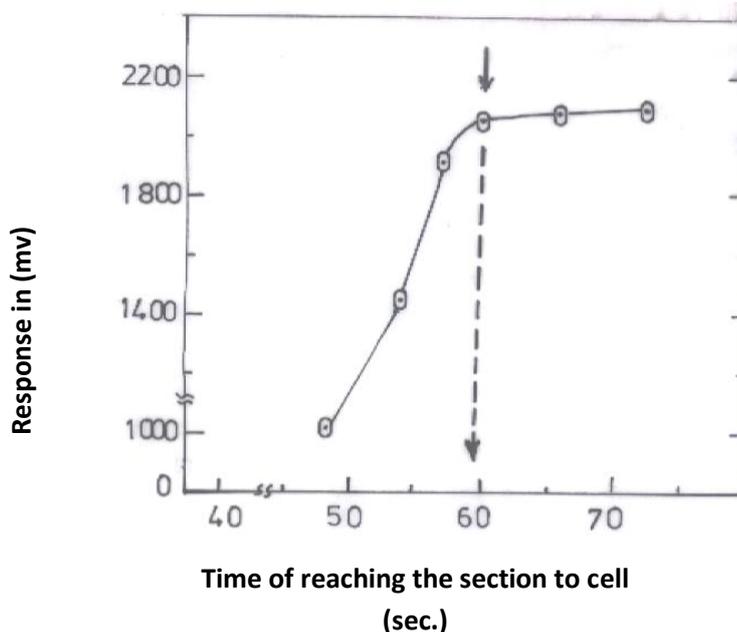


Figure (4-16): The effect of changing in the time of injection on the height of response peak and choosing the optimum time which is (6. sec.)

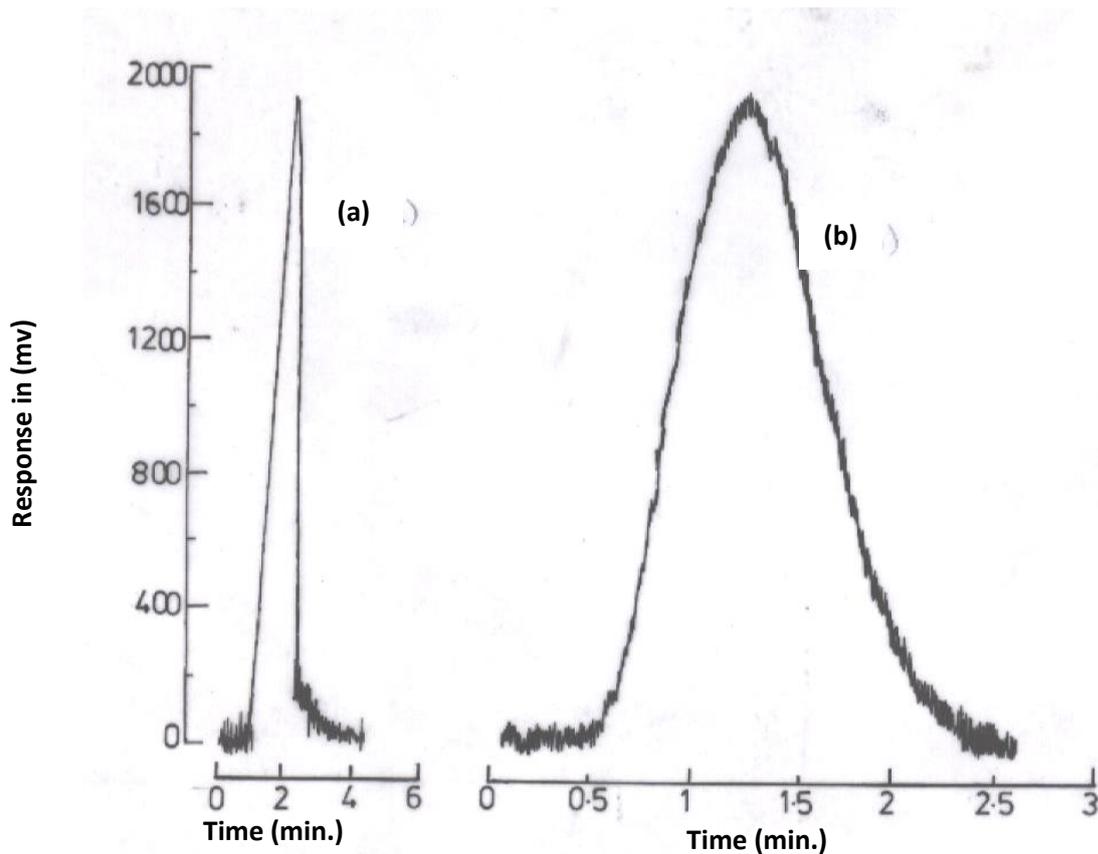


Figure (4-17): Effect the increasing in chart speed of recorder on the shape of response

a- at speed 1.0 cm.min.^{-1}

b- at speed 3 cm.min.^{-1}

ξ B-1-1-2: Flow-rate

The whole reaction consist of chlorate ion ($200 \mu\text{g.ml}^{-1}$), (0.12 M) of potassium iodide, and (1.0 M) of sulphuric acid with volume of sample injection ($10 \mu\text{l}$) and changing the flow rates ($1, 1.3, 1.8, 2, 3, 3.5, 4, 4.5$ and 5 ml.min^{-1}); this leads to obtain the results as shown in table ($\xi-19$) by repeating the injection for each sample three times successively.

Table ($\xi-19$): The changing in average of flow rate on the response of released iodine to system ($\text{ClO}_3^- - \text{I}^- - \text{H}_2\text{O}^+$).

Flow-rate (ml.min^{-1})	Reaching time the section coloured to cell (sec)	response \bar{Y} in (mV)	σ_{n-1} %RSD	$\bar{y} \pm t_{0.05} \frac{\sigma_{n-1}}{\sqrt{n}}$	Width of base response Δt_B (sec.)
1.0	96.00	140.0	2.30 0.17	140.0 ± 0.84	144
1.3	84.00	146.0	1.00 0.11	146.0 ± 3.80	132
1.8	72.00	160.0	1.03 0.072	160.0 ± 2.06	120
2.0	60.00	168.0	1.97 0.12	168.0 ± 4.89	96
3.0	50.00	172.0	1.33 0.077	172.0 ± 3.30	84

٣.٥	٥٠.٠٠	١٨٦.	٢.٠٥ ٠.١١	١٨٦.٠±٥.٠٩	٧٢
٤.٠	٤٨.٠٠	١٩٠.	١.٠١ ٠.٠٥٣	١٩٠.٠±٢.٥١	٦٠
٤.٥	٤٢.٠٠	١٨٠.	١.٩٢ ٠.١١	١٨٠.٠±٤.٧٧	٥٨
٥.٠	٤٠.٠٠	١٧٠.	١.٥٥ ٠.٠٩١	١٧٠.٠±٣.٨٥	٥٨

The time which has been calculated from departing valve of injection reaching to cell of absorption then the measurement.

The results from previous table indicated that in the low rates in which the effect of physical variables from dilution and dispersion is very high this lead to obtain on the response has low intensity and width in peaks by increasing volume of the section coloured comparison by increasing flow rate reaching to ($\xi \text{ ml.min}^{-1}$) obtained from highly intensity to response and with sharp peaks and width in the basis of response is low figure (ξ^{-1}) show that.

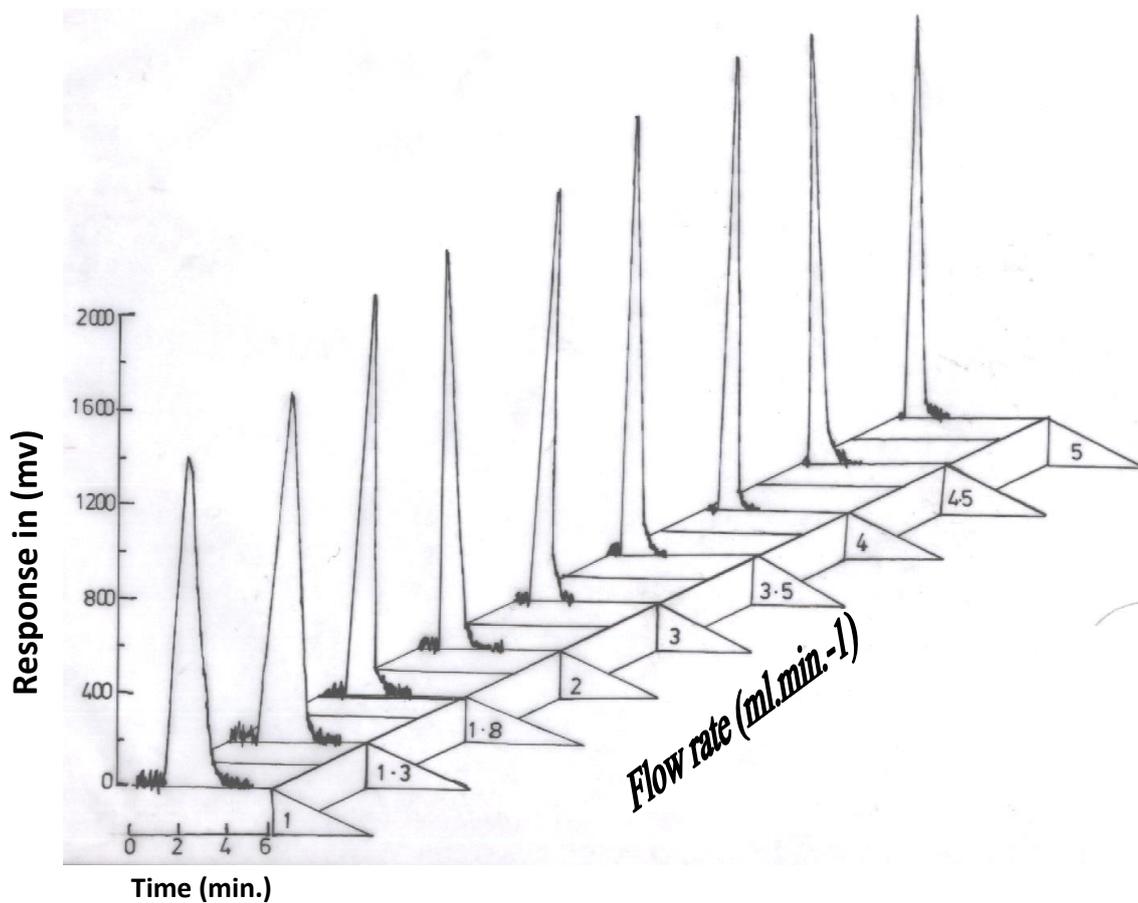


Figure (4-18): Effect of the changing in flow-rate on the intensity and shape of the response by using conc. For injection sample of chlorate ion $20 \mu\text{g.ml}^{-1}$

In de high rates, a sharp peaks of response were obtained, while in low because of the period of time needed to complete the reaction, and decrease iodine (I_2) from the system ($\text{ClO}_3^- + \text{I}^- + \text{H}_2\text{O}^+$), is little and not enough; this leads to obtain low intensity response as shown in figure (4-19 a).

