

Preparation and Characterization of Concrete Reinforced by the Super-Absorbent Hydrogel Nano Composites (SAHNCs) Used for Construction Applications

¹Sihama I. Salih, ¹Fadhel A. Hashem, ²Auda J. Braihi

¹Materials Engineering Department, University of Technology, Baghdad, Iraq.

²Babylon University-College of Materials Engineering, Babylon, Iraq.

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Address For Correspondence:

Sihama I. Salih, Materials Engineering Department, University of Technology, Baghdad, Iraq.
E-mail: sihama_salih@yahoo.com

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ABSTRACT

In this research cementitious hybrid composites were prepared by addition of super-absorbent hydrogel nano composites (SAHNCs) to the concrete and mortar pastes. The SAHNCs is composed of carboxymethyl cellulose / starch blend loaded with 0.3 wt % of nano graphite oxide and its absorbency reaches to 69 g/g. Concrete cubes have dimensions of 15x15x15 cm with a fixed cement: sand: gravel ratios (1:1.18:1.86) and the ratio of water to cement is 0.4. The SAHNCs was added to concrete cubes with 0.2, 0.4, 0.6, 0.8 and 1 wt%. Mortar cubes have dimensions of 70.7x70.7x70.7 mm with 1:3 ratio of cement: sand and 0.40 ratio of water: cement. The SAHNCs loading in mortar are 0.1, 0.2, 0.4 and 0.6 wt%. Compression and ultrasonic pulse velocity (UPV) tests were used to evaluate the compressive strength for these hybrid cementitious composites. UPV was also used to evaluate their elastic constants and qualities. Consistency and setting times of mortar paste were measured by Vicat apparatus. Acoustic impedance, portions of the energy reflected and the energy transmitted were calculated using the steel as the second medium. Results showed that compressive strength for both concrete and mortar decreased firstly and then exceeds their initial values when the addition ratio of SAHNCs exceeds 0.6 wt% in concrete, and exceeds 0.3 wt% in mortar. The additional amount of water to get the standard consistency seems to be reasonable. Initial and final setting times of mortar increased with SAHNCs content except at 0.2 wt%. Elastic modulus exceeds its initial value at 0.6 wt% for concrete and at 0.5 wt% for mortar. Shear modulus for concrete increased at higher ratios and there is some fluctuations in mortar shear modulus. Most values of Poisson's ratios are within the typical range for standard concrete. Concrete quality for all samples is excellent according to the BS, 1881, 1983 code because all the longitudinal velocities are more than 4500 m/sec. The acoustic impedance increased, while the energy reflected reaches to its minimum value at higher SAHNCs ratios and the energy transmitted reaches to its maximum value.

KEYWORDS: Superabsorbent hydrogel nano composites, Concrete, Compressive strength, Ultrasonic pulse velocity, Acoustic impedance.

INTRODUCTION

Superabsorbent polymers (SAPs) are hydrophilic networks that can absorb and retain huge amounts of water or aqueous solutions and the absorbed water is hardly removed under some pressure [1]. Superabsorbent hydrogel nano composites (SAHNCs) are formed from incorporation of clays and organo-modified clays into superabsorbent polymers formulations [2]. These materials consist of a network of polymer chains that are

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cross-linked to avoid dissolution. Usually there are ionic functional groups along the polymer chains to encourage diffusion of water within the network[3].

The hydrophilic groups are hydrated in an aqueous environment, thereby creating a hydrogel structure[4]. Due to their swelling properties, so, these hydrogels can be utilized in many applications, such as in drug delivery systems[5], agriculture [3], separation processes [6] and others. In cementitious hybrid composites (concrete and mortar), SAHNCs used as additives to:

- 1- Improve concrete performance by acting as a water-reducing agent.
- 2- Eliminate the negative effect of water on the hardening of cement.
- 3- Act as an air-entraining agent by virtue of its polar nature which may reduce surface tension and hence stabilize the fine foam of bubbles originating from the mixing process[7].
- 4- Prevent or reduce self-desiccation (or autogenous shrinkage) during hydration [8]. They rapidly absorb water (forming water-filled cavities), then release it when cement paste self-desiccates or is exposed to drying [9].
- 5- Promote internal curing of concrete to mitigate its autogenous shrinkage [10]. The water gel created in the fresh concrete by the use of SAP provides cushioning and lubrication in the concrete mass, which in turn improves the concrete workability as well as concrete stability[11].

Consistency of standard paste for any given cement determines the water content of the paste which will produce the desired consistency.

Setting process involves losing of plasticity with time and becoming dense and stiff. It refers to a change from a fluid to a rigid state and happened in two stages; initial setting and final setting [8]. Initial setting time refers to the beginning of solidification, while final setting time refers to the beginning of hardening process.

Setting is important in concrete work to keep fresh concrete plastic for enough time which helps the processes of transporting, casting, and compaction. Setting times influenced by many factors, such as: fineness types of cement, age, water content, temperature, and humidity.

Ultrasonic pulse velocity (UPV) method used to evaluate the quality of concrete and mortar as well as to calculate the elastic constants. The idea is to project the sound inside a material and measure the time necessary for the wave to propagate through it [12]. The ultrasonic pulses depend on the density and elastic properties of the material.