Therefore selection of flow rate (4 ml.min^{-1}) is optimum to set sharp peaks responses, low to base width the response and high intensity; this leads to moving toward low concentrations and improvement of detection limit.

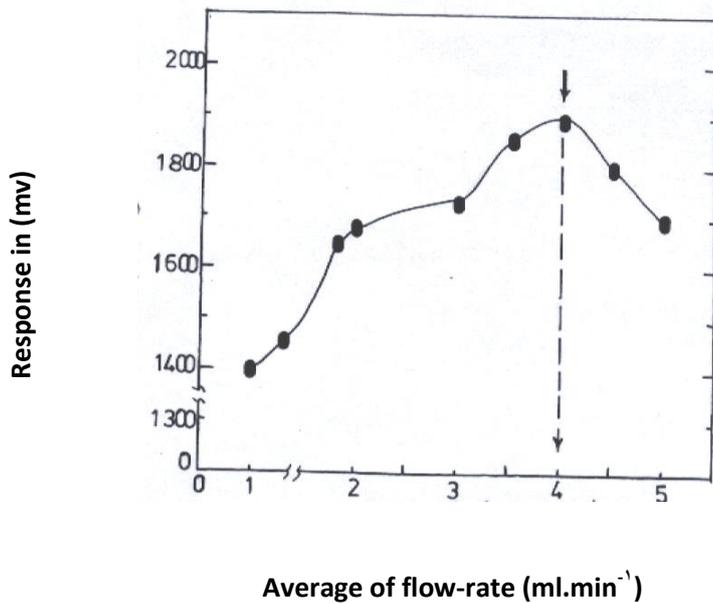


Figure (٤-١٩ a): Effect the changing in average of flow-rate on the height of response optimum flow rate is (٤ ml.min⁻¹)

Also it has been noticed that by increasing the flow rate, a decrease in the time is required to reach the coloured section cell of absorption, and physical variables decrease too (dilution or dispersion); this leads to the reduction in volume of section coloured although effect of it on the decrease in the width base of response (ΔtB) figure (٤-١٩ b, c).

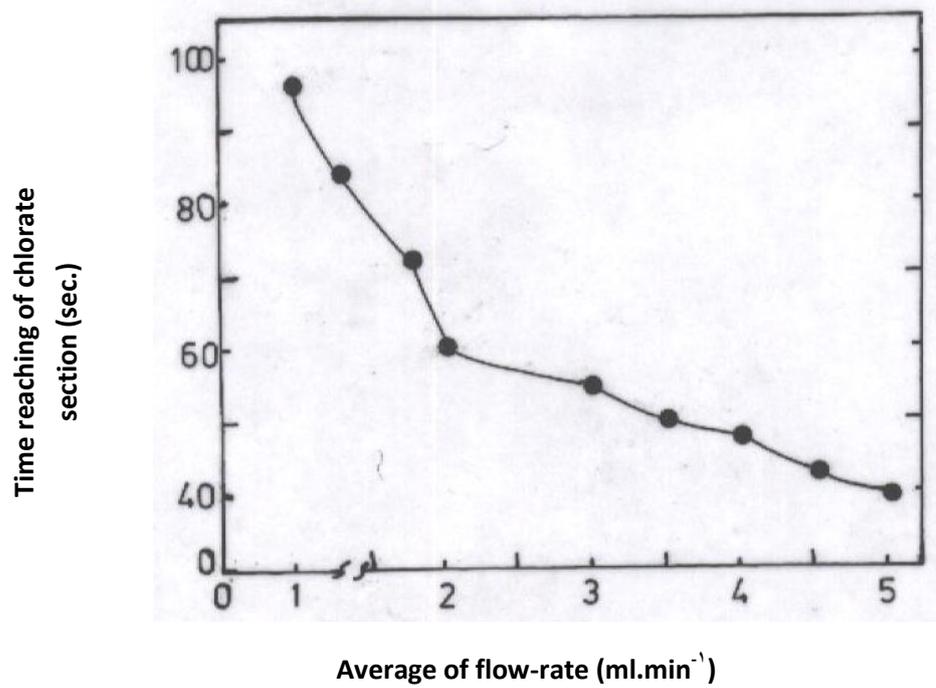


Figure (4-19b): Effect of increasing in flow rate on decreasing of reaching time of colored section to cell of absorption

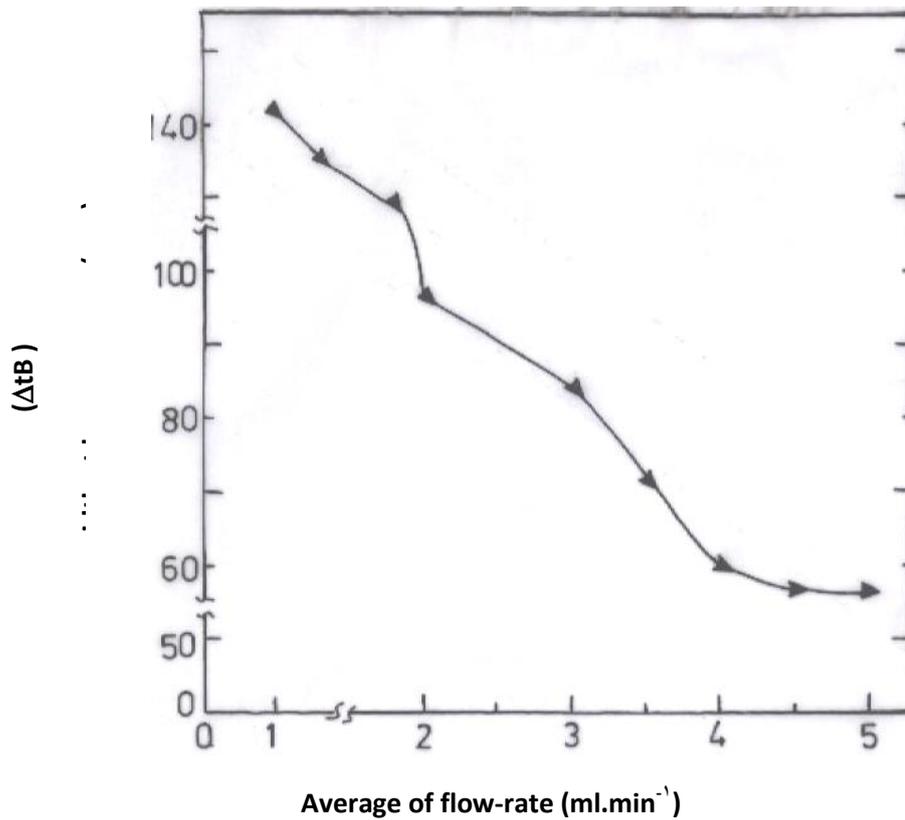


Figure (4-19c): The increasing in flow rate on decreasing the width of base response (ΔtB) expressed by unit of time (sec.)

The results in table (4-19) show the linear relationship between width of base response and required time from departing section of sample for valve injection reaching to coloured section to cell of absorption such as shown in table (4-20). By repeating the measurement three times, with small percentage of relative standard deviation occurs.

Table (٤-٢٠): Results of relationship width of base response with the time.

Reaching time of the coloured section to cell (sec.)	Width base response ΔtB (sec.)	\hat{Y} (sec.)
٤٢	٥٨	٥٩.٢٢
٤٨	٦٠	٦٩.٤٨
٥٠	٧٢	٧٢.٨٩
٥٥	٨٤	٨١.٤٤
٦٠	٩٦	٨٩.٩٨
٧٢	١٢٠	١١٠.٤٩
٨٤	١٣٢	١٣٠.٩٩
٩٦	١٤٤	١٥١.٥٠

٤B-١-١-٣: Sample volume

By using reaction unit (figure (٣-١٥)), the following materials are complementary to the reaction: chlorate ion ($٢٥٠ \mu\text{g.ml}^{-1}$), potassium iodide (٠.١٥mol.L^{-1}), and sulphuric acid (١.٢mol.L^{-1}), and using time of injection (٦٠sec.) at flow rate (٤ml.min^{-1}) with variable sections of sample by ٠.٧mm diameter, to the result in table (٤-٢١) are obtained.

Table (٤-٢١): The changing in the volume of section sample on the response of released iodine to system ($\text{ClO}_3^- - \text{I}^- - \text{H}^+ \text{O}^+$).

Length of sample section (cm)	Volume of section sample (μl) experimentally	Reaching time of the section to cell (sec.)	Width of base response ΔtB (sec.)	response \bar{Y} in (mV)	σ_{n-1} / %RSD	$\bar{y} \pm t_{0.05} \frac{\sigma_{n-1}}{\sqrt{n}}$
٥	٢٠	٤٧	٥٠	٢٧٠٠	١.٢٣ / ٠.٤٦	٢٧٠٠ \pm ٣.٠٦
١٠	٤٠	٤٧	٥٥	٢٧٨٠	١.٥٨ / ٠.٥٧	٢٧٨٠ \pm ٣.٩٣
١٥	٦٠	٤٨	٦٠	٣٠٠٠	٠.٩٥ / ٠.٣٢	٣٠٠٠ \pm ٢.٣٦
٢٠	٨٠	٤٨	٧٢	٢٩٩٠	١.٣٣ / ٠.٤٤	٢٩٩٠ \pm ٣.٣٠
٣٠	١١٥	٤٨	٧٥	٢٩٠٠	١.٥٥ / ٠.٥٣	٢٩٠٠ \pm ٣.٨٥

From table (4-21) we can conclude that with the increase of section volume the intensity of response for released iodine will increase reaching a volume of (7. μ l), then the response begins to decrease a little. This is due to the effect of internal filter that resulted from colour depth of released iodine that prevents sensitizer from accepting light intensity transmittance with high efficiency according to gradual decrease in response as shown in figure (4-2. a) that explains the intensity and shape of response. In addition figure (4-2. b) that shows the optimum section volume to obtain high intensity is (7. μ l).

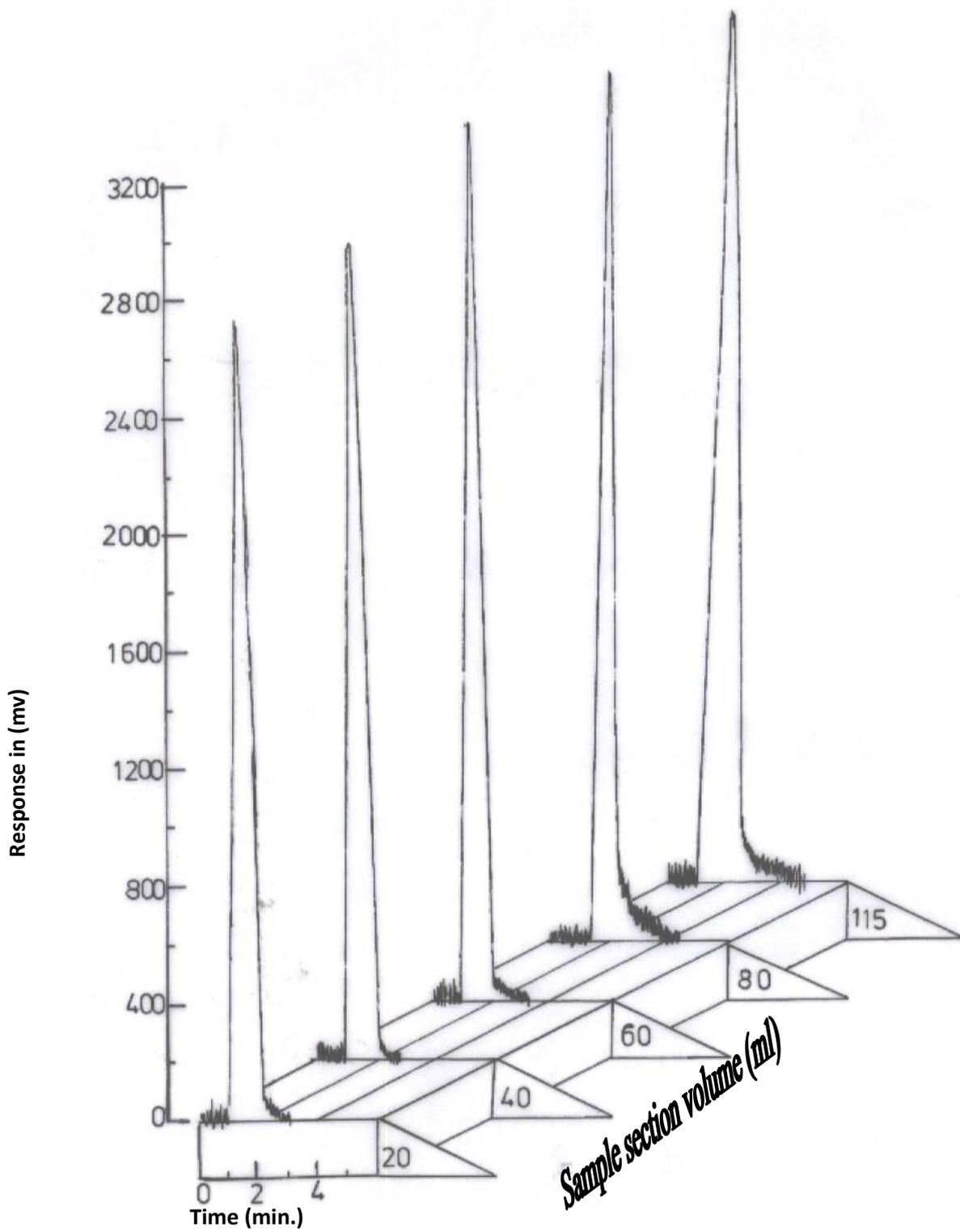


Figure (4-20 a): the changing of volume of injected sample section on intensity and shape of the response

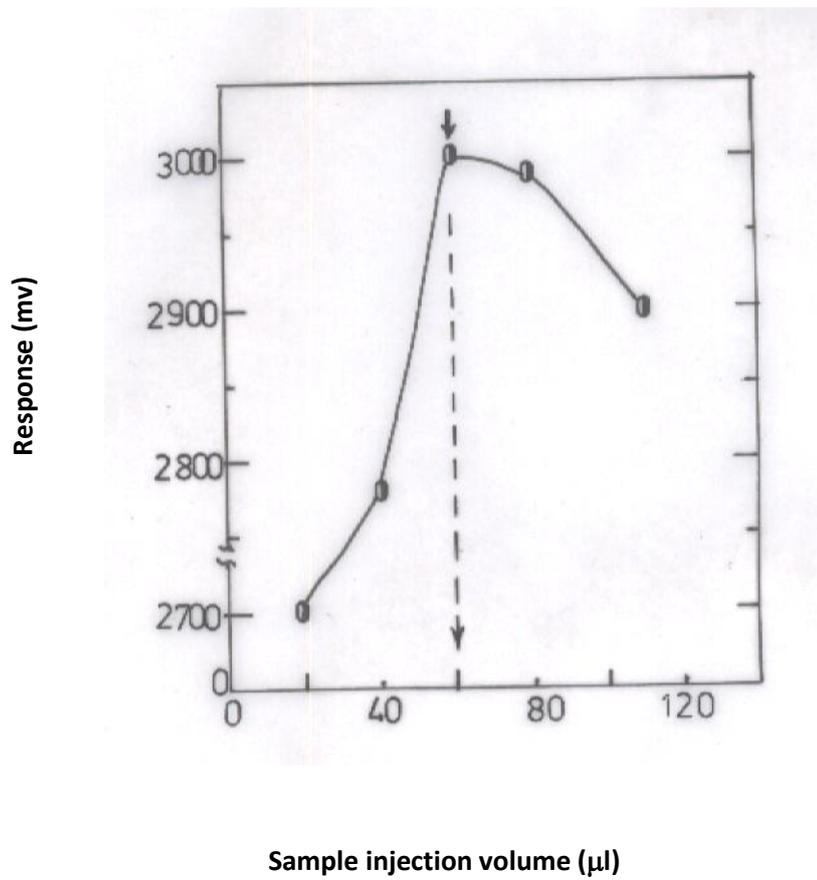


Figure (4-2, b): Effect of the changing in injected of sample volume on height of response and noticed the best volume of section is (60 μl)

ξB-١-٢: Chemical parameters

By using designed unit figure (٣-١٥) and fixed physical variables: injection time (٦٠ sec.), volume of injected sample (٦٠ μl), and flow rate (٤ ml.min⁻¹) and using changing percentage for each of sulphuric acid and potassium iodide with constant concentration of chlorate ion (٢٥٠ μg.ml⁻¹), the results indicates to the percentage of mixing in table (٤-٢٢) and by repeating all measurement three times.

Table (٤-٢٢): Effect the changing in conc.s of acid and potassium iodide on the response to system (ClO₃⁻-I⁻-H₂O⁺).

Conc. KI mol.L ⁻¹	Conc. acid H ₂ O ⁺ mol.L ⁻¹	response (n = 3) \bar{Y} in (mV)	σ_{n-1} %RSD	$\bar{y} \pm t_{0.05} \frac{\sigma_{n-1}}{\sqrt{n}}$
٠	٠	٠	٠	٠
٠	٢.٠	٠	٠	٠
٠.١	١.٥	٣٠٦٠	٢.١٥ ٠.٠٧٠	٣٠٦٠ ± ٥.٣٤
٠.١٥	١.٠	٢٨٤٠	١.٥٥ ٠.٠٥٥	٢٨٤٠ ± ٣.٨٥
٠.٢٥	٠	٠	٠	٠
٠.٢٥	٢.٠	٢٨٠٠	١.٣٢ ٠.٠٤٧	٢٨٠٠ ± ٣.٢٨

From results of the table, we can notice that on increasing the concentration of potassium iodide, the response will decrease compared with

increasing of acidic media concentration, this lead to increasing intensity of response because of liberated Iodine.

While increasing of potassium iodide due to depth colour and the influence internal filter phenomena increased, which prevent reaching transmittance of light to sensitizer, therefore; we can conclude that high concentration of acid (1.0 M) is the best and concentration of potassium iodide is more less (0.1 M).

At the absence of any substance of completion reaction which leads to prevent releasing of iodine, thus did not obtain any response.

According to that fixed the percent mixing of acid with concentration (1.0 M) with concentration of potassium iodide (0.1 M) this is optimum percent lead to obtaining of the highest intensity of response and can indicated intensity and shape of this response in figure (4-21).

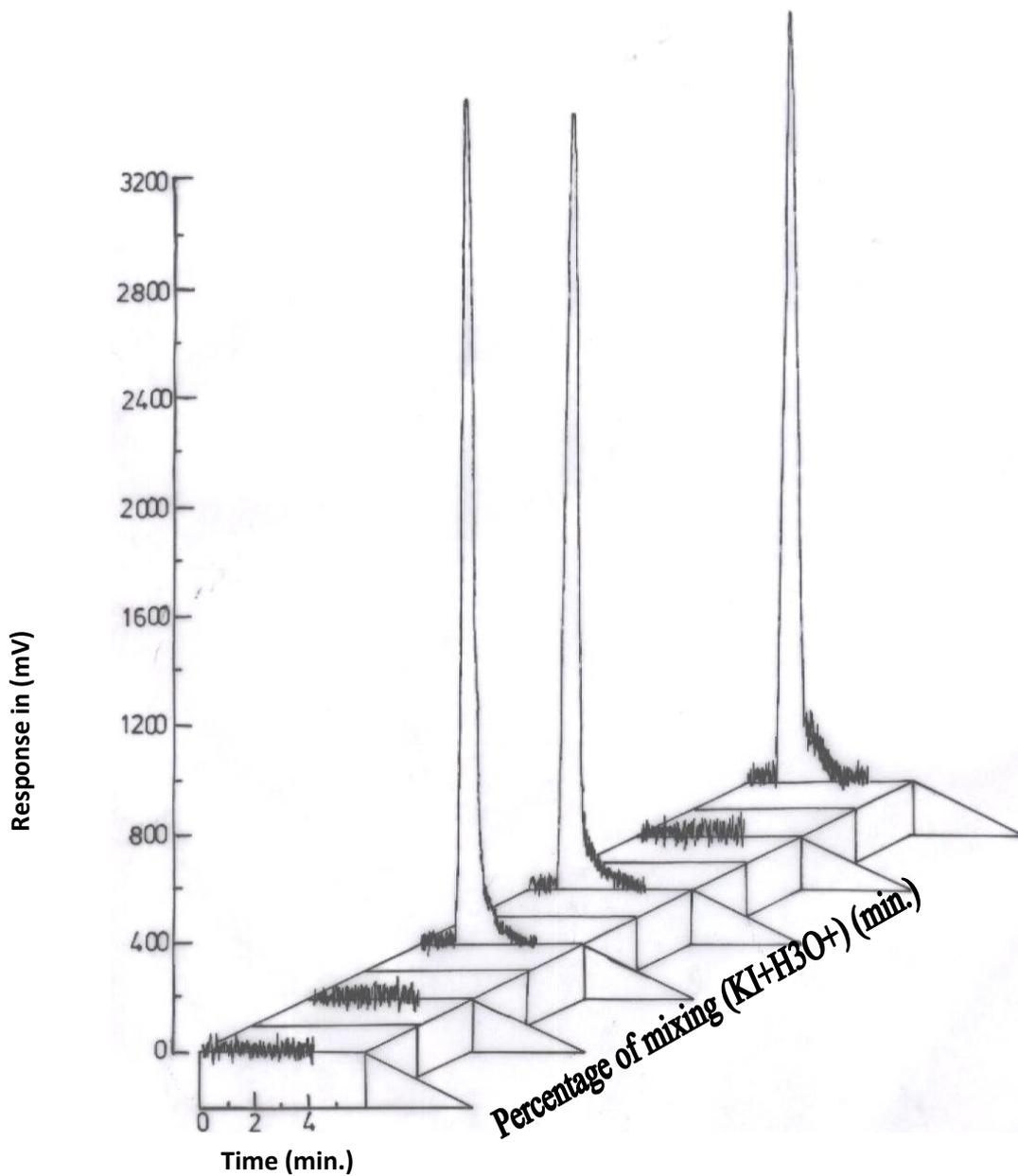


Figure (4-21): Effect of the changing in the percent mixing to both of sulphuric acid and potassium iodide on the intensity and shape of the response and noticed the percent of mixing to H_2O^+ (1.0 M) + KI (0.1 M) is the best.