UPV method was used to measure times required to transport the ultrasonic pulse wave in the longitudinal and transverse paths; t_L and t_T . Then, these two times were substituted in Equations 1 to 6 to calculate the longitudinal and transverse ultrasonic velocities (V_L and V_T respectively) as well as the elastic constants such as, elastic modulus (E), shear modulus (G) and Poisson's ratio (ν) for both the concrete and mortar cubes [13].

$$V_L = (L/t_L) \times 10 \quad (1)$$

$$V_T = (d/t_T) \times 10 \quad (2)$$

$$\rho = W / V \quad (3)$$

$$E = \rho \times V_L^2 \quad (4)$$

$$G = \rho \times V_T^2 \quad (5)$$

$$\nu = (E/2G) - 1 \quad (6)$$

Where

t_L : Time for longitudinal pulse (μs), t_T : Time for transverse pulse (μs)

L : Length of cube (15 cm for concrete and 7.07 cm for mortar)

d : Width of cube (10.6 cm for concrete and 5 cm for mortar)

ρ : Density (g/cm^3), W: Weight (g)

V: Cube volume (3375 cm^3 for concrete and 353.4 cm^3 for mortar)

As well as, UPV measurements can be used to:

1. Determine the uniformity of concrete in and between members.
2. Measures of changes occurring with time in the properties of concrete [14].
3. Evaluate concrete quality [12].
4. Using both the longitudinal velocity (V_L) and the density (ρ), the acoustic impedance (Z) was calculated by Equation 7 [15].

$$Z = \rho V \quad (7)$$

The Aim:

This research aims to prepare cementitious hybrid composites reinforced by the super-absorbent hydrogel nano composites (SAHNCs) and their characterization study.

*Experimental Part:**Materials:**Super-absorbent hydrogel Nano composites (SHNCs):*

This material is prepared from composed of carboxymethyl cellulose (CMC) / starch blend cross-linked by alum and loaded with 0.3 wt% nano graphite oxide (GO). Free water absorbency of this material reaches to 69 g/g and reaches to 29 g/g under 2.068 KPa load. This polymeric blend contains 1.5 wt% alum cross-linker.

Ordinary Portland Cement (OPC):

used in this research, have the chemical composition shown in Table 1.

Sand: The Properties, grading and chemical composition of the used sand are shown in Table 2.

Gravel: The grading and properties of the used gravel showed in Table 3.

*Preparations and testing:**1-Preparation and testing of concrete cubes:*

Concrete cubic samples have dimensions (15x15x15 cm) were prepared with a fixed cement: sand: gravel ratio of 1:1.18:1.86 according to ASTM C 192-90a with water/cement ratio equal to 0.4. The weight percent of SAHNC used are 0.2%, 0.4%, 0.6%, 0.8% and 1 wt%.

Cubic samples were subjected to humid environment for 24 hr, immersed in the water for another 27 day, then tested (compressive strength) according to ASTM C579-01 method B using impact machine of 2000 KN maximum capacity, resolution 1 KN, and loading rate 3KN/sec.

Table 1: Chemical composition of the used OPC

Oxide	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	SO ₃	Loss on Ignition (L.O.I)
%	22.01	5.26	3.3	62.13	2.7	2.4	1.45

Table 2: Properties and grading of the used sand

Property	Value
Fineness Modulus	2.51
SO ₃ %	4.45
Sieve Openings Size (mm)	Passing%
10.0	100
4.75	94.76
2.36	88.38
1.18	79
0.6	65.55
0.3	17.17
0.15	3.79

Table 3: Grading and properties of the used gravel

Property	Value
SO ₃ %	0.095
Sieve Openings Size (mm)	Passing%
3.75	100
20	70
14	40
10	10
5	0

2-Preparation and testing of mortar Cubes:

Mortar cubic samples have dimensions (70.7×70.7×70.7 mm) were prepared according to BS 4550-3.4:1978 with 1:3 ratio of cement:sand, 0.40 ratio of water:cement and the mass of water in the mix is 10 percent of the mass of the dry materials. The SAHNC loading ratios are 0.1, 0.2, 0.4 and 0.6 wt%, as shown in Table 4. These ratios were calculated as a percent to the cement weight.

Table 4: Ingredient of mortar samples

Cement (g)	Sand (g)	Water (ml)	SAHNC	
			%	(g)
200	600	80	0	0
199.8	600	80	0.1	0.2
199.6	600	80	0.2	0.4
199.2	600	80	0.4	0.8
198.8	600	80	0.6	1.2

Then, these ingredients were mixed for four minutes using a spark mixer and the resultant mixture was further mixed by a vibrating machine with a frequency of 200 Hz for another four minutes. Cubic samples were

subjected to humid environment for 24 hr and immersed in the water for another 27 day before testing using either impact machine or UPV methods.

3-Preparation and testing for consistency and setting times purposes:

In order to measure the consistency and the setting times by Vicat apparatus, neat cement pastes were prepared. These pastes include fixed weight of cement (400g) and variable amounts of water. These two components were mixed carefully for four minutes and then moulded in the cylindrical mould before testing.

The consistency is measured using a 10 mm diameter plunger (BS EN 196-3: 2005). The plunger is brought into contact with the top surface of the paste and released. Paste is considered to be standard when the plunger penetrates the paste to a point 6 ± 1 mm from the bottom of the mould. The water content of the standard paste is expressed as a percentage by mass of the dry cement, the usual range of values being between 26 and 33 per cent [9].

The setting times of cement are measured using different penetrating attachments (BS EN 196-3 : 2005) [9]. For the initial set, a round needle with a diameter 1.13 ± 0.05 mm is used. When the paste stiffens sufficiently for the needle to penetrate no deeper than to a point 5 ± 1 mm from the bottom, initial set is said to have taken place. Final set is determined by a similar needle fitted with a metal attachment hollowed out so as to leave a circular cutting edge 5 mm in diameter and set 0.5 mm behind the tip of the needle. Final set is said to have taken place, when the needle, gently lowered to the surface of the paste, penetrates it to a depth of 0.5 mm but the circular cutting edge fails to make an impression on the surface of the paste.

Ultrasonic Pulse Velocity (UPV) Test:

In order to measure the elastic constants for hybrid cementitious composites, the non-destructive UPV test was adopted. This test uses the CSI type CC-4 tester with 26000 Hz with aluminum reference bar which possess a $32.5 \mu\text{s}$ transition time. Test equipment generates a pulse which transmits through the concrete mass, then receiving the pulse to measure the elapsed time. UPV outputs was also utilized to evaluate the quality of concrete and mortar according to the IS code (BS, 1881, 1983) as well as to calculate the elastic constants [14]. In this test, two transducers arrangements were used; opposite faces (direct transmission) to measure V_L and adjacent faces (semi-direct transmission) to measure V_T .