ξB-۲: Variation of response versus concentration

ξB-۲-۱: Preparation of calibration curve

By using the optimum conditions of physical and chemical variables, series of solutions were prepared by changing the concentrations of chlorate ion from (۰-۶۰۰ $\mu\text{g.ml}^{-1}$). The response of released iodine was measured for system ($\text{ClO}_3^- - \text{I}^- - \text{H}^+ \text{O}^+$) and each concentration has been injected three times successively on the carrier stream of distilled water in unit figure (۳-۱۰) and the obtained results were indicated in table (ξ-۲۳) and figure (ξ-۲۲).

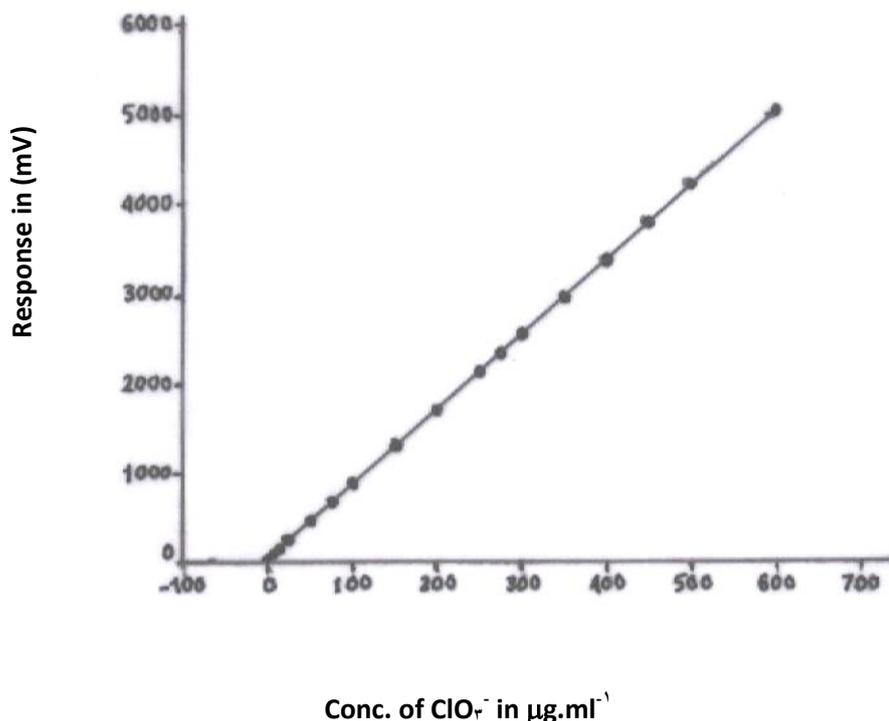


Figure (ξ-۲۲): Changing the response with concentration for obtaining on calibration curve for system ($\text{ClO}_3^- - \text{I}^- - \text{H}^+ \text{O}^+$)

Table (٤-٢٣): Results for the response obtained versus various concentration of chlorate; using the newly home made photometer.

$[\text{ClO}_3^-] \mu\text{g.ml}^{-1}$	Response to (n=٣) \bar{y} in (mV)	σ_{n-1} / %RSD	$\bar{y} \pm t_{0.05} \frac{\sigma_{n-1}}{\sqrt{n}}$	\hat{y} predicted in (mV)
٠	٠	٠ / ٠	٠	٥٥.٥٨
٥	٨٠	٠.٣٢ / ٠.٤٠	٨٠ ± ٠.٧٩	٩٧.٠٨
١٠	١١٢	٠.١١ / ٠.٠٩٨	١١٢ ± ٠.٢٧	١٣٨.٥٧
١٥	٢٠٠	٠.١٥ / ٠.٠٧٥	٢٠٠ ± ٠.٣٧	١٨٠.٠٦
٢٥	٢٤٠	٠.٣٣ / ٠.١٣٨	٢٤٠ ± ٠.٨٢	٢٦٣.٠٥
٥٠	٤٠٠	٢.١٥ / ٠.٥٣٨	٤٠٠ ± ٥.٣٤	٤٧٠.٥٣
٧٥	٦٠٠	١.٤٥ / ٠.٢٤٢	٦٠٠ ± ٣.٦٠	٦٧٨.٠٠
١٠٠	١٠٨٠	٢.٥٥ / ٠.٢٣٦	١٠٨٠ ± ٦.٣٤	٨٨٥.٤٨
١٥٠	١٤٦٠	١.٩٥ / ٠.١٣٤	١٤٦٠ ± ٤.٨٤	١٣٠٠.٤٢
٢٠٠	١٧٨٠	٢.٠٠ / ٠.١١٢	١٧٨٠ ± ٤.٩٧	١٧١٥.٣٧
٢٥٠	٢٠٤٠	٣.٠٥ / ٠.١٤٩	٢٠٤٠ ± ٧.٥٨	٢١٣٠.٣٢
٢٧٥	٢٣٤٩	٢.٣٥ / ٠.١٠٠	٢٣٤٩ ± ٥.٨٤	٢٣٣٧.٧٩
٣٠٠	٢٤٦٠	٢.١١ / ٠.٠٨٦	٢٤٦٠ ± ٥.٢٤	٢٥٤٥.٢٧
٣٥٠	٢٩٥٧	٢.٠٩ / ٠.٠٧١	٢٩٥٧ ± ٥.١٩	٢٩٦٠.٢١
٤٠٠	٣٣٧٥	٣.٤٥ / ٠.١٠٢	٣٣٧٥ ± ٨.٥٧	٣٣٧٥.١٦
٤٥٠	٣٧٩٠	٢.١٩ / ٠.٠٥٨	٣٧٩٠ ± ٥.٤٤	٣٧٩٠.١١
٥٠٠	٤٢٠٥	١.٨٧ / ٠.٠٤٤	٤٢٠٥ ± ٤.٦٥	٤٢٠٥.٠٥
٦٠٠	٥٠٣٥	٢.٤٥ / ٠.٠٤٩	٥٠٣٥ ± ٦.٠٩	٥٠٣٤.٩٥

Table (٤-٢٤): The changing of response with concentration for obtaining on calibration curve

Lowest value theoretically can begin it calibration curve $x=0$.DL		٠.٢٧ ng
Detection limit each ١٠ μ L	Theoretically from linear equation $y=L.O.D.=Y_B + rS_B$ at confidence limit ٩٥%	٢٩١.٧٠ μ g
	Theoretically from equation $D.L = \frac{3S_D}{\text{slope}}$	٥.٤٢٥ pg
	practically from dilution to low conc. In calibration curve	١ μ g.ml ^{-١}
Conc. Allowed to reach it calibration curve (١٠%r→r)		٠.٩٩٨٨٤ → ٠.٨٩٨٩٥
t calculate from $t = \frac{ t \sqrt{n-2}}{\sqrt{1-r^2}}$		٣٥١.٩٨
t from table at confidence limit ٩٥% for (n-٢)		٤.٣٠٣
Correlation coefficient and percentage of linearity %r ^٢		٠.٩٩٨٨٤ %٩٩.٧٧
No. of [ClO _٢ ⁻] measured		١٨
Linear equation at confidence limit ٩٥% Abs.I. (mV)=(a±Sat)+(b±Sbt) [ClO _٢ ⁻] μ g.ml ^{-١}		٥٥.٥٨±٣١.٥٤٥*٤.٣ ٠.٣+٨.٢٩٨±٠.١١٢*٤ .٣٠٣
Range of [ClO _٢ ⁻] μ g.ml ^{-١} in calibration curve		٥ → ٦٠٠

[ClO ₂ ⁻] in μg.L ⁻¹ measured	0 → 6.0
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ξB-2-2: The standard deviation for the relationship response with concentration and normal distribution of results:

According to the results for changing the response with concentration in (ξB-2-1) and taking δ , 2δ , 3δ from value \hat{Y}_i predicted, the results are shown in table (ξ-20); there results showed approximately obey to the normal distribution behaviour .

68% falling within $\pm\delta n^{-1}$ from value \hat{Y}_i predicted, 90% falling within $\pm 2\delta n^{-1}$ from value \hat{Y}_i and predicted 99% falling within $\pm 3\delta n^{-1}$ from value \hat{Y}_i predicted.

And from the results in table (ξ-20) and figure (ξ-23) we can notice the practical values.

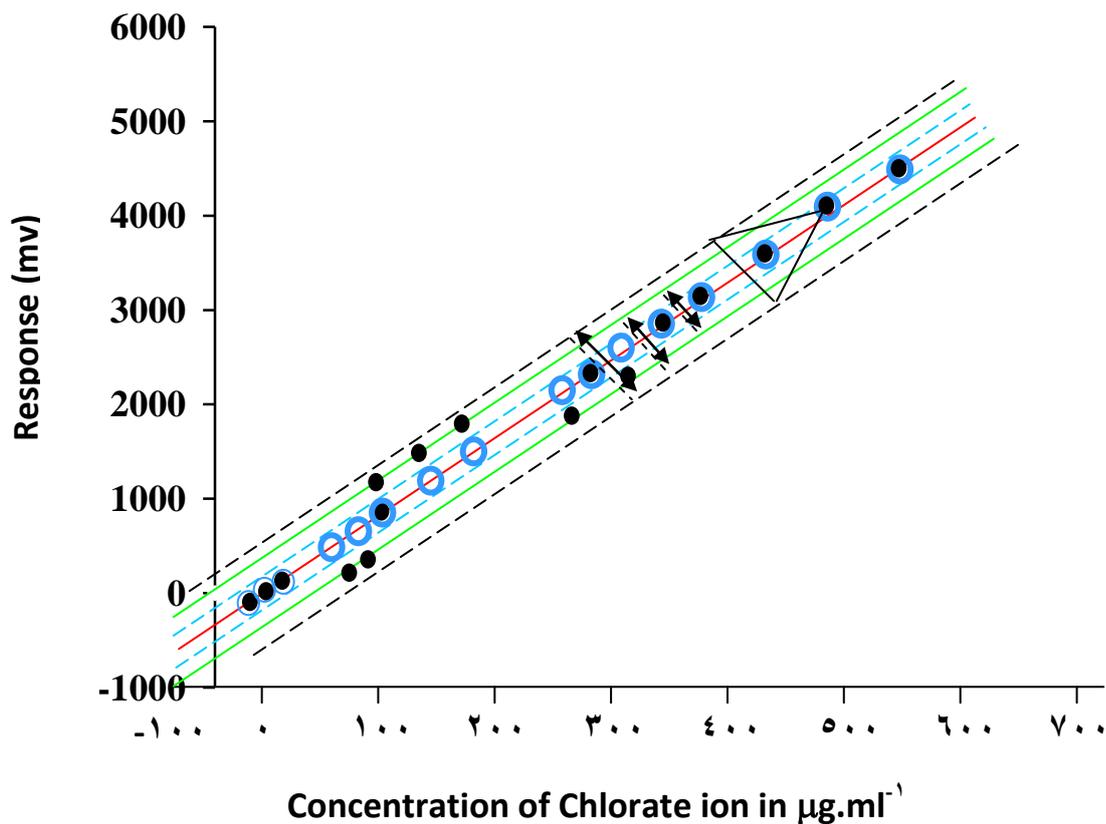


Figure (4-23): Calibration curve for determination of chlorate ion expressed by (mv) against concentration ($\mu\text{g.ml}^{-1}$) shown standard deviation and ranges of satisfy $\pm 1\sigma_{\hat{y}}$ represented 68%, $\pm 2\sigma_{\hat{y}}$ represented 95% and $\pm 3\sigma_{\hat{y}}$ represented 99.7% according to Gauss curve of normal distribution. The curve shows at $\pm 1\sigma_{\hat{y}}$ there is 20 of 36 measurement fall in range that act 69.4% while in $\pm 2\sigma_{\hat{y}}$ its follows 34 of 36 measurement in the range at 94.4% and at $\pm 3\sigma_{\hat{y}}$ all points fall in normal distribution curve.