RESULTS AND DISCUSSIONS

1- Compressive Strength (CS):

The effect of addition SHNCs to concrete and mortar on the behavior of compressive strength (CS) are shown in Figures 1 and 2 respectively. It is clear from figure 1 that CS of concrete was decreased from 40.2 MPa for pure concrete to 35.9 MPa when the addition of (SAHNC) in concrete reach to ratio of 0.4% wt.

This behavior is due to the competition between the cement paste and SAHNC particles to absorb the available water. This competition leads to reduce the hydration reaction between cement and water (decreasing in H-bonds formed between cement paste and water), therefore CS will decrease. The reduction in the hydration reaction results also in the formation of entraining pores. These pores were initially filled with the curing water and then dried out; therefore, these voids affect the CS negatively.

Beyond the 0.4wt% SAHNCs, the CS increased up from 35.9 MPa to 45.8 MPa when the (SAHNC) content in the concrete reach to ratio of 1 wt % which means there are 14% increasing compared with the pure concrete. This new manner is due to the fact that the negative influence of additional voids induced by the addition of SAHNC particles was compensated by the improved degree of hydration and the self-curing effect in the matrix containing 0.4wt% SAHNC. Also, loading levels from 0.4 to 1wt% lowering the internal stresses due to the hindrance of shrinkage deformations by stiff aggregates [8].

Results of these two behaviors are in a good agreement with Dudziak and Mechtcherine conclusions which were reported in [10]. Also, this overall enhancement in the compressive strength property results coincides with results of both Gao et al (12.3% increasing) and Hareendran et al (10.6% increasing) [10].

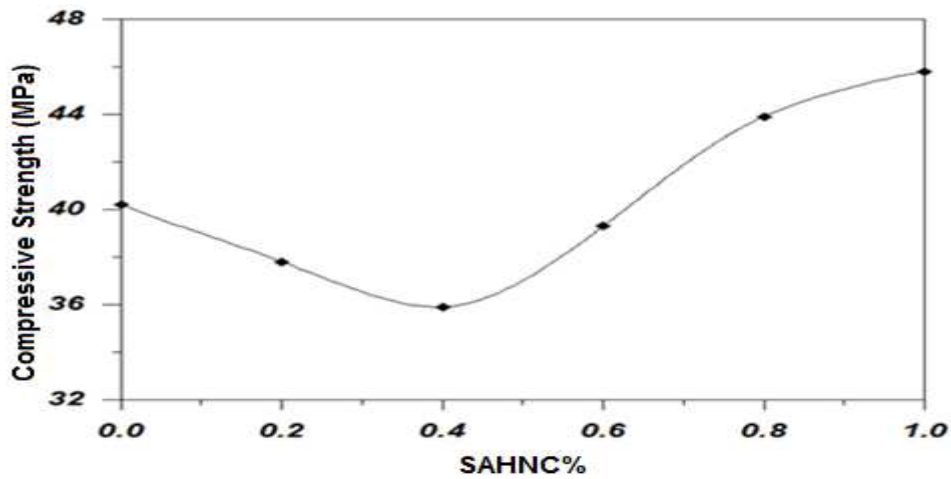


Fig. 1: Compressive strength of concrete hybrid composites as a function of SHNCs content

Effects of SAHNCs addition on the mortar CS are shown in Figure 2. Through this figure, a decrease is noted at the first in CS, especially at 0.1wt% of SAHNCs from 41.5 MPa (for pure sample) to 40.1 MPa with the addition of 0.1wt% SAHNCs. After that, the CS increased with any increasing in the SAHNC contents. Highest CS value was obtained at the 0.5wt% ratio of SAHNCs (42 MPa), then it became stable.

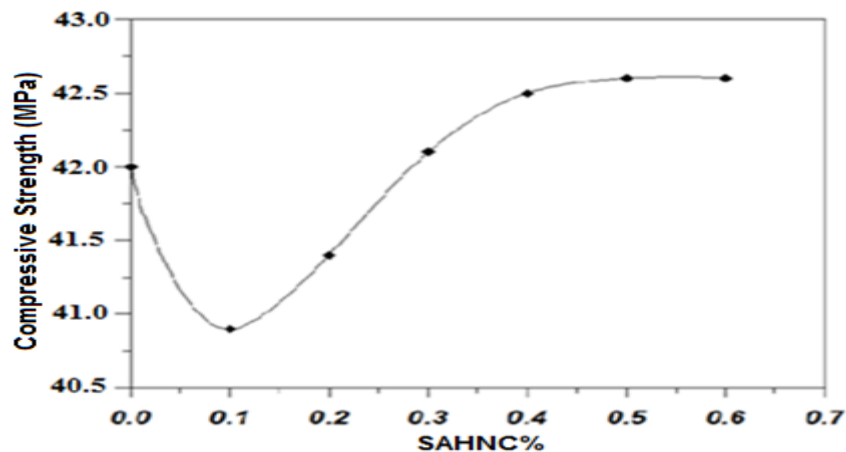


Fig. 2: Compressive strength of mortar hybrid composites as a function of SHNCs content

By comparing the two previous curves in figures 1 and 2, a similarity is observed in the concrete and mortar behaviors of the curves, except there is stability in the mortar compressive strength at higher SAHNC levels.

2. Consistency of Standard Mortar Paste Test:

Consistency of cementitious paste is considered a critical property because of its strong relation with water amount in the paste. Certain quantity of water is required for hydration process and to obtain the desired rheological properties for proper mixing, compacting and transporting. Increasing water content causes segregation, bleeding, increased porosity of the hardened concrete, reduction in the mechanical performance, reduction in durability, increased shrinkage and increased creep deformations. Therefore, there is a real need to control the water content in the paste.

Figure 3 shows the effect of SAHNC ratios on the amount of additional water required to obtain the standard consistency of the mortar paste. From this figure, it was found that these additional amounts increased with the increasing SAHNC content, and reached to maximum level with 0.6 wt % SAHNC ratio. So, these amounts of the required water increased from 110 ml for the reference mortar paste (without SAHNCs) to 150 ml for the paste with 0.6wt% SAHNC.

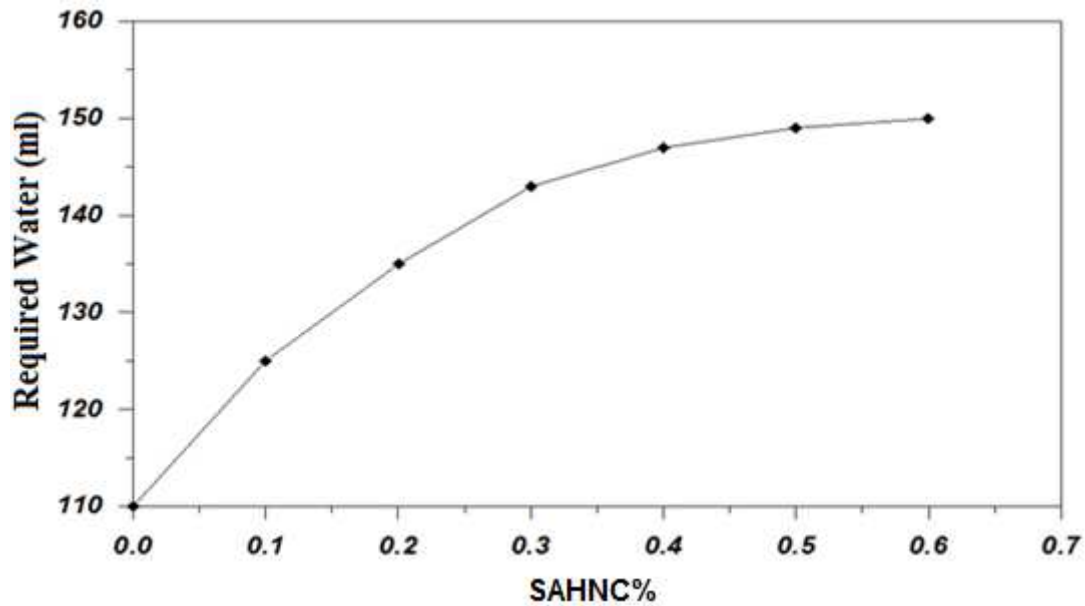


Fig. 3: The amount of additional water required to obtain the standard consistency of the mortar paste as a function of SAHNC content

This amount of additional water; 40 ml, seems to be reasonable, since the excessive amount (more than 160 ml) added to the fresh concrete alters its properties (reduces both its strength and workability, increases its shrinkage). Also, it seems to be reasonable from economical viewpoint.

3. Setting Times Results:

Setting time is an important factor in concrete work to keep fresh concrete plastic for enough time, which helps the processes of transporting, casting, and compaction. Initial setting time refers to the beginning of solidification, while final setting time refers to the beginning of hardening process. The initial and final setting times of the pure sample, and the effect of the addition of SAHNC with ratios of 0.2, 0.4, 0.6, and 0.8 wt% are shown in Table 5. It is clear that these two times have the same behavior; they increased linearly with the SAHNC ratios except at 0.2 wt% SAHNC. This indicates that SAHNC materials act as retarder at high concentrations.

Table 5: SAHNC effects on the setting times of mortar paste

SAHNCs %	Initial Set Time (hr min)	Final Set Time (hr min)
0	3 ⁴⁵	5 ⁴⁵
0.2	3 ¹⁵	5 ²⁵
0.4	4 ⁰⁰	5 ⁵⁰
0.6	5 ²⁰	6 ²⁰
0.8	5 ³⁵	6 ⁵⁰

The hydration of tricalcium aluminate ($3\text{CaO}\cdot\text{Al}_2\text{O}_3$) is responsible for the setting of cement [8]. Therefore, small internal water sources (corresponded to low SAHNC ratio; 0.2 wt%) cannot complete the hydration reaction. During hydration process, insoluble calcium or aluminum compounds are formed and interspersed through the crystalline mass. These compounds are not removable from the stiffened mass, thus retard the rate of absorption of H_3O^+ ions on cement surface and slow down the setting reaction [11].

4. Ultrasonic Pulse Velocity (UPV) Results:

The longitudinal and transverse ultrasonic velocities (V_L and V_T) were calculated according to Equations 1 and 2 respectively, as well as the elastic constants, such as elastic modulus (E) eq. 4, shear modulus (G) eq. 5 and poisson's ratio (ν) eq. 6 for both the concrete and mortar cubes, as shown in Tables 6 and 7 and figures from 4 to 9.

Table 6: Ultrasonic velocities and elastic constants for concrete cubes

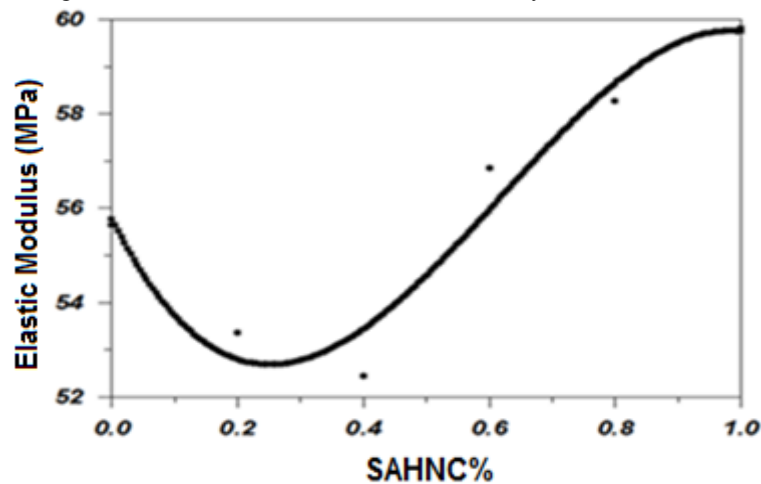
SAHNC %	ρ g/cm ³	t_L μ s	V_L Km/s	t_T μ s	V_T Km/s	E MPa	G MPa	ν
0	2.318	30.60	4.90	33.65	3.15	55.655	23.000	0.209
0.2	2.316	31.25	4.80	34.19	3.10	53.360	22.256	0.198
0.4	2.315	31.50	4.76	34.52	3.07	52.452	21.818	0.202
0.6	2.320	30.30	4.95	34.08	3.11	56.845	22.439	0.266
0.8	2.331	30.00	5.00	33.54	3.16	58.275	23.276	0.251
1	2.364	29.82	5.03	33.12	3.20	59.811	25.743	0.161

It is clear from Table 6 that for concrete hybrid composites with low SAHNC contents (up to 0.4 wt. %), the ultrasonic waves elapsed increasing times when transported through concrete cubes in both longitudinal and transverse directions.