While the calculation of residual of $(y_i - \hat{y}_i)$ and the percentage can be shown in table (٤-٢٦) and figure (٤-٢٤).

Table (٤-٢٦): The results of changing the response with concentration to calculating residual (y_i) practical from (\hat{y}_i) predicted and the percentage.

[ClO₂⁻] μg.ml⁻¹	Practical y_i mv	Predicted \hat{y}_i mv	Residual $(y_i - \hat{y}_i)$ mV	% Residual $\frac{y_i - \hat{y}_i}{y_i} \times 100$
٠	٠	٥٥.٥٨	-٥٥.٥٨	٠.٠٠
٥	٨٠	٩٧.٠٧	-١٧.٠٨	-٢١.٣٤
١٠	١١٢	١٣٨.٥٧	-٢٦.٥٧	-٢٣.٧٢
١٥	٢٠٠	١٨٠.٠٦	١٩.٩٤	٩.٩٧
٢٥	٢٤٠	٢٦٣.٠٥	-٢٣.٠٥	-٩.٦١
٥٠	٤٠٠	٤٧٠.٥٢	-٧٠.٥٢	-١٧.٦٣
٧٥	٦٠٠	٦٧٨.٠٠	-٧٨.٠٠	-١٣.٠٠
١٠٠	١٠٨٠	٨٨٥.٤٨	١٩٤.٥٢	١٨.٠١
١٥٠	١٤٦٠	١٣٠٠.٤٢	١٥٩.٥٨	١٠.٩٣
٢٠٠	١٧٨٠	١٧١٥.٣٧	٦٤.٦٣	٣.٦٣
٢٥٠	٢٠٤٠	٢١٣٠.٣٢	-٩٠.٣٢	-٤.٤٣
٢٧٥	٢٣٤٩	٢٣٣٧.٧٩	١١.٢١	٠.٤٨
٣٠٠	٢٤٦٠	٢٥٤٥.٢٧	-٨٥.٢٧	-٣.٤٧
٣٥٠	٢٩٥٧	٢٩٦٠.٢١	-٣.٢١٢	-٠.١١
٤٠٠	٣٣٧٥	٣٣٧٥.١٦	-٠.١٥٩	-٠.٠٠٤٧
٤٥٠	٣٧٩٠	٣٧٩٠.١١	-٠.١٠٧	-٠.٠٠٢٨
٥٠٠	٤٢٠٠	٤٢٠٠.٠٥	-٠.٠٥٥	-٠.٠٠١٣
٦٠٠	٥٠٣٥	٥٠٣٤.٩٥	-٠.٠٥٥	-٠.٠٠١٠

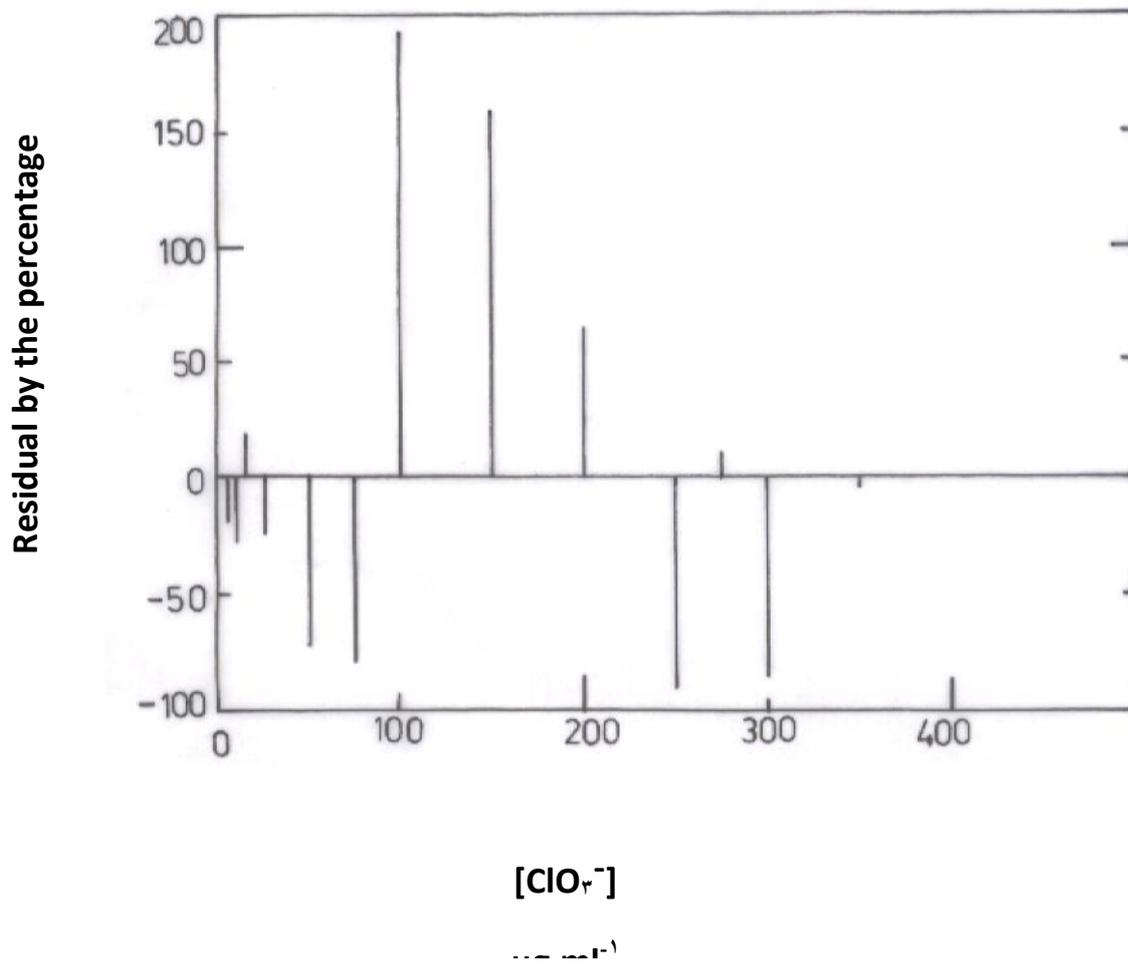


Figure (4-24): Indicating value of residual response that obtained practically (y_i) from predicated response (obtained on it from linear equation (\hat{y}_i)) by percentage

ξ B-۲-۳: Detection limit:

Whereas detection limit is less concentration and the given response is higher than response of blank solution with amount (γS_B), therefore there are three ways to determine detection limit:

۱. From gradually dilution for less concentration has been obtained from calibration curve is ($\rho \cdot \mu\text{g}\cdot\text{ml}^{-1}$) this dilution lead to moving toward low concentrations ($\lambda \cdot \mu\text{g}\cdot\text{ml}^{-1}$) by using the volume of sample injection ($\tau \cdot \mu\text{l}$).

$$\because \chi = 1\mu\text{g}\cdot\text{ml}^{-1}$$

$$\because \chi = 0.06 \mu\text{g}/60 \mu\text{l}$$

$$= \tau \cdot \text{ng}/\tau \cdot \mu\text{l} = \text{D.L}$$

This given response can be sensed and higher than response of distilled water by amount (γS_B) and with intensity ($\rho \gamma$ mV) as indicated in figure

(ξ-۲۵).

۲. By depending on the value of slope::

$$D.L = \frac{3S_B}{\text{slope}} \Rightarrow \frac{3 \times 0.001 \text{ mV}}{8.299 \frac{\text{mV}}{\mu\text{g} \cdot \text{ml}^{-1}}}$$

$$\Rightarrow D.L. = 3.615 \mu\text{g} \cdot \text{ml}^{-1}$$

$$= 21.7 \text{ pg}/60 \mu\text{l}$$

3. From linear equation

$$Y = L.O.D = y_B + 3S_B$$

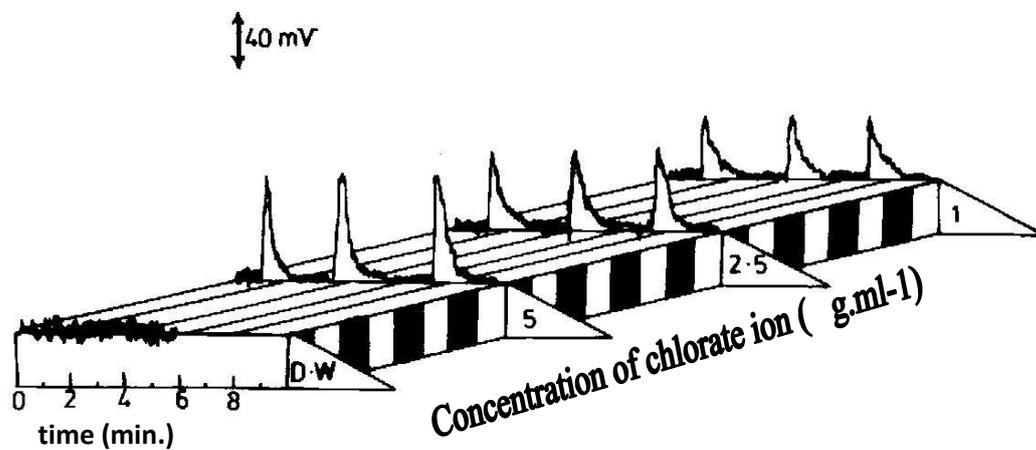


Figure (4-20) Detection limit for determination of chlorate ion for system $(\text{ClO}_3^- - \text{I}^- - \text{H}_2\text{O}^+)$ and from dilution moving toward low concentration by amount $6 \cdot \text{ng}$ for $6 \cdot \mu\text{l}$.

ξB-۲-ξ: The reproducibility:

The study in this unit is distinguished with high reproducibility, whereas the values of percentage for relative standard deviation was very small after fixing the optimum conditions of chemical variables: concentrations of sulphuric acid (۱.۰ M) and potassium iodide (۰.۱ M), and for changing concentration of injection sample and physical variables: volume of sample (۶.۰ μl), injection time (۶.۰ sec.) and flow rate (ξ ml.min⁻¹), and results are shown in table (ξ-۲۵) and figure (ξ-۲۶).