In contrast, for hybrid composites with high SAHNC contents (0.6-1wt %), the ultrasonic waves elapsed decreasing times. So, V_L decreased from 4.9 Km/s for pure sample to 4.76 km/s for hybrid composite with 0.4 wt% SAHNC, and then increased up to 5.03 when the SAHNC content increased up to 1 wt%. In similar manner, V_T decreased from 3.15 Km/s to 3.07 Km/s then increased up to 3.2 Km/s in the same ratio.

These opposite two behaviors are due to heterogeneity and voids in hybrid composites with low SAHNC contents (up to 0.4 wt%). This heterogeneity arises from the presence of both hydrated and anhydrated portions in the cementinuous pastes; therefore the sound energy will dissipate and attenuate at the interfacial boundaries between these phases.

It was observed from Figure 4 that elastic modulus of concrete firstly

**Fig. 4:** Elastic modulus of concrete hybrid composites as a function of SAHNC content

decreased from 55.655 MPa for pure sample to 52.6 MPa for hybrid composite with 0.25 wt% SAHNC, and then increased up to 59.811 MPa for hybrid composite with 1 wt% SAHNC. These behaviors are due to insufficient amount of stored water to complete the hydration process with SAHNC ratios up to 0.4 wt%, and then water amounts be enough to complete the setting reaction. Therefore, concrete became stiffer.

Figure 5 shows the shear modulus as a function of SAHNC contents in hybrid concrete. It is clear that the shear modulus decreased from 23 MPa for pure sample to 21.8 MPa for hybrid composite having 0.4 wt% SAHNC, then increased up to 25.743 MPa when SAHNC content increased up to 1 wt%.

Declined values at low SAHNC contents are due the attenuation counter waves in voids which are available in the un-reacted zones. In contrast, when SAHNC contents are increased (more than 0.4 wt %), chemical reaction occurs through chemical bonds. This bonding increases the homogeneity between the composite ingredients and reduces the phase separation. Thus, waves elapsed short time, wave velocity becomes high and the shear modulus increased.

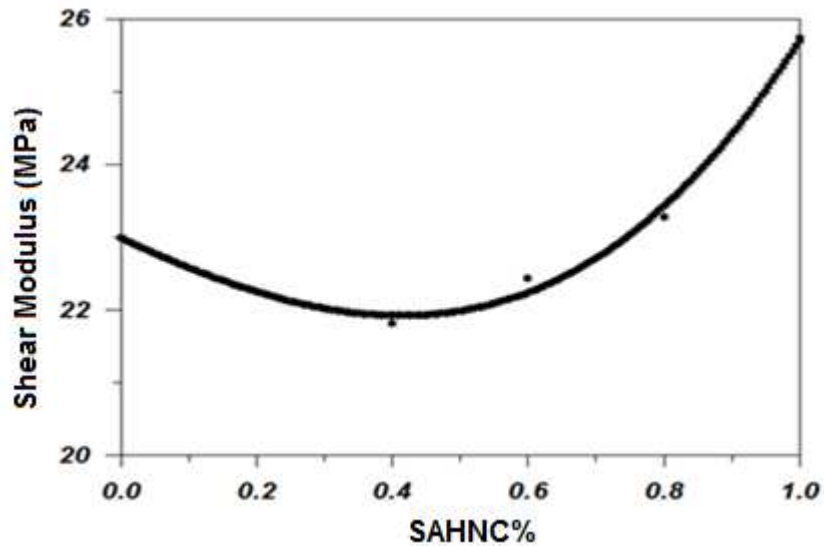


Fig. 5: Shear modulus of concrete hybrid composites as a function of SAHNC content

The effects of addition of SAHNCs on the Poisson's ratio of concretes hybrid composite was shown in Figure 6. It is clear from this figure that the variations in Poisson's ratio were limited to small range (0.161-0.252), which indicates that the longitudinal extension and the transverse contraction are equal.

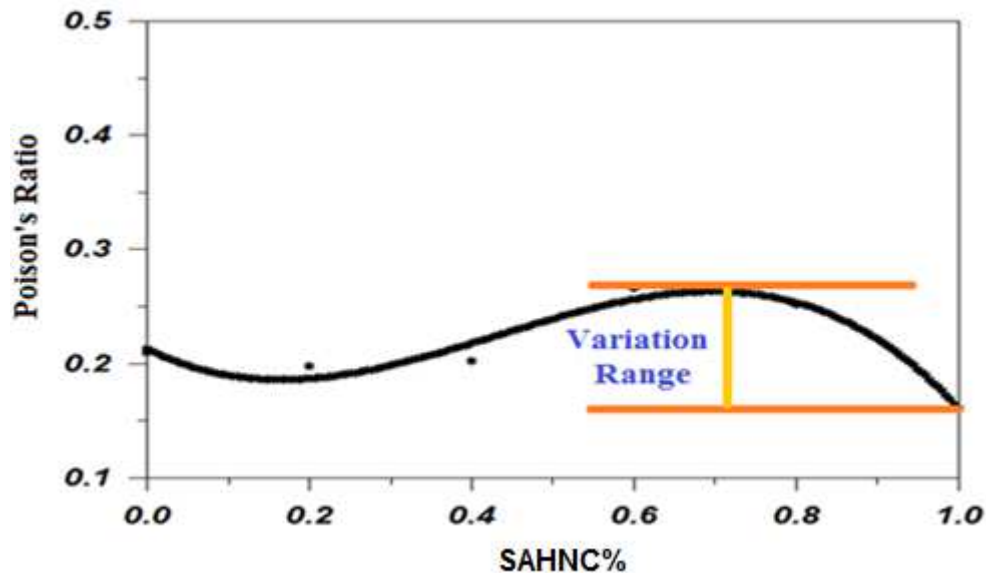


Fig. 6: Poisson's ratio of concrete hybrid composites as a function of SAHNC content

Furthermore, since the Poisson's ratio values, for concrete are within the range of 0.2- 0.35, and the typical value reaches to 0.24 [8], therefore the obtained Poisson's ratios considered as acceptable values except that for 1 wt% SAHNC.

Table 7 shows the values of ρ, V_L, V_T, E, G and ν for the mortar hybrid composites with different concentrations of SAHNC.

Table 7: Ultrasonic velocities and elastic constants for mortar cubes

SAHNCs %	ρ g/cm ³	t_L μ s	V_L km/s	t_T μ s	V_T km/s	E MPa	G MPa	ν
0	2.223	14.34	4.93	16.0	3.125	54.03	21.71	0.244
0.1	2.153	14.40	4.91	15.8	3.164	51.90	21.56	0.203
0.2	2.130	14.45	4.90	15.5	3.225	51.14	22.15	0.154
0.3	2.100	14.36	4.92	15.7	3.185	50.83	21.3	0.193
0.4	2.124	14.25	4.96	15.9	3.145	52.25	21.0	0.244
0.5	2.128	14.14	5.00	16.1	3.105	53.20	20.52	0.296
0.6	2.280	14.00	5.05	16.3	3.067	58.15	21.44	0.356

From Table 7, it is clear that the ultrasonic pulses elapsed times (t_L and t_T) in mortar cubes are less than times elapsed in concrete cubes mentioned earlier in Table 6. And, this is related to the dimensions of mortar cube that are less than the dimensions of concrete cube.

Also, it is clear that V_L decreased firstly from 4.93 Km/s for the pure sample to 4.9 Km/s for hybrid composite with 0.2 wt% of SAHNC, then increased up to 5.05 Km/s for sample with 0.6 wt% of SAHNC. Such trend (increasing V_L with SAHNC content) is in accordance with the works published by Winker and Nur, 1982; Ohdaira and Masuzawa, 2000 as well as by Veraara et al., 2001 [10].

The behavior of mortar elastic modulus shown in Figure 7, this modulus continues its decreasing from its initial value; 54.03 MPa (for pure sample) to reach its minimum value; 50.7 MPa at 0.3 wt% of SAHNC, then increases gradually to reach 58.15 MPa at 0.6 wt% of SAHNC. The elastic modulus exceeds its initial value only with the later ratio; 0.6 wt% SAHNC, which indicates that the hydration process completes only with this ratio.

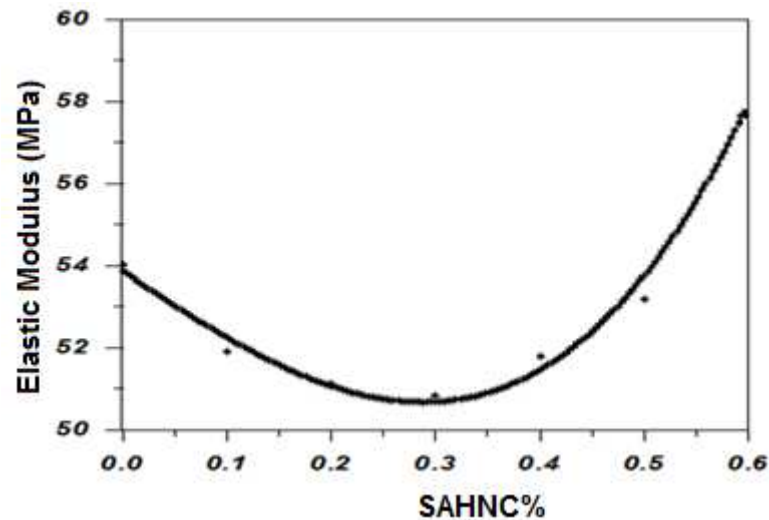


Fig. 7: Elastic modulus of hybrid mortar composite as a function of SAHNC content

Shear modulus values for mortar composite are shown in Figure 8. This figure shows the fluctuating behavior in shear modulus values with the increase SAHNC contents. Shear modulus reaches its maximum value at 0.2 wt% SAHNC, then reaches its minimum value at 0.5 wt% SAHNC and then increases at 0.6 wt% SAHNC to reach 21.44 MPa which is lower than its initial value. This means that the optimum SAHNC ratio in mortar paste is the 0.2 wt% from the shear modulus viewpoint.

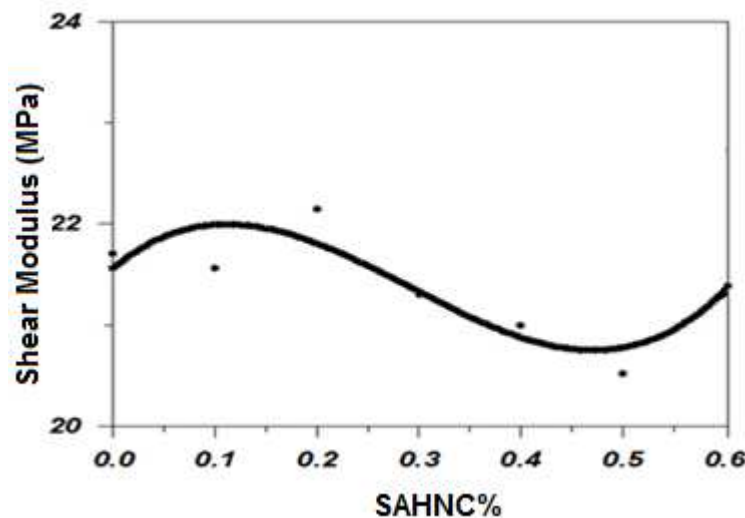


Fig. 8: Shear modulus behavior of mortar hybrid composite as a function of SAHNC content

Effects of SAHNC addition on the values of Poisson's ratio for mortar hybrid composites are shown in Figure 9. Firstly, there is a decrease from 0.224 value (for pure sample) to 0.193 value at 0.3 wt% of

SAHNC. Then, the Poisson's ratio increased with the increasing of SAHNC ratios reaching to 0.356 at 0.6wt% of SAHNC.