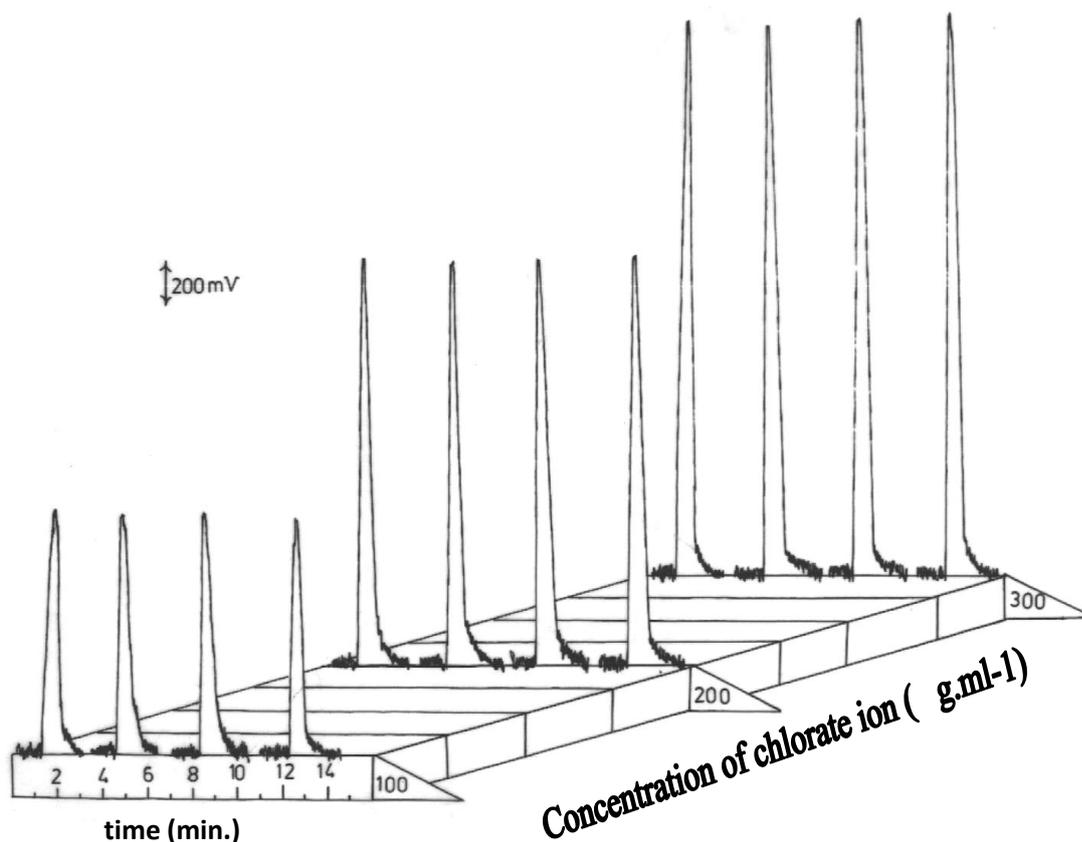


Figure (ξ-۲۶): Study of reproducibility through determination of chlorate ion for system (ClO_۳⁻-I⁻-H_۲O⁺)

Table (4-27): The results of reproducibility to measurement intensity of response for releasing iodine from system ($\text{ClO}_3^- - \text{I}^- - \text{H}_2\text{O}^+$).

$[\text{ClO}_3^-]$ $\mu\text{g.ml}^{-1}$	\bar{y} (mV)	Standard deviation σ_{n-1}	Reproducibility $\text{RSD}\% = \frac{\sigma_{n-1}}{\bar{y}} \times 100$	Injection No.	$\bar{y} \pm t_{0.05} \frac{\sigma_{n-1}}{\sqrt{n}}$ to n-1 and confidence limit 90%
100	1080	0.98	0.091	ξ	1080 ± 1.008
200	1780	1.32	0.074	ξ	1780 ± 2.098
300	2470	2.00	0.104	ξ	2470 ± 4.004

4 B-3: Effect of interferences

Although methods of continuous flow injection are sensitive methods and through it moving toward low concentrations but exposed to interfering for many of positive and negative ions and in this study chlorate ion was determined and it's oxidant material and influenced with finding many of interference ions and this effect on the shape and intensity of the response, therefore should after fixed all variables study effect other of cations, such as

Fe (II), Ni (II), Zn (II), Cr (II), Co (II)

And anions, such as

NO_3^- , $\text{Cr}_2\text{O}_7^{2-}$, CrO_4^{2-} , Br^- , Cl^- ,

And this study was done by using constant concentration of chlorate ion ($100 \mu\text{g.ml}^{-1}$) in three bottles which have capacity (100 ml) contain changing of concentration for interferences ions ($20, 0.0 \mu\text{g.ml}^{-1}$) in bottles (2, 3) and first bottle was prepared that contain chlorate ion is reference to compare with variable concentration of interference ion by finding chlorate ion in bottles 2,

3, injected of reference solution and other solutions for three times sequentially caused increasing in response of reference that compare with responses obtained from solutions contain interference ion to calculate percentage for interference or response of chlorate ion of unit ($\text{ClO}_3^- \cdot \text{I}^- \cdot \text{H}_2\text{O}^+$) in tables (4-28), (4-29).

That show percentage of interference effect for positive and negative ions with small value of relative standard deviation.

Table (4-28): Effect of cation interferences on height response for system ($\text{ClO}_3^- \cdot \text{I}^- \cdot \text{H}_2\text{O}^+$) by percentage of interfering effect.

Conc. of interference ion ($\mu\text{g} \cdot \text{ml}^{-1}$)	Percentage of interfering effect (%)				
	CO^{+2}	Zn^{+2}	Cr^{+3}	Ni^{+2}	Fe^{+2}
20	-1.08	+1.30	-7.20	+1.06	-70.82
50	-12.69	+2.98	-7.03	+3.13	-70.89

Table (4-29): Effect of Anion interferences on height response for system ($\text{ClO}_3^- \cdot \text{I}^- \cdot \text{H}_2\text{O}^+$) by percentage of interfering effect.

Conc. of interference ion ($\mu\text{g.ml}^{-1}$)	Percentage of interfering effect (%)					
	IO_3^-	$\text{Cr}_2\text{O}_7^{2-}$	NO_3^-	CrO_4^{2-}	Cl^-	Br^-
20	+3.17	+11.11	+80.71	+4.76	-2.03	-40.01
0.1	+11.11	+34.92	+114.29	+20.63	-32.91	-43.04

The cation interferences can be removed by putting small column before entering the loop or by putting resin to solution before entering the unit of flow injection analysis, while anion interferences can not remove the interference.

4B-4: Standard addition method and applications:

After fixing optimum condition, the sample of hypochlorate which is used is homemade from Babylon company of soap and detergent for limited industry-Baghdad, and pull a constant volume from it (0.1 ml) in five volumetric flasks, the first flask was prepared and contains enough sample solution, while the rest of the flasks are added to each one gradually, increasing of volume chlorate ion for obtaining finally on changing concentrations of chlorate ion (20, 0.1, 70, 100 $\mu\text{g.ml}^{-1}$). In addition it contains constant volume of sample solution as shown in table (4-30).

Table (٤-٣٠): Results of additions by standard addition method

No. of Bottles	١	٢	٣	٤	٥
Volume of sample (ml)	٠.١	٠.١	٠.١	٠.١	٠.١
[ClO _٢ ⁻] μg.ml ^{-١}	-	٢٥	٥٠	٧٥	١٠٠
Type of solution	Sample solution	Standard solutions + sample solution			

The complete flask to (١٠٠ ml) by distilled water after that measured the sample and obtained results in table (٤-٣١); the measurement was repeated for three times.

Table (٤-٣١): Changing the response with concentration by standard addition method.

[ClO _٢ ⁻] μg.ml ^{-١}	Response height (ȳ) mV	σ_{n-1} %RSD	$\bar{Y} \pm t_{0.05} \frac{\sigma_{n-1}}{\sqrt{n}}$
Sample solution	١٧٠٠	١.٢٣ ٠.٠٧٢	١٧٠٠ ± ٣.٠٥٥٨
٢٥	١٩٠٠	٢.٣٣	١٩٠٠ ± ٥.٧٨٨٦

		$\cdot.122$	
50	2100	5.00	2100 ± 12.4220
70	2300	3.12	2300 ± 7.7013
100	2460	2.00	2460 ± 6.3302

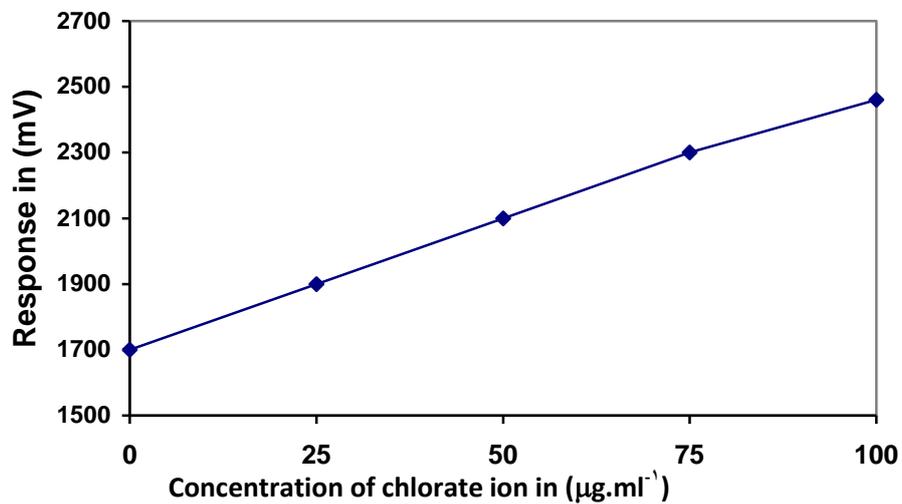


Figure (ξ-27): Determination the concentration of chlorate ion in hypochlorite solution.

ξ B-0 - Comparison between the first unit and the second unit

From the results of two units, figure (ξ-27 a) shows that unit A is good sensitive and correlation coefficient of it ($\cdot.9998$).