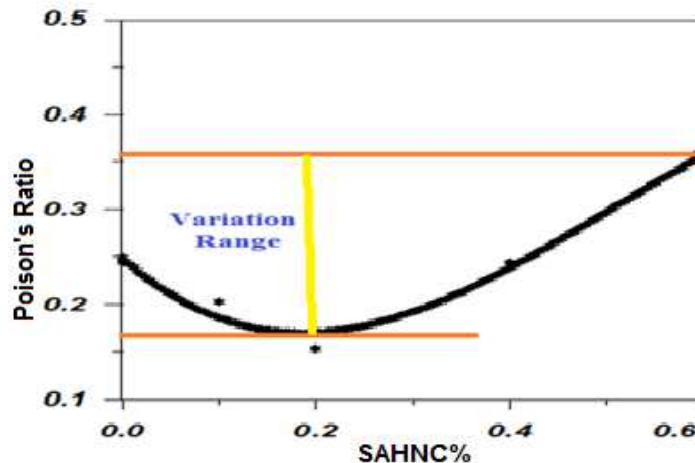


Fig. 9: Poisson's ratio of mortar hybrid composites as a function of SAHNC content

So the Poisson's ratios, seems to be more affected than those for concrete; its range extended from 0.154 to 0.356. The value corresponded to the 0.4wt% SAHNC; 0.244 seems to be a typical value.

5. Quality Evaluation:

All longitudinal velocities (V_L) for concrete and mortar hybrid composites are more than 4.5 Km/s ; more than 4500 m/sec as shown in Tables 6 and 7. Therefore the quality for all samples seems to be excellent according to the BS, 1881, 1983 code (Table 8)[13].

Table 8: Concrete quality as a function of UPV (BS, 1881, 1983)[13]

UPV(m/s)	Concrete Quality
Above 4500	Excellent
3500 to 4500	Good
3000 to 3500	Medium
Below 3000	Doubtful

These high velocities also indicate the high homogeneity and uniformity levels of pastes, which in turn mean the good dispersion of the SAHNCs in the hybrid cementitious composites.

6. Acoustic Impedance Results:

Using both the longitudinal wave velocity (V_L) and the density (ρ), the acoustic impedance (Z) for concrete and mortar was calculated according to Equation 8[14].

$$Z = \rho V \tag{8}$$

So, the acoustic impedance (Z) for concrete and mortar are shown in Figures 10 and 11 respectively.

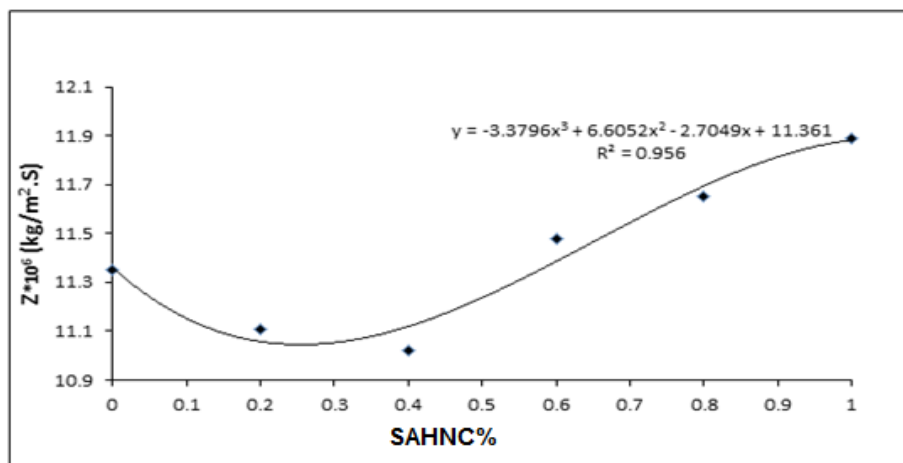


Fig. 10: Acoustic impedance for concrete as a function of SAHNC

The acoustic impedance of concrete samples (figure 10) decreased from $(11.35 \times 10^6 \text{ kg/m}^2 \cdot \text{s})$ for pure sample to reach $(11.02 \times 10^6 \text{ kg/m}^2 \cdot \text{s})$ for sample with 0.4wt% ratio of SAHNC, and then increased to its maximum value $(11.89 \times 10^6 \text{ kg/m}^2 \cdot \text{s})$ at 1wt% of SAHNC. These opposite two behaviors give evidence about the completing of hydration process at high SAHNC ratios.

Whereas, the acoustic impedance of mortar samples (figure 11) decreased from $(10.95 \times 10^6 \text{ kg/m}^2 \cdot \text{s})$ for pure sample to reach $(10.33 \times 10^6 \text{ kg/m}^2 \cdot \text{s})$ for sample with 0.3wt % of SAHNC, and then increased to $(11.5 \times 10^6 \text{ kg/m}^2 \cdot \text{s})$ at 0.6wt% SAHNC ratio.

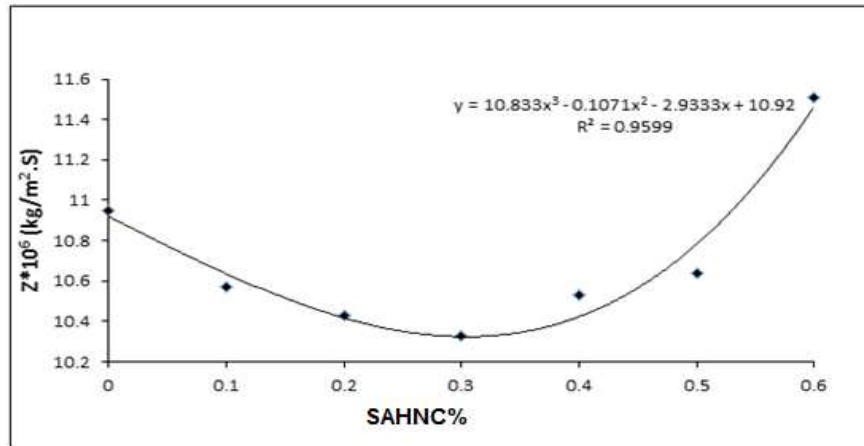


Fig. 11: Acoustic impedance for mortar as a function of SAHNC content

To determine the percentages of both the energy reflected (E_R) and the energy transmitted (E_T) when the wave projected on a plane between two media, steel ($Z = 45.41$) was used in this study as the second medium.

E_R and E_T were calculated according to Equations 9 and 10 respectively [15].

$$E_R = [(Z_1 - Z_2) / (Z_1 + Z_2)]^2 \times 100 \tag{9}$$

$$E_T = (4Z_1Z_2) / (Z_1 + Z_2)^2 \times 100 \tag{10}$$

The percentages of both the energy reflected (E_R) and the energy transmitted (E_T) are shown in Figures 12 and 13 for each of the concrete hybrid composite and mortar hybrid composite respectively. In both two figures, E_R reaches to their minimum values at higher SAHNCs ratios while E_T reaches to their maximum values at higher ratio of SAHNCs. This means that at higher SAHNCs ratios content, the energy will dissipate due to high porosity levels. Also, both figures contain a maximum point in both E_R and E_T which support that the maximum hydration levels occur at these points.

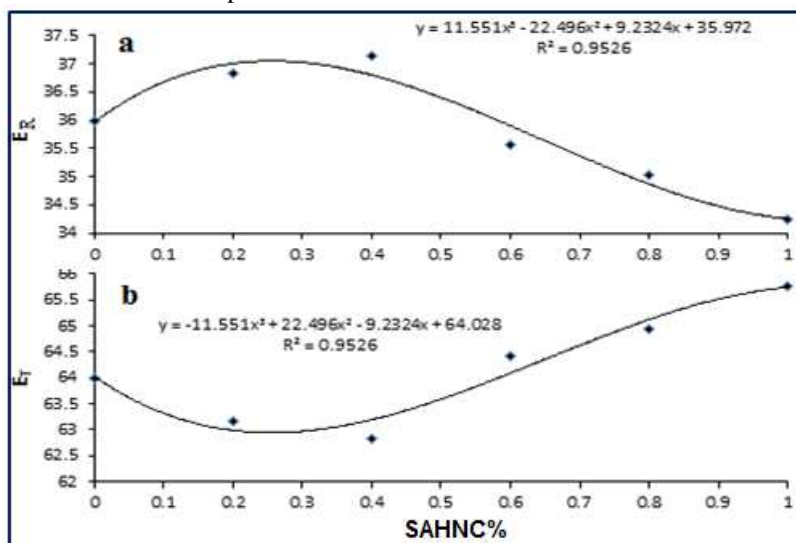


Fig. 12: Percentages of reflected (a) and transmitted (b) energies between steel and concrete hybrid composites

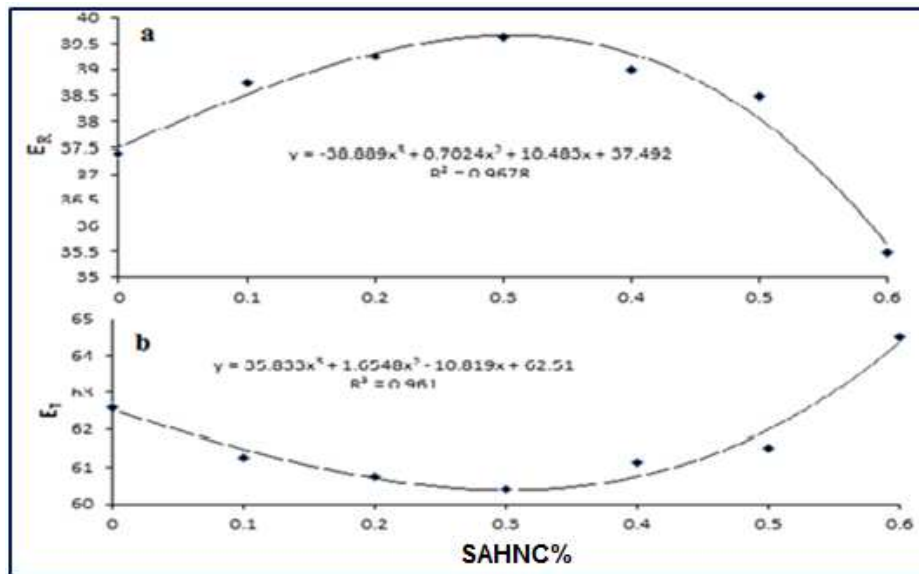


Fig. 13: Percentages of reflected (a) and transmitted (b) energies between steel and mortar hybrid composites

Conclusions:

In this research an attempt was down to improve the concrete and mortar properties by adding SAHNCs. Based on this, it was concluded the following:-

- 1- Compressive strength for concrete and mortar hybrid composites exceeds their initial values at higher SAHNCs ratios.
- 2- The additional amounts of water which is required to get the standard consistency in mortar seem to be reasonable.
- 3- Elastic modulus for these hybrid composites increased at higher ratios.
- 4- Shear modulus increased at higher ratios and there is some fluctuations in mortar shear modulus.
- 5- Most values of Poisons ratio within the typical range for concrete.
- 6- Initial and final setting times of mortar increased with SAHNCs loadings.
- 7- Concrete quality are excellent according to the BS, 1881, 1983 code.
- 8- The acoustic impedance increased, while the energy reflected reaches to its minimum value at higher SAHNCs ratios and the energy transmitted reaches to its maximum value at this ratio.

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