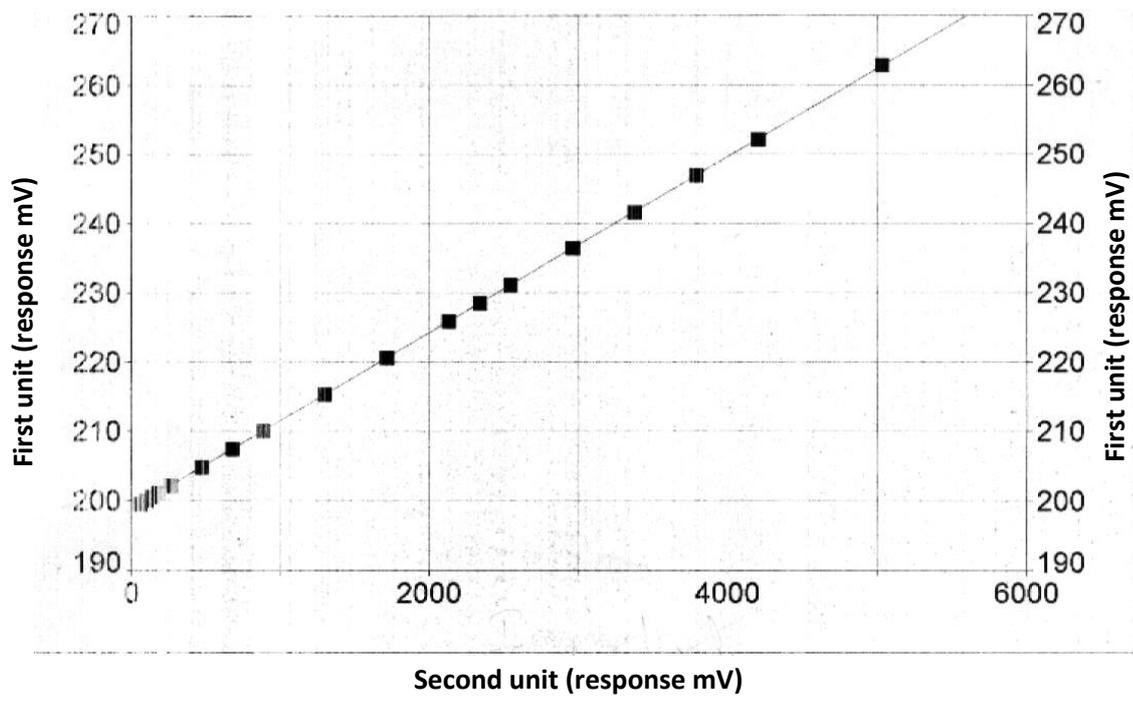


Figure (٤-٢٨ a): The unit is good sensitive

While figure (ε-٢٨ b) shows that unit B is more sensitive and high linearity because of negative intersection and correlation coefficient of it (٠.٩٩٨٨).

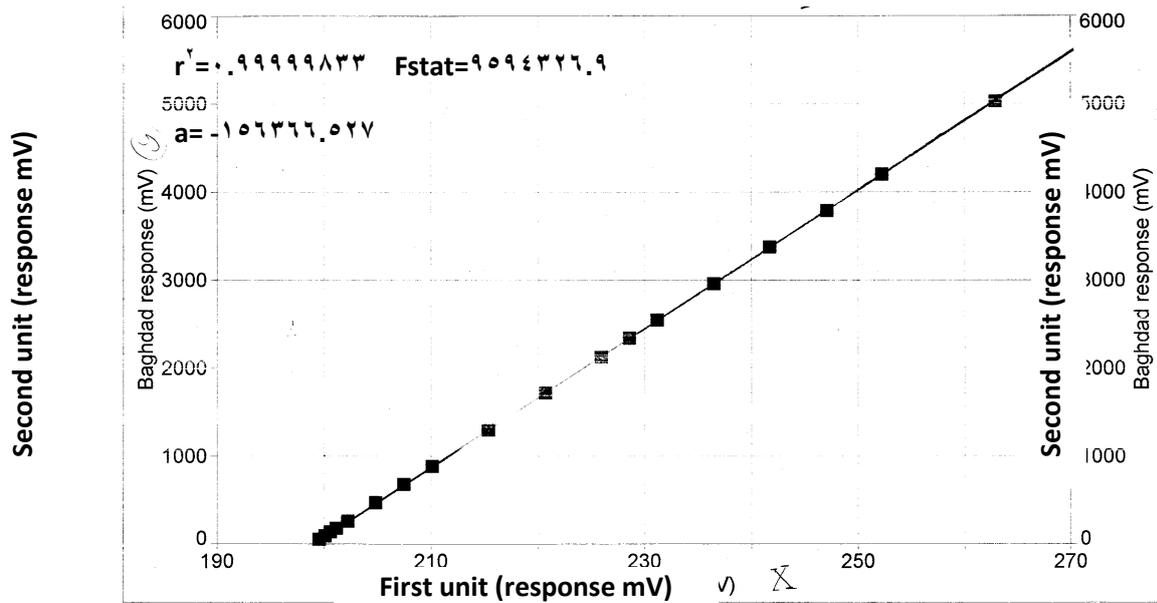


Figure (ε-٢٨ b): Show the first and second unit

Figure (ε-٢٨ c) shows that calibration curve form both units which explain the high sensitivity of unit b compared with unit a.

The sensitivity of unit b is larger than ٧^٩ time of unit a and the linearity of unit b is best for same range of concentration.

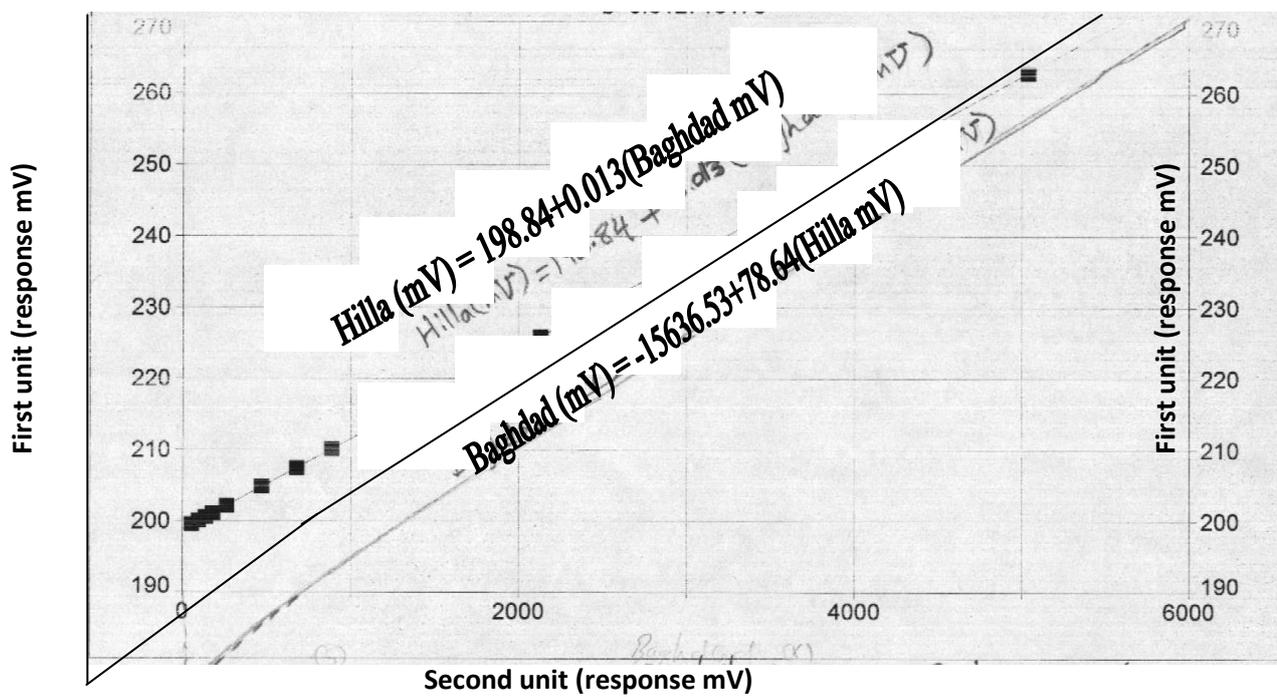


Figure (ε-٢٨ c)

Figure (a,b,c) Comparison between two units of the rule of response

Figure (a,b,c) shows the value of y (y predicted) for the two units which indicate the sensitivity of the both units

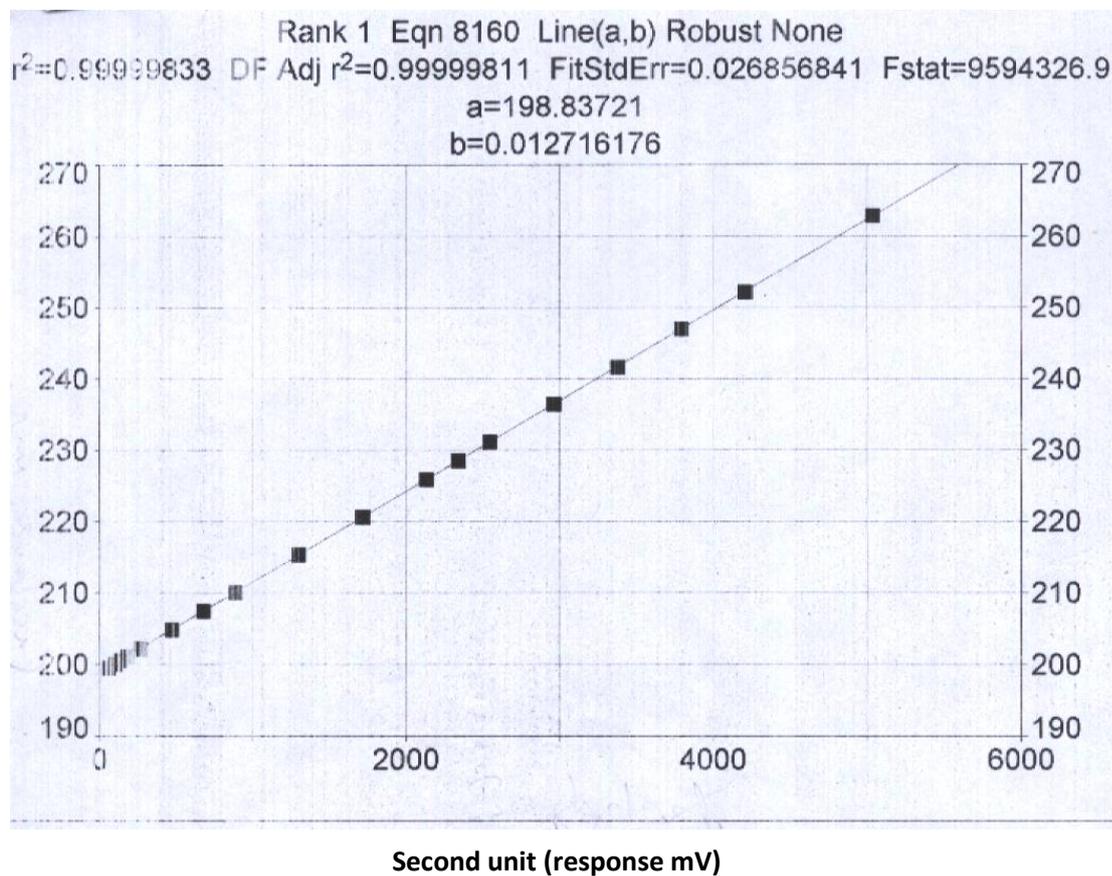


Figure (٤-٢٩ a): Comparison between two units of y (y predicted)

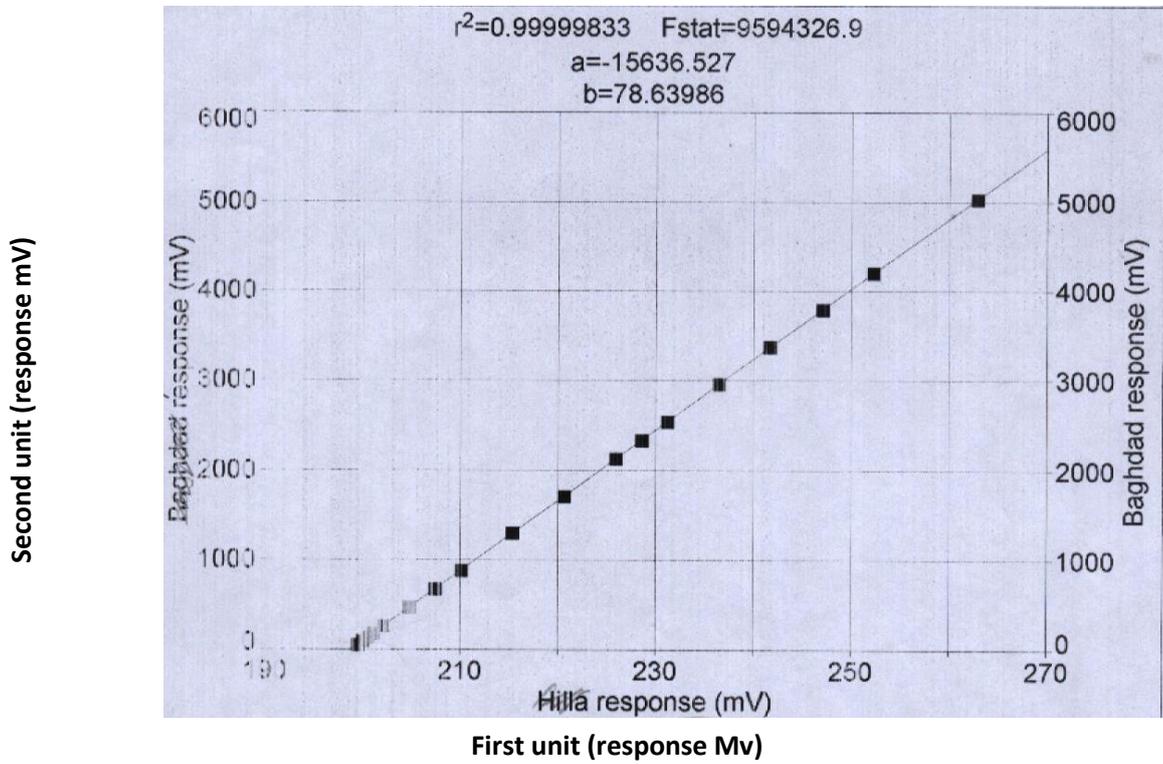


Figure (٤-٢٩ b)

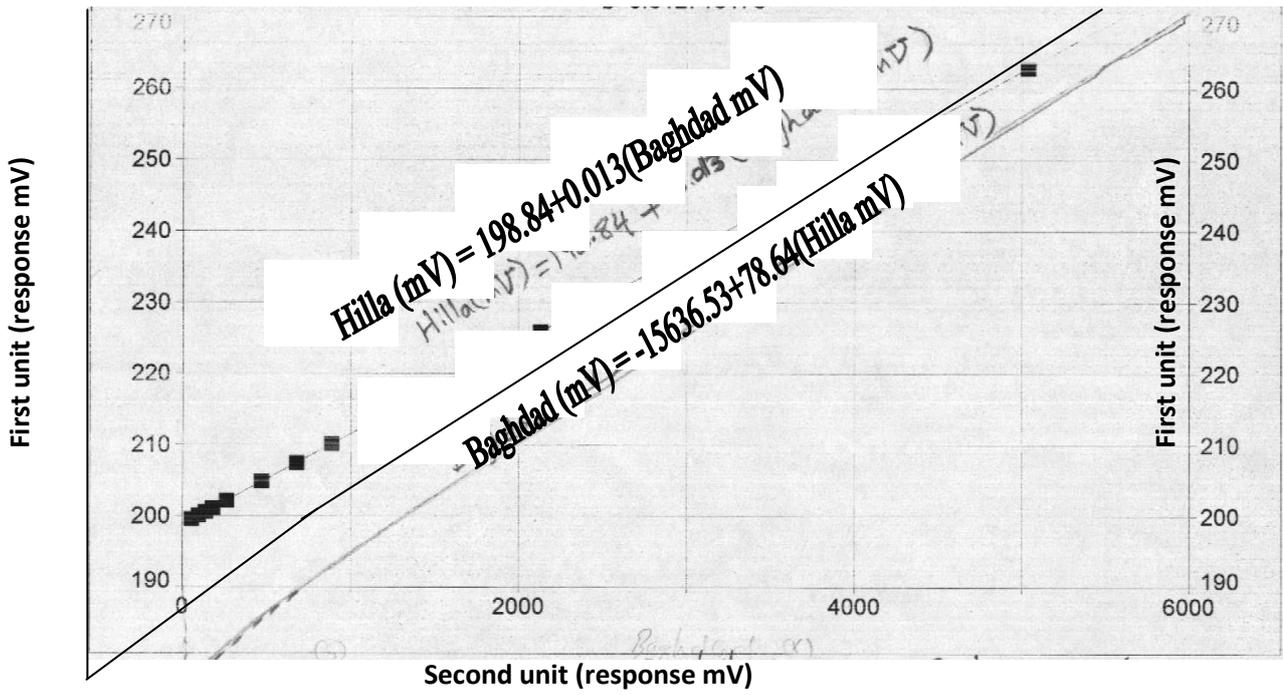


Figure (٤-٢٩ c)

Figure (٤-٢٩ a,b,c) Comparison between two units of \bar{y} (y predicted)

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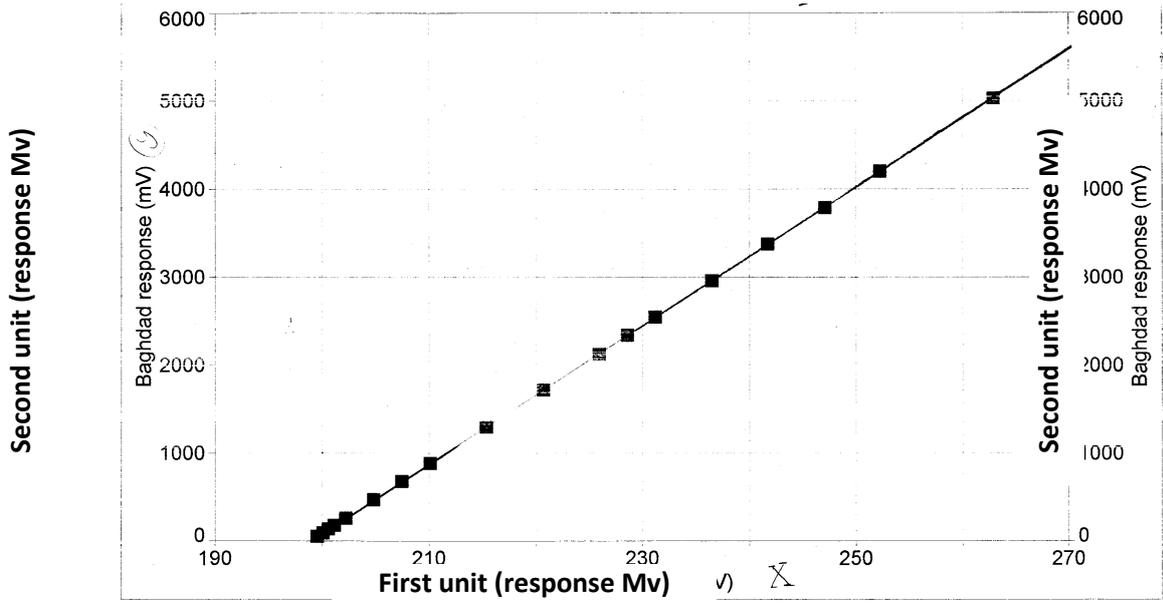
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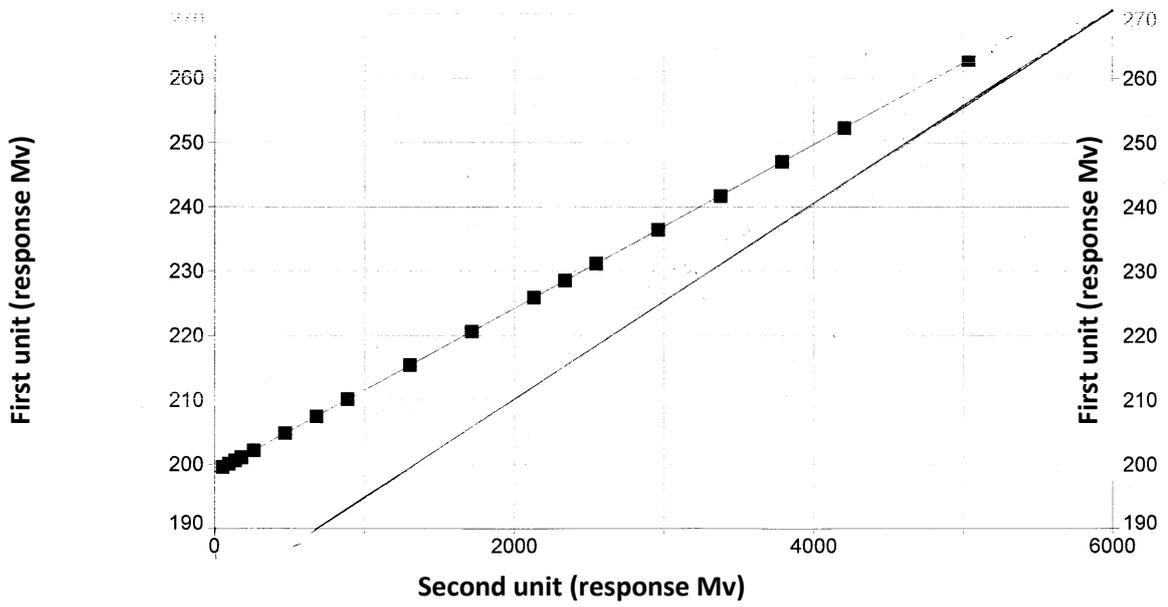
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$$r^2 = 0.99999833 \quad \text{Fstat} = 9094326.9$$

$$a = -106366.027$$



(4-b)



Y_i practically (mV)	.	8.	112	200	240	400	700	1080	1460	1780	2040	2349	2460	2907	3370	3790	4200	0.30
\hat{y} predicted (mV)	00.0 8	97.0 8	138.0 07	180.0 06	223.0 00	270.0 03	318.0 00	380.0 48	430.0 42	470.0 37	513.0 32	5337 79	5040 26	4960 21	3370 10	3790 10	4200 00	0.34 94
$\bar{y}_i - 1\sigma$	$n-1$ 3.00	38.7 3	81.0 0	123.0 27	167.0 76	218.0 82	279.0 06	339.0 92	399.0 18	457.0 00	509.0 03	5296 03	501.0 44	491.0 79	3318 69	3720 63	4131.0 91	4943 24
$\bar{y}_i - 2\sigma$	$n-1$ 44	- 79.6 9	- 37.9 4	38.0 9	87.2 8	190.0 80	204.0 20	312.0 01	328.0 04	404.0 93	490.0 67	5160 79	5372 70	4787.0 19	3199 01	3611 23	4022.0 87	4844 06
σ_{n-1}	.	0.32	0.11	0.10	0.33	2.10	1.40	2.00	1.90	2.00	2.00	2.30	2.11	2.09	2.40	2.19	1.87	2.40